

Stantec Consulting Services Inc. 5 Dartmouth Drive Suite 200, Auburn NH 03032-3984

February 20, 2024 File: 195113533

Attention: Mr. Rudy Cartier Candia Planning Board 74 High Street Candia, NH 03034

Dear Mr. Cartier,

Reference: 669 High Street - Major Site Plan Review#1 Candia Tax Map 405 Lot 48 – Candia Planning Board Case#24-002

In accordance with the request of the Town of Candia, NH Land Use Office we have reviewed the following submitted information, received by email on January 23, 2024, by Jones and Beach Engineers, for the referenced proposed Major Site Plan application in Candia, NH with an associated notice to proceed dated February 7, 2024:

- Major Site Plan, entitled Multi-Family Development, prepared by Jones & Beach, 17-page plan set, dated January 22, 2024.
- Major Site Plan Application, prepared by Jones & Beach, dated January 10, 2024

The project submission was reviewed for conformance with the Town of Candia Zoning Ordinances (Ordinances) and Major Site Plan Regulations (Regulations), as well as other applicable state and local rules and regulations and accepted engineering practices.

Based on our review of the submitted documents we offer the following comments for your consideration:

PROJECT DESCRIPTION

The plans propose the development of an existing 87.8-acre lot, with a 550 linear cul-de-sac common drive roadway proposed intersecting with High Street, across from Donavan Road; with three proposed multifamily buildings (6-units in total), a proposed barn, associated clearing, drainage, utilities, and site improvements. The units will be serviced with an on-site shared well and individual septic systems.

It should be noted that the pre and post storm water calculations and associated report were not provided with the application and that a waiver has been requested by the Applicant for this requirement.

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- 1. The plans specify that 99,000 SF will be disturbed for the proposed improvements; however, based on our review of the proposed improvements the disturbance areas that are specified are unrealistic and the proposed improvements as shown will disturb more than 100,000 SF and will require a NHDES Alteration of Terrain (AoT) permit.
- 2. The plans propose the construction of a barn to the North of the proposed duplex units by accessing an existing 8-foot-wide existing trail through and between existing wetlands, based on this we offer the following comments:
 - a. additional erosion control measures are required to be provided/specified for the access, disturbance and construction activities associated with providing access and constructing the proposed barn.
 - b. The plans specify the use of an existing woods trail for access for the construction of the proposed barn, the existing trail is shown as 8-feet wide in plan view and 12-feet wide in the detail. The 12 –foot wide access seems appropriate but appears to require a wetlands dredge and fill permit at the existing wetlands crossing. Additionally, the grading for this proposed trail widening must be shown on the plans and the disturbance associated with these proposed improvements must be included in the disturbance area total.
 - c. The plans specify a 'proposed trail to connect to the existing trail' and a 'proposed 8-footwide trail to barn' that extends to the proposed barn but the materials and specifics of the proposed trail widening are unclear, we recommend that a typical cross section for construction be provided.
 - d. It is recommended that a subsurface assessment (borings and or test pits) of the existing trail be performed to confirm that the existing trail is suitable to support the necessary construction vehicles and vehicle traffic to the proposed barn without rutting and/or eroding the existing trail and causing impacts to the adjacent wetlands and properties.
- 3. The plans specify that the property is outside of the FEMA Regulated 100-Year Flood Plain, it is required that it also be confirmed that there are no other FEMA FEMA regulated flood plains located within the limits of the proposed improvements, in addition to the 100-year flood plain, as specified in Regulation Section 2.07.
- 4. Test pit logs for the test pits that were performed on the property show a depth to ground water between sixteen and twenty-four inches for the available test pit information that was submitted with the application, additional subsurface investigations including test pits and/or borings are also required to be obtained for the design of the roadway, underdrains and proposed drainage systems, as specified in regulation section 8.06-U.
- 5. The plans show a proposed shared private well to provide the domestic water supply for the three buildings (6 housing units) but no details were submitted with the application regarding the existing hydrogeological information that was obtained for the design of the well or details and no details of the proposed well have been provided by the applicant and/or included on the plans. Additional information and details are required to be specified on the plans and submitted for review to confirm

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Reference: 669 High Street - Major Site Plan Review#1 Candia Tax Map 409 Lot 228

that the proposed well location is suitable and the yield is sufficient for the proposed anticipated domestic and fire protection system(s) demands.

- 6. The specified limits of clearing of the existing/proposed woods trail to the proposed barn appear to be insufficient to provide fire apparatus access to and around the proposed barn. We defer to the Fire Chief on whether the proposed access to and around the proposed buildings are sufficient.
- 7. The plans specify one parking space per unit, but it is required that a minimum of two spaces per unit are provided, as specified in Ordinance section 9.06. The plans specify that twenty-four spaces are proposed/provided in total, but it is unclear how this number is being determined.
- 8. Building setbacks are required to be shown on the plans, including land use restrictions for poorly drained and very poorly drained soils and wetlands in conformance with Ordinance Section 10.
- 9. The plans specify a plan scale of one-inch equals fifty feet (1" = 50') but are required to be provided at a minimum of one-inch equals twenty feet (1" =20'), as specified in Regulation Section 4.03-E, it should be noted that the Applicant has requested a waiver for this regulation.
- 10. The plans only provide a partial boundary, physical conditions, and topographical survey for part of the lot but are required to provide a survey of the entire parcel including the lot perimeter, boundary survey, as specified in Regulation section 4.03-F, 4.03-G and 4.03-I. It should be noted that the applicant has requested a waiver to provide a partial survey for and in proximity to the proposed improvements.
- 11. The plans are required to specify the height of the existing and proposed structures, as specified in Regulation section 4.03-H.
- 12. The plans are required to specify the location, size, and material of all existing and proposed public and private utilities, as specified in Regulation Section 4.03-L.
- 13. The plans are required to provide a schedule for construction, as specified in Regulation section 4.03-Q.
- 14. The plans specify a 'proposed development sign' but no additional details are provided with the application, the Applicant is required to submit, for review and approval, details for the proposed signage for the property, as specified in Regulation Section 4.03-M, in conformance with Ordinance section 8.01 and Specification section 8.03.
- 15. The plans are required to specify the location and type of the proposed fire suppression system(s), as required by the Fire Department, as specified in Regulation Section 4.03-T, in conformance with Regulation section 8.08B.
- The plans provide a signature block for five (5) Board members but are required to provide a signature block for seven (7) Board members, including the chairman, as specified in Regulation section 4.03-U.

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- 17. The plans are required to provide vehicle turning movements for a WB-67, into, around and exiting the site without potentially impacting other vehicles or pedestrian traffic, as specified in Regulation section 4,03-V and section 8.03-A-2.
- 18. The plans propose the installation of culverts, rip rap and a plunge pool in conjunction with the proposed improvements but no drainage analysis or associated drainage report is provided to demonstrate that the design of this proposed drainage infrastructure is appropriate. A drainage analysis and associated report, stamped by a professional Engineer licensed in the State of New Hampshire, with support drainage calculations is required to be provided, as specified in Regulation section 4.05. It should be noted that the Applicant has requested a waiver for this regulation requirement; we recommend that a drainage analysis be performed, calculations and an associated report be submitted for review to confirm conformance with the stormwater standards specified Regulation section 8.06.
- 19. The proposed improvements require the submittal to and approval by the ZBA, NHDOT driveway permit (and/or amendment to the existing permit), NHDES subsurface disposal systems permit, NHDES Alteration of Terrain (AoT), NHDES Dredge and Fill permit and USACOE permit based on the proposed improvements. It is required that a copy of all necessary permits for the project be submitted with the application to the Town in conjunction with the application and that the required permit approval numbers be listed on the cover sheet of the plan set for reference, as specified in Regulation section 4.05.
- 20. The site is required to be provided with a designated and striped space for delivery vehicles, as specified in Regulation Section 8.03-A-2.
- 21. The plans specify that a private driveway is to be built to Town standards, but the access drive, as proposed, does not meet Town roadway standards, we recommend that this note be updated, as appropriate, for clarity or that the design be upgraded to meet town standards.
- 22. Additional existing and proposed spot grades, low/high points and proposed driveway slopes are required to be specified on the plans to confirm that the proposed access drives and parking spaces are provided with slopes that in compliance with Regulation section 8.03-A-4 and that the proposed driveways will not create icing conditions with the shared access road/drive.
- 23. The proposed access drive, barn and parking spaces are provided with less than 0.2 horizontal foot candles; lighting is required to be provided with a minimum of 0.2 horizontal foot candles with an average uniformity ratio of 4:1 and minimum color ratio index of 50 for common space, shared space and parking spaces, as specified in Regulation section 8.03-D.
- 24. The Applicant is required to provide the Planning Board with architectural renderings, including side elevations, proposed materials, and colors for construction for the proposed buildings, as specified and in conformance with the requirements of Regulation Section 8.03-G. No renderings have been submitted for the proposed barn and some of the required architectural rendering information was not submitted with the application for the proposed duplex units.

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- 25. The proposed multi-family structures are required to be provided with a fire alarm system and Knox Box, as specified in Regulation section 8.04-E; it is recommended that a note be added to the plans specifying these requirements.
- 26. All buildings are required to be provided with signage with a minimum of a 4-inch-high letters on a post or mailbox with the property address, it is recommended that the location of the proposed address labels be reviewed and confirmed appropriate with the Fire Department.
- 27. Storage and/or waste collection areas are required to be specified on the plans and provided with proposed screening, as specified in Regulation section 8.05.
- 28. The proposed access drive culverts are specified as twelve-inch HDPE culverts, but are required to be a minimum of fifteen-inch RCP for open drainage systems, as specified in Regulation section 8.06-K and 8.06-Q.
- 29. The plans are required to specify that all excavated waste will be disposed of from the site, as specified in Regulation Section 8.09.
- 30. The plans are required to specify that the solid waste requirements for the disposal of materials from the site shall be performed in conformance with Regulation Section 8.10.
- 31. The landscaping plan is required to be designed by a qualified landscape designer with proposed buffers to mitigate impacts to neighboring properties, as specified in Regulation section 8.14-B and 8.14-C. In general, the proposed landscaping does not appear to satisfy the requirements of Regulation section 8.14.
- 32. The construction of the proposed access driveway will require an NHDOT driveway permit (and/or permit amendment) and temporary traffic signage for construction, it is required that the plans included and specify temporary maintenance and protection of traffic signage plans and details for construction, as specified in Regulation section 8.16.
- 33. The demolition plan (DM-1) specifies that several items are to be removed from the existing property; it is recommended that these notes be expanded to specify the removal <u>and</u> legal disposal offsite for these items being specified as being removed.
- 34. The demolition plan (DM-1) specifies trees to be removed; however, these notes should be expanded to specify trees and stumps to be removed and disposed of offsite.
- 35. The demolition plan (DM-1) specifies 'stone wall toppled over', but it is unclear if this stone wall is being reset as part of the project, which we recommended.
- 36. Additional details regarding the abandonment of the existing well and demolition of the existing buildings are recommended to be specified on the plans to avoid future health and safety concerns.
- 37. On the demolition plan (DM-1) the following tree clearing/tree removal notes should be either standardized or clarified if there are separate intent/direction for the removal and/or disposal of the existing trees on site: "Treeline to Be Removed, Proposed Treeline and Trees to be Removed".

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- 38. On the demolition plan (DM-1), demolition note#2 specifies that the contractor shall stake the clearing limits and that a minimum of 48 hours shall be provide, it is recommended that this note be revised to indicate that the limits of clearing shall be staked for Town's review and approval prior to clearing, in conformance with the tree clearing permit.
- 39. On the demolition plan (DM-1), demolition note#5 specifies that the existing septic system shall be abandoned in accordance with NHDES or Town Standards and Regulations, but no existing septic systems are shown on the plans; it is recommended that the existing septic systems be shown on the plans to confirm whether it (they) are required to be removed to perform the proposed improvements.
- 40. On the demolition plan (DM-1), Demolition note#7 specifies that excavated material will be placed in upland area, but no areas are designated on the plans for excavated material to be placed, given the shallow depth to ground water and the amount of wetlands on the property it is recommended that an excavation material stock pile area and concrete wash out area and associated erosion control measures in conformance with NHDES standards be specified on the plans.
- 41. It is required that the Applicant demonstrate sufficient, all season NHDOT sight distance, at the proposed intersection, as specified in Regulation section 10.06-r.
- 42. The drainage trench detail specifies a minimum of 2-feet of cover, but the proposed grading provides less than 2-feet of cover over the proposed driveway culverts and less than 2-feet of cover behind the proposed headwalls, it is recommended that the driveway culverts be provided with a minimum of 3-feet of cover in paved areas and a minimum of 2-feet of cover in unpaved areas.
- 43. It is recommended that the proposed driveway specify a saw cut and asphalt emulsion joint at the existing High Street pavement for the installation of the proposed driveway.
- 44. Scour protection (rip rap) is required to be specified/provided for the outlet to the proposed 18-inch culvert.
- 45. Rip rap sizing calculations in conformance with NHDES standards are required to be provided to confirm that the proposed rip rap apron stone sizes, stone thickness, and apron dimensions are sufficient.
- 46. The swale, down stream of the proposed 18-inch head wall outlet, is proposed with a slope greater than 5-percent, rip rap is required to be provided in/for this swale to prevent erosion.
- 47. The material details for the proposed water service including the water shut off, water pipe material and water pipe class are required to be specified on the plans for construction.
- 48. The proposed intersection of the primary access drive and the end of the cul-de-sac proposed two different cross slopes at this location, 1.4-percent and 2.0-percent, additional details are required to be specified for the construction of this proposed intersection.
- 49. Additional details and/or deed occupancy restrictions are required to ensure that the proposed well is not being proposed as or could potentially serve a small community system; for a water supply of 25, or more, people the well would be considered a small community system and would be subject

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Reference: 669 High Street - Major Site Plan Review#1 Candia Tax Map 409 Lot 228

to the requirements of NHDES Env Dw 305. If deed restrictions are not put on the property maximizing the number of occupants, then we recommend that the proposed community well be submitted to NHDES for review and approval as a small community well system.

- 50. It is required that a statement from the Candia Tax Collector indicating whether the property is under current taxation status or not be received for the project, as specified in Regulation section 10.06m.
- 51. It is required that a letter from the Fire Chief and Police Chief be obtained regarding their review and recommendations regarding safety issues and/or concerns for the project, as specified in Regulation section 10.06-n.
- 52. Additional erosion control measures are required to be specified between the disturbed area at the proposed intersection/access drive and the adjacent wetlands.
- 53. The typical road cross section detail specifies underdrain, but no underdrain is specified in plan view(s). It is required that the proposed underdrain be shown on the plans.
- 54. It is recommended that the access drive stationing be shown on all the plan sheets.
- 55. It appears that, based on the proposed grading, that guardrail is required from STA 1+60 to STA 2+70 on the right side of the road.
- 56. It appears that a cross culvert is necessary under the access drive at approximate STA 0+30 to keep stormwater from impounding up grade of the proposed access driveway.
- 57. A minimum of three benchmarks are recommended to the specified on the plans for construction.
- 58. It is recommended that the Board discuss whether the proposed cul-de-sac road should be designated as a private road with an associated street sign and property address numbers to minimize potential confusion from future first responders.
- 59. The plans specify/reference an assumed vertical and horizontal bearing, given the shallow ground water and proximity to wetlands it is recommended that a horizontal and vertical datum be established and specified on the plans for construction.
- 60. A 2:1 slope is proposed on both sides of proposed duplex unit 5/6, it is recommended that the grading be revised to eliminate these steep slopes where immediately adjacent to the proposed building.
- 61. The proposed grading creates a swale within 35-feet to the south of the proposed subsurface septic disposal system for duplex units 5/6, this proposed grading, and/or the location of the proposed leach field are required to be revised to conform with NHDES requirements.

These comprise our comments at this time. We invite the Engineer and Applicant to meet with us to discuss these comments and other design related topics, which may affect the project and the associated design. We reserve the right to make future comments based on proposed revisions and additional submissions.

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If you have any questions or need any additional information, please feel free to contact us.

Respectfully,

Stantec Consulting Services Inc.

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Bryan Ruoff PE Associate Phone: 603 854 9501 Fax: 603 669 7636 bryan.ruoff@stantec.com

Attachment: N/A

c. Candia Planning Board Amy Spencer, Town of Candia Rene LaBranche, Stantec



85 Portsmouth Avenue, PO Box 219, Stratham, NH 03885 603.772.4746 - JonesandBeach.com

March 21, 2024

Candia Planning Board Attn. Rudy Cartier 74 High Street Candia, NH 03034

RE: Response Letter & Special Use Permit Criteria response. Beaver Meadows Duplex Development 669 High Street Candia, NH Map 405, Lot 48 JBE Project No. 22201

Dear Mr. Cartier,

We are in receipt of comments from Brian Ruoff, P.E. from Stantec Consulting Services dated February 20, 2024, Rudy Cartier, Planning Board Chair dated February 22, 2024, Michael McGillen, Candia Police dated March 5, 2024, and Jeff Wuebbolt, Road Agent dated March 6, 2024. Review comments are listed below with our responses in bold.

We are also providing the criteria for the Special Use Permit for the wetland buffer impacts for the driveway. We will be providing performance security to ensure that the construction is carried out in accordance with the approved design as required by the Planning Board. This will be done prior to construction and after Planning Board approval and is typically a condition of approval.

Section 10.09: Conditional Uses

- A. A Special Use Permit may be granted by the Planning Board (RSA 674:21-11) for the construction of roads and other access ways, and for pipelines, power lines and other transmission lines provided that all of the following conditions are found to exist:
- 1. The proposed construction is essential to the productive use of land not within the Wetlands Conservation District.

RESPONSE: The proposed location of the driveway is over the existing driveway in order to minimize the impacts to the site. The existing driveway is aligned with Donovan Road and so is the proposed driveway. The proposed driveway needs to be widened to allow for 2 way traffic and is currently only one lane wide as it provides access to a single family house. This is the ideal location for access and is essential to the productive use of the uplands given the alignment with Donovan Road. The existing yard and landscaping in the front of the site will not be impacted with this design. The wetland at the front of the property is a small isolated wetlands.

2. Design, construction and maintenance methods will be such as to minimize detrimental impact upon the wetland and will include restoration of the site as nearly as possible to its original grade and condition.

RESPONSE: The new driveway will be a 20' wide paved driveway which will minimize the erosion and be stabilized. As you know, maintenance of gravel driveways often ends up with sediment flowing off the driveway during hard rain events and gravel being plowed in the winter off of the driveway. Paving this driveway will reduce both of those things from happening. A condition of the ZBA approval is that the back of the land will not be further developed for housing.

 No alternative route which does not cross a wetland or has less detrimental impact upon the wetland is feasible.
 RESPONSE: The Town Road Agent wants this driveway to be aligned with Donovan Road as that is property driveway design and access management for roadways. We do not have another location that would accomplish this access point.

Stantec Comments:

- The plans specify that 99,000 SF will be disturbed for the proposed improvements; however, based on our review of the proposed improvements the disturbance areas that are specified are unrealistic and the proposed improvements as shown will disturb more than 100,000 SF and will require a NHDES Alteration of Terrain (AoT) permit.
 RESPONSE: A NHDES Alteration of Terrain permit is not required. We are below the threshold for this permit and we have moved the proposed units closer to the road in order to reduce the area of disturbance.
- 2. The plans propose the construction of a barn to the North of the proposed duplex units by accessing an existing 8-foot-wide existing trail through and between existing wetlands, based on this we offer the following comments:
- a. additional erosion control measures are required to be provided/specified for the access, disturbance and construction activities associated with providing access and constructing the proposed barn.

RESPONSE: Additional erosion control measures have been added to the plans, including silt soxx at the existing wetland crossing and silt fence near the proposed barn.





- b. The plans specify the use of an existing woods trail for access for the construction of the proposed barn, the existing trail is shown as 8-feet wide in plan view and 12-feet wide in the detail. The 12 –foot wide access seems appropriate but appears to require a wetlands dredge and fill permit at the existing wetlands crossing. Additionally, the grading for this proposed trail widening must be shown on the plans and the disturbance associated with these proposed improvements must be included in the disturbance area total.
 RESPONSE: The plan is to keep the existing rural driveway to the future barn. We are not widening the driveway to 12', that was a holdover on the detail. No wetland permit is required. The trail has been actively used by vehicles for equipment for decades.
- c. The plans specify a 'proposed trail to connect to the existing trail' and a 'proposed 8-footwide trail to barn' that extends to the proposed barn but the materials and specifics of the proposed trail widening are unclear, we recommend that a typical cross section for construction be provided.
 PESPONSE: A note specifying the materials and surface treatment for the trail has

RESPONSE: A note specifying the materials and surface treatment for the trail has been added to the Woods Trail Section on Sheet D1.

- d. It is recommended that a subsurface assessment (borings and or test pits) of the existing trail be performed to confirm that the existing trail is suitable to support the necessary construction vehicles and vehicle traffic to the proposed barn without rutting and/or eroding the existing trail and causing impacts to the adjacent wetlands and properties.
 RESPONSE: We do not believe test pits are required, this is an existing trail/gravel drive to access a barn, not a road or a highway. However, test pit 5 represents conditions near the proposed trail extension coming off of the shared access driveway for the duplexes and test pit 7 represents the conditions near the gravel access driveway to the barn.
- 3. The plans specify that the property is outside of the FEMA Regulated 100-Year Flood Plain, it is required that it also be confirmed that there are no other FEMA regulated flood plains located within the limits of the proposed improvements, in addition to the 100-year flood plain, as specified in Regulation Section 2.07. RESPONSE: There are no FEMA Regulated flood plains within the area of the proposed development.
- 4. Test pit logs for the test pits that were performed on the property show a depth to ground water between sixteen and twenty-four inches for the available test pit information that was submitted with the application, additional subsurface investigations including test pits and/or borings are also required to be obtained for the design of the roadway, underdrains and proposed drainage systems, as specified in regulation section 8.06-U. RESPONSE: Test pits were performed and that is why the proposed driveway is raised and designed the way it is. Test pits 3 and 4 specifically represent the subsurface conditions near the proposed access driveway.
- 5. The plans show a proposed shared private well to provide the domestic water supply for the three buildings (6 housing units) but no details were submitted with the application regarding the existing hydrogeological information that was obtained for the design of the well or details and no details of the proposed well have been provided by the applicant and/or included on the plans. Additional information and details are required to be specified on the plans and submitted for review to confirm that the proposed well

location is suitable and the yield is sufficient for the proposed anticipated domestic and fire protection system(s) demands.

RESPONSE: A conceptual well layout detail has been added to Sheet D3 and more detail has been added to Sheet C6 regarding the layout and design intent of the water system. Fire protection systems are not required and the yield should be suitable for the domestic services.

6. The specified limits of clearing of the existing/proposed woods trail to the proposed barn appear to be insufficient to provide fire apparatus access to and around the proposed barn. We defer to the Fire Chief on whether the proposed access to and around the proposed buildings are sufficient.

RESPONSE: We spoke with the Fire Chief after the Planning Board meeting and he is not concerned about the width of the existing and proposed gravel trails. He should be providing a letter to the Planning Board ahead of the next meeting.

- 7. The plans specify one parking space per unit, but it is required that a minimum of two spaces per unit are provided, as specified in Ordinance section 9.06. The plans specify that twenty-four spaces are proposed/provided in total, but it is unclear how this number is being determined.
 RESPONSE: We are providing 3 spaces per unit one in the garage, one in the driveway, and one in the 9'x18' bumpout. This is explained in Note #5 on Sheet C4.
- Building setbacks are required to be shown on the plans, including land use restrictions for poorly drained and very poorly drained soils and wetlands in conformance with Ordinance Section 10.
 RESPONSE: Building setbacks are shown on the plans.
- 9. The plans specify a plan scale of one-inch equals fifty feet (1" = 50') but are required to be provided at a minimum of one-inch equals twenty feet (1" =20'), as specified in Regulation Section 4.03-E, it should be noted that the Applicant has requested a waiver for this regulation.
 RESPONSE: No response necessary.
- 10. The plans only provide a partial boundary, physical conditions, and topographical survey for part of the lot but are required to provide a survey of the entire parcel including the lot perimeter, boundary survey, as specified in Regulation section 4.03-F, 4.03-G and 4.03-I. It should be noted that the applicant has requested a waiver to provide a partial survey for and in proximity to the proposed improvements. **RESPONSE: No response necessary.**
- 11. The plans are required to specify the height of the existing and proposed structures, as specified in Regulation section 4.03-H.
 RESPONSE: The heights of the existing and proposed structures have been added to the plans. The heights of the existing buildings are measured in stories based on publicly available GIS data on Sheet C1 while the heights of the proposed buildings are measured in feet on Sheet C4.



- 12. The plans are required to specify the location, size, and material of all existing and proposed public and private utilities, as specified in Regulation Section 4.03-L.
 RESPONSE: The location, size, and material of all existing and proposed public and private utilities are already on the plans.
- 13. The plans are required to provide a schedule for construction, as specified in Regulation section 4.03- Q.
 RESPONSE: A schedule for construction is included with this letter and also on Sheet C4.
- 14. The plans specify a 'proposed development sign' but no additional details are provided with the application, the Applicant is required to submit, for review and approval, details for the proposed signage for the property, as specified in Regulation Section 4.03-M, in conformance with Ordinance section 8.01 and Specification section 8.03. RESPONSE: We will provide a detail for the development sign prior to final plan approval but this information is not available at this time.
- 15. The plans are required to specify the location and type of the proposed fire suppression system(s), as required by the Fire Department, as specified in Regulation Section 4.03-T, in conformance with Regulation section 8.08B.
 RESPONSE: Fire suppression is not required for duplexes in New Hampshire and Section 8.08B specifically says that fire suppression is required for "all new multi-family structures of three or more dwelling units".
- 16. The plans provide a signature block for five (5) Board members but are required to provide a signature block for seven (7) Board members, including the chairman, as specified in Regulation section 4.03-U.
 RESPONSE: The signature block for the Planning Board has been increased to include 7 lines.
- 17. The plans are required to provide vehicle turning movements for a WB-67, into, around and exiting the site without potentially impacting other vehicles or pedestrian traffic, as specified in Regulation section 4,03-V and section 8.03-A-2.
 RESPONSE: Vehicle turning movements have been added to the plans for realistic sized vehicles including a fire truck and a SU-30. Typically, we would only run a WB-67 as the design vehicle for a commercial or industrial site that is anticipated to take tractor-trailer deliveries. We are requesting a waiver for the requirement to run a WB-67.
- 18. The plans propose the installation of culverts, rip rap and a plunge pool in conjunction with the proposed improvements but no drainage analysis or associated drainage report is provided to demonstrate that the design of this proposed drainage infrastructure is appropriate. A drainage analysis and associated report, stamped by a professional Engineer licensed in the State of New Hampshire, with support drainage calculations is required to be provided, as specified in Regulation section 4.05. It should be noted that the Applicant has requested a waiver for this regulation requirement; we recommend that a drainage analysis be performed, calculations and an associated report be submitted for review to confirm conformance with the stormwater standards specified Regulation section 8.06.

RESPONSE: A drainage report is included with this resubmission.



- 19. The proposed improvements require the submittal to and approval by the ZBA, NHDOT driveway permit (and/or amendment to the existing permit), NHDES subsurface disposal systems permit, NHDES Alteration of Terrain (AoT), NHDES Dredge and Fill permit and USACOE permit based on the proposed improvements. It is required that a copy of all necessary permits for the project be submitted with the application to the Town in conjunction with the application and that the required permit approval numbers be listed on the cover sheet of the plan set for reference, as specified in Regulation section 4.05. RESPONSE: A list of permits has been added to the cover sheet. Only NHDOT and septic approvals are required, and they are filed digitally with the state. We will provide permit numbers once received.
- 20. The site is required to be provided with a designated and striped space for delivery vehicles, as specified in Regulation Section 8.03-A-2.
 RESPONSE: A waiver has been requested for the cited requirement.
- 21. The plans specify that a private driveway is to be built to Town standards, but the access drive, as proposed, does not meet Town roadway standards, we recommend that this note be updated, as appropriate, for clarity or that the design be upgraded to meet town standards. **RESPONSE: The access driveway is to meet the gravel quality of a town road, not** the dimensions. The note stating that the private driveway is to be built to Town standards.

the dimensions. The note stating that the private driveway is to be built to Town standards has been removed from the plan.

22. Additional existing and proposed spot grades, low/high points and proposed driveway slopes are required to be specified on the plans to confirm that the proposed access drives and parking spaces are provided with slopes that in compliance with Regulation section 8.03-A-4 and that the proposed driveways will not create icing conditions with the shared access road/drive.

RESPONSE: Additional spotgrades and driveway slopes have been added to confirm that the driveway and parking lot grades are within the allowable range per Section 8.03-A-4. The driveway for Units 5-6 is the longest driveway and it is sloped toward a low point, while the driveways for Units 1-2 and Units 3-4 slope toward the roadway but they are 55' long and 44' long respectively. We do not anticipate the driveway runoff to cause icing conditions on the shared access driveway, which is sloped directly toward the center island and is not curbed.

23. The proposed access drive, barn and parking spaces are provided with less than 0.2 horizontal foot candles; lighting is required to be provided with a minimum of 0.2 horizontal foot candles with an average uniformity ratio of 4:1 and minimum color ratio index of 50 for common space, shared space and parking spaces, as specified in Regulation section 8.03-D.

RESPONSE: A waiver has been requested for the cited requirement in order to preserve the rural character of the neighborhood.

24. The Applicant is required to provide the Planning Board with architectural renderings, including side elevations, proposed materials, and colors for construction for the proposed buildings, as specified and in conformance with the requirements of Regulation Section 8.03-G. No renderings have been submitted for the proposed barn and some of



the required architectural rendering information was not submitted with the application for the proposed duplex units.

RESPONSE: Floor plans and elevations as well as a front rendering showing the color and materials for the siding and roofs of the duplexes is included with this resubmission. Additional information, including a rendering of the barn, will be submitted once ready but it is not available at this time.

- 25. The proposed multi-family structures are required to be provided with a fire alarm system and Knox Box, as specified in Regulation section 8.04-E; it is recommended that a note be added to the plans specifying these requirements.
 RESPONSE: The cited requirement references "multi-family structures of three (3) or more dwelling units" and therefore is not applicable for duplexes.
- 26. All buildings are required to be provided with signage with a minimum of a 4-inch-high letters on a post or mailbox with the property address, it is recommended that the location of the proposed address labels be reviewed and confirmed appropriate with the Fire Department.

RESPONSE: See Note #23 on Sheet C4.

- 27. Storage and/or waste collection areas are required to be specified on the plans and provided with proposed screening, as specified in Regulation section 8.05.
 RESPONSE: See Note #22 on Sheet C4. In lieu of a dumpster, each tenant or unit owner will be responsible for their own trash removal.
- 28. The proposed access drive culverts are specified as twelve-inch HDPE culverts, but are required to be a minimum of fifteen-inch RCP for open drainage systems, as specified in Regulation section 8.06-K and 8.06-Q.
 RESPONSE: The proposed culverts have been revised to be the required minimum 15" diameter. However, we do not typically spec RCP culverts under driveways. ADS-N12 HDPE is industry standard and we are requesting a waiver to use ADS-N12 HDPE culverts.
- 29. The plans are required to specify that all excavated waste will be disposed of from the site, as specified in Regulation Section 8.09. **RESPONSE: See Note #8 on Sheet DM-1.**
- 30. The plans are required to specify that the solid waste requirements for the disposal of materials from the site shall be performed in conformance with Regulation Section 8.10. **RESPONSE:**
 - a) Description of the solid waste to be generated by the site.
 Common household waste will be generated by this multi-family residential use.
 - b) Description of the on-site solid waste facilities. Each tenant or unit owner shall store trash indoors and shall be responsible for their own waste removal. See Note #22 on Sheet C4.
 - *c)* A removal schedule showing volume and frequency. Each tenant or unit owner will likely haul their trash and recycling to the dump weekly or by-weekly. The volume of waste will be dependent on the number of people living in each unit.
 - *d)* A statement acknowledging the conditions imposed by the Candia Recycling Center Regulations and the method by which the site will conform with those conditions.



These conditions will remain in effect. See Note #25 on Sheet C4.

31. The landscaping plan is required to be designed by a qualified landscape designer with proposed buffers to mitigate impacts to neighboring properties, as specified in Regulation section 8.14-B and 8.14-C. In general, the proposed landscaping does not appear to satisfy the requirements of Regulation section 8.14.

RESPONSE: We are keeping existing tree buffers around the property and we meet all applicable requirements of Section 8.14.

Section 8.14 A: All site plans shall include a landscaping plan designed by a qualified landscaping Designer. The Board shall make the final determination of whether the landscape Designer is qualified.

Response: This is for the Planning Board to determine.

Section 8.14 B: For all proposed landscaped areas a minimum of 4-inches of topsoil, with 5% organic matter incorporated shall be spread in all planting and turf areas. Response: See Note #16 on Sheet L1.

Section 8.14 C: Landscape plans shall be designed to provide buffers in an effort to mitigate impacts to neighboring properties. Buffers are intended to physically separate one use or property from another so as to visually shield or block, noise, lights, provide a water quality benefit and to minimize other impacts.

Response: We are maintaining existing tree buffer in order to shield abutting properties from the proposed land use.

Section 8.14 C (continued): a. Along the property line of a property, buffers are required in the following instances: i. Where a proposed non-residential use abuts a residential zoning district.; ii. Where a proposed non-residential use abuts an existing residential use; and iii. Where a proposed roadway abuts an existing property line or is within 20-feet of a property line where the existing use is residential. b. Within a property, buffers are required to provide visual screens in the following instances: i. Outdoor Storage Areas; and ii. Refuse and Recycling Collection Areas Response: None of these are applicable. This is a residential use; the shared access driveway is more than 20' from the nearest abutter and no refuse and recycling collection areas are proposed.

Section 8.14 D: Within a property landscaping buffers shall meet the following criteria: a. Buffers shall be located to prevent visibility of the above listed items from the parking areas, traveled right-of-way or neighboring properties. b. Buffers shall be at least 6-feet in height and may consist of fencing, evergreens, berms, mounds or combinations thereof. Chain link fencing with privacy slats are discouraged. Response: The existing tree buffers that we are maintaining meet this requirement.

Section 8.14 E: Landscaping shall be provided along all building frontage. A minimum of one (1) shrub for every 12-feet of building frontage shall be provided. In instances where it is not possible to locate all required shrubs along the building frontage due to doorways, walkways or other impervious surfaces, the required shrubs shall be utilized within the parking lot or landscape buffers. Plant locations are designed to be flexible and not necessarily in even spaced intervals.

Response: 20 New England Aster perennials are proposed in front of each building. 80 feet of frontage are provided on each duplex building and therefore a minimum



of 7 shrubs or perennials shall be required. These are placed in the corner between each driveway and parking space for maximum aesthetic appeal.

Section 8.14 F: Peripheral landscaping shall be required along all sides of a parking lot or access way that abuts adjoining property or a public right. Response: A combination of existing and proposed landscaping is provided along the proposed access driveway in order to satisfy this requirement.

Section 8.14 G: Landscaping within parking lots or green space encompassing not less than five (5%) percent of the total parking area shall be required. A minimum of one (1) tree for every fifteen (15) parking spaces shall be provided. These trees shall be complemented by suitable ground cover and shrubs.

Response: Not applicable. A parking lot is not proposed.

Section 8.14 H: A minimum 4-foot wide landscape area shall be provided surrounding each free-standing sign base.

Response: Perennials are proposed surrounding the development sign in the front of the property.

Section 8.14I: Bare soil is not acceptable. The introduction of groundcovers and/or perennials planted, the use of mulch or other natural material as a soil covering is acceptable. However, no more than twenty percent of the minimum landscaped area may be covered with nonliving landscaping materials such as bark mulch, woodchips or leaf litter.

Response: All pervious areas of the subject parcel will be covered by plantings, grass, or natural woods post-construction.

Section 8.14 J: Use of Existing Landscaping Towards Requirements: a. Each existing healthy and native or non-invasive tree, with a caliper of 3-inches or greater, preserved using proper protection methods within the interior parking lot area may be substituted for one tree required for every fifteen (15) parking spaces. b. Where an Applicant proposes leaving a significant portion of healthy non-invasive trees and other vegetation within the proposed parking area, the Board may consider alternative landscaping designs.

Response: We are proposing to maintain a natural tree buffer that meets this requirement.

Section 8.14 K: All trees, shrubs and ground cover shall be planted according to accepted horticultural standards. a. Minimum for shade or canopy trees shall be 3inches in diameter measured at breast height, with a height not less than 12-feet. b. Minimum size for small or minor shade trees shall be 2.5-inches in diameter measured breast height, with a height of not less than 9-feet. c. Minimum size for ornamental or flowering fruit trees shall be 2-inches in diameter measured at breast height, with a height of not less than 7-feet. d. Minimum size for evergreen trees shall be 6-feet in height. e. Minimum size for a shrubbery shall be 1.5-feet in height or spread. f. All trees and shrubs shall be appropriately pruned after planting with all broken or damaged branches removed.

Response: The proposed landscaping meets these size requirements.

Section 8.14 L: All landscaping shall be completed prior to the issuance of a Certificate of Occupancy. An inspection of all plantings to ensure compliance with the approved



landscaping plan shall be conducted prior to the issuance of a Certificate of Occupancy. Ongoing inspections of landscapes shall be conducted to ensure compliance of the site with the approved landscape plan in perpetuity. Response: See Note #17 on Sheet L1.

Section 8.14 M: All landscaping shall be warranted for one (1) year from the issuance of a Certificate of Occupancy. Response: See Note #8 on Sheet L1.

- 32. The construction of the proposed access driveway will require an NHDOT driveway permit (and/or permit amendment) and temporary traffic signage for construction, it is required that the plans included and specify temporary maintenance and protection of traffic signage plans and details for construction, as specified in Regulation section 8.16. RESPONSE: A NHDOT permit will be obtained for this project. Temporary sign placement is unknown at this time and will be incidental to the construction. The cited Regulation section does not state that temporary signs need to be shown on the plan set.
- 33. The demolition plan (DM-1) specifies that several items are to be removed from the existing property; it is recommended that these notes be expanded to specify the removal and legal disposal offsite for these items being specified as being removed. **RESPONSE: See Note #11 on Sheet DM-1.**
- 34. The demolition plan (DM-1) specifies trees to be removed; however, these notes should be expanded to specify trees and stumps to be removed and disposed of offsite.
 RESPONSE: The note "Trees to be removed" on the plan has been revised to state "Trees and stumps to be removed and legally disposed off-site."
- 35. The demolition plan (DM-1) specifies 'stone wall toppled over', but it is unclear if this stone wall is being reset as part of the project, which we recommended.
 RESPONSE: This refers to a stone wall in the Route 27 right of way that is not being rebuilt at this time.
- 36. Additional details regarding the abandonment of the existing well and demolition of the existing buildings are recommended to be specified on the plans to avoid future health and safety concerns. RESPONSE: See Notes 9 and 10 on Sheet DM-1.
- 37. On the demolition plan (DM-1) the following tree clearing/tree removal notes should be either standardized or clarified if there are separate intent/direction for the removal and/or disposal of the existing trees on site: "Treeline to Be Removed, Proposed Treeline and Trees to be Removed".

RESPONSE: Most of the work is being done in the cleared area. The owner may remove trees or keep ones for firewood or lumber milling. This will be the owner's decision.

38. On the demolition plan (DM-1), demolition note#2 specifies that the contractor shall stake the clearing limits and that a minimum of 48 hours shall be provide, it is recommended that this note be revised to indicate that the limits of clearing shall be



staked for Town's review and approval prior to clearing, in conformance with the tree clearing permit.

RESPONSE: Note #2 on the demolition plan has been revised to indicate that the limits of clearing shall be staked for Town's review and approval prior to clearing.

- 39. On the demolition plan (DM-1), demolition note#5 specifies that the existing septic system shall be abandoned in accordance with NHDES or Town Standards and Regulations, but no existing septic systems are shown on the plans; it is recommended that the existing septic systems be shown on the plans to confirm whether it (they) are required to be removed to perform the proposed improvements. RESPONSE: It is noted on Sheet DM-1 that the existing septic system shall be removed or abandoned. The existing septic system is old and minimal in size.
- 40. On the demolition plan (DM-1), Demolition note #7 specifies that excavated material will be placed in upland area, but no areas are designated on the plans for excavated material to be placed, given the shallow depth to ground water and the amount of wetlands on the property it is recommended that an excavation material stock pile area and concrete wash out area and associated erosion control measures in conformance with NHDES standards be specified on the plans.
 RESPONSE: The intent of this note is that the contractor will use any suitable spoils from excavation as fill materials in other upland parts of the site. A stockpile area is shown on Sheet DM-1 and C5 as well.
- 41. It is required that the Applicant demonstrate sufficient, all season NHDOT sight distance, at the proposed intersection, as specified in Regulation section 10.06-r.
 RESPONSE: See Sheet H1 showing 400' of intersection sight distance in both directions.
- 42. The drainage trench detail specifies a minimum of 2-feet of cover, but the proposed grading provides less than 2-feet of cover over the proposed driveway culverts and less than 2-feet of cover behind the proposed headwalls, it is recommended that the driveway culverts be provided with a minimum of 3-feet of cover in paved areas and a minimum of 2-feet of cover in unpaved areas.

RESPONSE: The culvert depths have been revised to provide at least 2' of cover in unpaved areas and at least 3' of cover in paved areas.

- 43. It is recommended that the proposed driveway specify a saw cut and asphalt emulsion joint at the existing High Street pavement for the installation of the proposed driveway. **RESPONSE: A sawcut line and a leadered note stating to place an asphalt emulsion joint has been added to Sheet DM-1.**
- 44. Scour protection (rip rap) is required to be specified/provided for the outlet to the proposed 18-inch culvert.
 RESPONSE: Rip rap outlet protection is now provided at all proposed culvert outlets.
- 45. Rip rap sizing calculations in conformance with NHDES standards are required to be provided to confirm that the proposed rip rap apron stone sizes, stone thickness, and apron dimensions are sufficient.



RESPONSE: Rip rap calculations have been performed and these calculations are available within the drainage report.

46. The swale, downstream of the proposed 18-inch head wall outlet, is proposed with a slope greater than 5-percent, rip rap is required to be provided in/for this swale to prevent erosion.

RESPONSE: A rip rap outlet protection apron is proposed at the end of the 15" culvert (we changed the size after running the drainage analysis) and NAG S150 erosion control fabric is proposed to line the bottom of the swale.

- 47. The material details for the proposed water service including the water shut off, water pipe material and water pipe class are required to be specified on the plans for construction.
 RESPONSE: It is noted on Sheet C6 that the water services shall be CTS SDR 9 HDPE or stronger.
- 48. The proposed intersection of the primary access drive and the end of the cul-de-sac proposed two different cross slopes at this location, 1.4-percent and 2.0-percent, additional details are required to be specified for the construction of this proposed intersection.

RESPONSE: Additional spotgrades have been added to clarify the design intent around the intersection of the primary access drive and the end of the cul-de-sac.

49. Additional details and/or deed occupancy restrictions are required to ensure that the proposed well is not being proposed as or could potentially serve a small community system; for a water supply of 25, or more, people the well would be considered a small community system and would be subject to the requirements of NHDES Env Dw 305. If deed restrictions are not put on the property maximizing the number of occupants, then we recommend that the proposed community well be submitted to NHDES for review and approval as a small community well system.

RESPONSE: See Note #24 on Sheet C2 stipulating that the maximum occupancy of each unit shall be 4 persons.

50. It is required that a statement from the Candia Tax Collector indicating whether the property is under current taxation status or not be received for the project, as specified in Regulation section 10.06m.

RESPONSE: Per the landowner, the property is not under current use. We have not been able to obtain a statement from the Tax Collector to this effect at this time, but this requirement is in the Subdivision Regulations and is not applicable to a residential site plan.

- 51. It is required that a letter from the Fire Chief and Police Chief be obtained regarding their review and recommendations regarding safety issues and/or concerns for the project, as specified in Regulation section 10.06-n.
 RESPONSE: We received a review letter from the Police Chief dated March 5, 2024. A response to his comment is contained within this letter. We have not yet received a review letter from the Fire Chief.
- 52. Additional erosion control measures are required to be specified between the disturbed area at the proposed intersection/access drive and the adjacent wetlands.



RESPONSE: We added silt soxx where the existing trail intersects the two wetland areas. No work is planned there. Otherwise, silt fence has been added between the entrance driveway and the isolated wetland pocket.

- 53. The typical road cross section detail specifies underdrain, but no underdrain is specified in plan view(s). It is required that the proposed underdrain be shown on the plans.
 RESPONSE: The road is a fill condition above seasonal high water table, so no underdrain is needed. The underdrain has been removed from the typical road cross section details.
- 54. It is recommended that the access drive stationing be shown on all the plan sheets. RESPONSE: The access drive stationing has been added to the site plan and utility plan. Showing it on the grading plan would be redundant and messy.
- 55. It appears that, based on the proposed grading, that guardrail is required from STA 1+60 to STA 2+70 on the right side of the road.
 RESPONSE: The side slopes in this area have been switched from 2:1 to 3:1 in order to avoid the need for guardrail.
- 56. It appears that a cross culvert is necessary under the access drive at approximate STA 0+30 to keep stormwater from impounding upgrade of the proposed access driveway. RESPONSE: In lieu of a culvert, we have expanded the proposed swale along the east edge of the entrance driveway to extend almost to the right of way line. This will prevent stormwater from impounding upgrade of the driveway. A driveway cross culvert here would not be able to have 2' of cover as required. The grade of the isolated wetland that the culvert would be ouletting into is approximately 196 and the grade of the driveway in this location is approximately 199 and cannot be brought higher. Therefore, a 15" culvert at this location with an invert elevation of 196.2 would only have 1.55' of cover, so we need to instead extend the swale.
- 57. A minimum of three benchmarks are recommended to be specified on the plans for construction.
 RESPONSE: Three benchmarks (TBM A, TBM B, and SPK 18) are shown on Sheet C2.
- 58. It is recommended that the Board discuss whether the proposed cul-de-sac road should be designated as a private road with an associated street sign and property address numbers to minimize potential confusion from future first responders. RESPONSE: Per the Road Agent comment that we respond to below, the access driveway shall never become a public or town-maintained road.
- 59. The plans specify/reference an assumed vertical and horizontal bearing, given the shallow ground water and proximity to wetlands it is recommended that a horizontal and vertical datum be established and specified on the plans for construction. **RESPONSE: The horizontal and vertical datums are relative & sufficient. There is nothing to gain by putting the plan on a different datum.**
- 60. A 2:1 slope is proposed on both sides of proposed duplex unit 5/6, it is recommended that the grading be revised to eliminate these steep slopes where immediately adjacent to the proposed building.



RESPONSE: The slopes adjacent to buildings have been changed to 3:1 minimum.

61. The proposed grading creates a swale within 35-feet to the south of the proposed subsurface septic disposal system for duplex units 5/6, this proposed grading, and/or the location of the proposed leach field are required to be revised to conform with NHDES requirements.

RESPONSE: The top of the swale, which does not intercept the seasonal high water table, is 35' away from the leach fields and 25' from the septic tanks at minimum.

Planning Board Comments:

- Section I, Line 5: Scale of Plan (1" =20' minimum)

 Scale of Plan submitted as 1" = 50'
 Waiver requested.

 RESPONSE: No response necessary.
- Section II, Line 10: Boundary line of site shown.
 Boundary lines are not all shown.
 Waiver requested.
 RESPONSE: No response necessary.
- Section II, Line 11: Bearings and distances shown.
 - Bearings and distances not all shown.
 - Waiver requested.

RESPONSE: No response necessary.

- Section II, Line 13: Plans drawn in ink on transparent mylar.
 - *Mylar not submitted.*
 - *Mylar to be submitted upon final plat approval.*

RESPONSE: A mylar will be submitted once final plat approval is received.

- Section II. Line 14: Existing grades shown.
 - Existing grades are not all shown.
 - Waiver requested.

RESPONSE: No response necessary.

- Section II, Line 17: Use of all abutting properties shown with all structures there on and access roads.
 - o Structures not shown.
 - Add abutting properties existing structures.

RESPONSE: See Aerial Site Plans – Sheet AR1 & AR2. Abutting structures are shown on these plans.

- Section II, Line 20: Special features, natural and man-made, affecting site or giving it character (see list).
 - Several items (such as streams and wetlands) not fully shown for part of site.
 - Waiver requested.

RESPONSE: No response necessary.



- Section III, Line 2: Proposed streets, including names.
 Proposed streets not shown.
 - Proposed streets to be determined.

RESPONSE: The street name has not been determined at this time.

- Section III, Line 3: Proposed drives, parking spaces and sidewalks.
 - Sidewalks not shown.
 - Sidewalks to be added.

RESPONSE: A waiver for the sidewalk requirement is included with this resubmission.

- Section III, Line 5: Widths of streets, drives and sidewalks shown.
 Widths of sidewalks not shown.
 - Sidewalk details to be added.

RESPONSE: A waiver for the sidewalk requirement is included with this submission.

- Section III, Line 7: Size and location of all proposed and public utilities.
 Water supply information not provided.
 - *Add water supply information.*

RESPONSE: The location and size of all proposed and public utilities are shown on Sheet C6. This sheet contains the water supply information as well.

- Section III, Line 10, Drainage Calculations /Report
 - Drainage Calculations/Report not submitted.

• Waiver requested.

RESPONSE: A drainage report is included with this resubmission. We hereby withdraw this waiver request.

- Section III, Line 11: Circulation plan provided.
 - Circulation plan not provided.
 - *Provide circulation plan.*

RESPONSE: Circulation information, including pavement radii and arrows indicating direction of travel, is shown on Sheet C4.

- Section III, Line 12(a): Pavement and road profiles.
 - Information not provided for access road/driveway to rear barn.
 Provide specifications and location for access to rear barn (including wetlands crossings).
 - **RESPONSE:** The existing trail/driveway to be extended provides access to the barn. No wetland permit is needed and no change to driveway is proposed.
- Section III, Line 12(c): Curbing.
 - Information on curbing was not provided.
 - *Provide details on curbing.*

RESPONSE: A waiver for the requirement to provide curbing is included with this submission.



- Section III, Line 14: Solid Waste Disposal Plan
 - Solid waste disposal plan not provided.
 - *Add a note concerning solid waste disposal requirements.*

RESPONSE: Note 22 on Sheet C4 is stipulates solid waste disposal requirements.

- Section III, Line 25 Timetable for construction and completion of buildings, improvements, and landscaping.
 - *Timetable not provided.*
 - *Provide timetable for above.*

RESPONSE: A construction timeline is included with this response and on Sheet C4 of the plan set.

- Section III, Line 17 Location of any fire suppression system as required by the Fire Department.
 - No fire suppression information provided.
 - Add fire suppression system requirements per Fire Departments and regulations.

RESPONSE: Fire suppression systems are not required for duplexes.

- Section III, Line 19: All required State, Federal and Local permits, and permit numbers.
 Permits not provided.
 - Permits will be required to be submitted prior to final plat approval. RESPONSE: All state, federal and local permits will be obtained and noted on the plans prior to final plat approval.
- Section III, Line 22: SWPPP
 - SWPPP not provided.

• SWPPP will be required to be submitted prior to final plat approval. **RESPONSE: A SWPPP will be submitted prior to the start of construction.**

- Section III Line 23: Sight Distance Plan
 - Sight distance plan not submitted.
 - Driveway approval from NHDOT will be required to be submitted prior to final plat approval.

RESPONSE: See Sheet H1 – Highway Access Plan for sight distance profile. A NHDOT permit will be obtained prior to final plat approval.

Section IV, Line 3: Review letter by Fire Department
 Letter not provided.

• *Provide letter from Fire Department review.* **RESPONSE: A letter from the Fire Chief is pending.**

- Section IV, Line 3: Review letter by Police Department
 - *Letter not provided.*
 - *Provide letter from Police Department review.*

RESPONSE: We have received a review letter from the Police Chief and our response to his comment is below.



INGINEERS IN

- Section IV, Line 7: Drainage calculations and report.
 - Drainage calculations and report not provided.
 - Waiver requested.

RESPONSE: A drainage report is included with this resubmission. We hereby withdraw this waiver request.

- Section V: Engineering Review.
 - The plans and drawings are required to be reviewed by Stantec, the Town of Candia's engineering consultants, prior to the Public Hearing for the project.

RESPONSE: Responses to Stantec's comments are included above in this letter.

Police Chief Comment:

1. *The proposed driveway is askew from Donovan Road. I would like it to line up with Donovan Road.*

RESPONSE: The proposed driveway is aligned with Donovan Road. It is at a different angle so that Units 5-6 will be outside of the wetland buffer, but it will be a 4-way intersection regardless. The proposed access driveway is at an angle of 80° with respect to High Street where 75° is the Town minimum per Section 14.09 of the Subdivision Regulations.

Road Agent Comments:

 There should be a note on the plans to ensure that this access never becomes a townmaintained road or will ever be a responsibility of the town to maintain. RESPONSE: See Note #26 on Sheet C4.

Included with this response letter are the following:

- 1. Three (3) Full Size Plan Sets.
- 2. Architectural Plans (at end of plan set).
- 3. Email from Postmaster Sean Dooley.
- 4. Letters from Police Chief and Road Agent.
- 5. Waiver Request Letter.
- 6. Construction Schedule.
- 7. Two (2) Drainage Analysis.

Thank you very much for your time.

Very truly yours, YONES & BEACH ENGINEERS, INC. Joseph Coronati

Vice President

cc: Bob Carr (via email) Jason A. Bielagus, Esq. (via email) Bryan Ruoff, Stantec Consulting Services (via email)



Daniel Meditz

From:	Bob Carr <bob.carr22@comcast.net></bob.carr22@comcast.net>
Sent:	Wednesday, March 20, 2024 4:01 PM
Го:	Daniel Meditz
Subject:	Fwd: [EXTERNAL] 669 High Street

Message from the Postmaster

Begin forwarded message:

From: "Dooley, Sean - Candia, NH" <Sean.T.Dooley@usps.gov> Subject: RE: [EXTERNAL] 669 High Street Date: March 5, 2024 at 2:12:34 PM EST To: Bob Carr <bob.carr22@comcast.net>

Good afternoon Mr. Carr,

at some point someone from the e911 system will work with the fire chief and generate the addresses to match up with the 911 system. I would advise against calling it a new road. I would see them as be 669 High St. unit 1, 669 High St. unit 2, 669 High St. unit 3, 669 High St. unit 4, 669 High St. unit 5, and 669 High St. unit 6. The Post office will establish the actual delivery location as a valid address once 911 certifies its location and it's entered the e911 system.

If possible, I would like to see the deliveries on the left side of each delivery unit's driveway as indicated by the red dots on the map picture below.

If we were looking at the properties from the road it would be preferred the mailboxes be to the left of each driveway on their own post with a large mailbox for each unit. I put two read dots on the map to indicate where I think they should be placed. My carrier would make a left hand turn into the driveway from High ST deliver the boxes in reverse order from unit six to unit one and exit back onto High Street. If the driveway is paved, obviously clear in the winter, and the mailboxes are not blocked for any other reason, there should be no issue with them delivering to them in the driveway. Which is more appealing to your residents than having to cross the street I would imagen. I also included a photo of the new regulation mailboxes and where they can be purchased. Just throwing it out there if you need a good contractor for whatever, siding, decks, etc.. JJB construction his number is 6039966042.

If you have any other questions don't hesitate to reach out to me, best of luck with everything.





Candia Police Department

74 High Street Candia, New Hampshire 03034 Telephone (603) 483-2317 emergency (603) 483-2318 business Fax (603) 483-0253

Michael D. McGillen Chief of Police

March 5, 2024

Candia Planning Board Attn: Chairman Rudy Cartier 74 High Street Candia, NH 03034

Re: Multi-Family Development 669 High St. Tax Map 405, Lot 48

Dear Rudy:

I have reviewed the plans and visited the site at 669 High Street. It appears that the proper stopping distance 400' is available. From what I can see the proposed driveway is askew from Donovan Road. I would like for it to line-up with Donovan Road.

hi

Chief Michael McGillen



MAR 0 6 2024

Town of Candia Town Road Agent Jeffrey Wuebbolt Candia, New Hampshire 03034 (603) 483-8588

From: Candia Town Road Agent To: Rudy Cartier, Chairman of the planning Committee Subj: 669 High Street, Major Site Plan

I have reviewed the plans submitted for above project and my concerns are as follows:

1. There should be a note on the plans to ensure that this access never becomes a town-maintained road or will ever be a responsibility of the town to maintain.

Jeff Wuebbolt Candia Town Road Agent

CONSTRUCTION SCHEDULE MEMO 669 HIGH STREET

- Sept 1. All approvals for construction complete and Building Permits in hand.
- Oct 1. Erosion Controls installed. Begin Clearing trees for Units 1&2 and stripping loam
- Nov 1. Pour foundations for all three buildings Install drainage and underground utilities
- Dec 1. Begin Framing units Rough grade properties
- Jan 1. Continue framing
- Feb 1. Continue framing and begin interior fit ups
- March 1. Interior rough fit ups of all units continues Drill well
- April 1. Interior rough fits up cont.
 - Run well lines throughout Begin fine grading Complete rip rap Begin exterior finishes
- May 1. Install all three septic tanks Begin septic fields Begin interior finishes
- June1. Continue septic fields Continue interior finishes Continue exterior finishes 1st coat of paving throughout
- July 1. Septic systems complete Fine grading loam and seed Continue interior finishes Continue exterior finishes Build Decks for units 3-6 Pour patios for units 1 & 2
- August1. Unit 1&2 substantially complete Install trees and shrubs Erosion control for barn area installed Trees cleared and stumped
- Sep 1. C of O for unit 1 & 2 Continue interior and exterior finishes for units 3-6 Prep for foundatoin
- Oct. 1. C of O for units 3 & 4 Pour foundation walls to barn and back fill
- Nov. 1. C of O for units 5 & 6 Finish paving Dec. 1 Erect Pre-Engineered steel barn
- March 1. Pour floor to barn
 - Finish grade
- May1. Barn C of O



85 Portsmouth Avenue, PO Box 219, Stratham, NH 03885 603.772.4746 - JonesandBeach.com

March 21, 2024

Candia Planning Board Attn. Rudy Cartier 74 High Street Candia, NH 03034

RE: Waiver Request Letter 669 High Street Candia, NH Map 405, Lot 48 JBE Project No. 22201

Dear Mr. Cartier:

Jones & Beach Engineers, Inc. respectfully requests the following waivers for the proposed multi-family residential development on the above-referenced parcel on behalf of our client & owner, Bob Carr, Claudia Patricia Carr Rev Trust due to the unique characteristics of the subject property and the proposed use. We have consolidated all of the proposed waivers into this one letter for ease of review rather than having multiple separate letters. We have also removed the waiver for the drainage design as we are providing a report now.

Section II, Article 4.03.E – Plan Scale: The scale of the plan shall be at a minimum of oneinch equals twenty feet $(1^{"} = 20^{"})$, and the plan shall include a north arrow and the date.

We are asking for a waiver from this requirement because this site is 88 acres and most of that property is not being developed. Typically housing developments would be at a larger scale than 1"=20'. Since we are required to apply under the site plan regulations, those are more geared towards commercial sites and additions, which makes more sense for a more detailed site plan. Our plans are at 1"=50' and provide adequate detail for this spread out housing design.

Section II, Article 4.03.F – Boundary Survey: A survey of the perimeter boundaries of the proposed use subject to site plan review, including compass bearings, distances, and area in acres.

We are asking for a waiver from this requirement because the site is 88 acres and mostly undeveloped backland. The client also agreed to no further development as part of the ZBA approval to allow the multi-family housing development. The units are not being sold off individually and therefore we are not required to survey the entire lot per the condominium law. We have surveyed approximately 17.6 acres of boundary which is well past the proposed barn in the rear of the parcel and enough to prove out density. Because of these reasons, we feel that this is a reasonable request given the small size of this developed compared to overall parcel size.

Section II, Article 4.03.G – Topography Survey: Existing and proposed topography showing surface contours at intervals not in excess of 2-feet.

We are asking for a waiver from this requirement because the site is 88 acres and mostly undeveloped backland. The client also agreed to no further development as part of the ZBA approval to allow the multi-family housing development. We have provided detailed topography on the front 15 acres, which is well more than the area needed for this small development. Because of these reasons, we feel that this is a reasonable request given the small size of this developed compared to overall parcel size.

Section II, Article 4.03.I – Natural Features: The location of natural features such as rivers, streams, marshes, wetlands, and any man-made feature such as existing dams, roads, stone walls, and structures. The plan shall indicate those natural and man-made features which are to be removed, retained, or altered.

We are asking for a waiver from this requirement because the site is 88 acres and mostly undeveloped backland. The client also agreed to no further development as part of the ZBA approval to allow the multi-family housing development. We have provided detailed existing features for the front 15 acres, which is well more than the area needed for this small development. Because of these reasons, we feel that this is a reasonable request given the small size of this developed compared to overall parcel size.

Section II, Article 4.03.K – Sidewalk: Proposed streets, driveways, parking spaces and sidewalks, with indication of direction of travel and inside radii of all curves. The width of the traveled way of all streets, driveways and sidewalks, and the total number of all parking spaces shall be shown. Loading spaces, trash disposal facilities, and facilities used in connection with any structure on the site shall be shown.

We comply with most of this section but we are asking for a waiver from the sidewalk requirement because:

We are proposing a short shared private driveway, just over 300' in length, for six (6) dwelling units. The purpose of having sidewalks is to improve pedestrian safety on roadways with high traffic volume, so that pedestrians will not be walking in the travel lane. Traffic on the shared driveway will be minimal and does not warrant the need for sidewalks. There is no sidewalk along Route 27 to connect to and the residents will be able to walk along the driveway with no issues.

Section III, Article 8.03.A.2 – Truck Turning: Turning movements shall be provided for a WB-67 vehicle demonstrating that a delivery vehicle can access, maneuver and exit the site without impacting other motorists or pedestrians.

We believe that this requirement is intended for industrial and major commercial sites where deliveries via a large tractor trailer such as a WB-67 are anticipated. A WB-67 is specifically intended for deliveries of materials to warehouses or superstores, and it would have no business utilizing a shared access driveway between three duplexes. The largest vehicles anticipated to use the proposed shared access driveway are fire trucks and delivery box trucks similar to a SU-30. Turning movements for these two vehicles were run on Sheets T1 and T2 of the plan set.



Section III, Article 8.03.A.3 – Delivery Area: An area designated and striped for delivery vehicles (is required).

Again, this requirement seems like it is intended for industrial and commercial sites. The delivery vehicles will mostly like stop in the cul-de-sac near the driveway for the unit it is delivering to and walk to the front door. Residents exiting their driveways would be able to go the other direction away from the delivery vehicle on the cul-de-sac and therefore wouldn't pose any traffic congestion.

Section III, Article 8.03.D.3.D – Lighting Design: Parking lot and sidewalk lighting shall provide a minimum 0.2 horizontal foot candles with an average uniformity ratio of 4:1 and a minimum color ratio index of 50.

A parking lot is not proposed and neither are sidewalks. Lighting on the units is proposed above their garage doors and at front doors like most homes. We want to avoid having too many lights in this development and I believe that is the goal of the Town as well in a rural area like this one.

Section III, Article 8.03.I – Granite Curbing: Parking spaces shall be of adequate size and number in accordance with Candia's Zoning Ordinance, and shall be physically delineated by granite curbing so as to protect adjacent pedestrians.

We are providing three parking spaces per dwelling unit – two in the driveway and one in the garage. The parking requirement per zoning is only two spaces per dwelling unit and therefore we exceed the required number and a waiver is not required for the number or dimension of parking spaces. However, no curbing is being proposed anywhere for the use. The intent of curbing typically is twofold; to stop stormwater from leaving pavement where it is not intended to, and to physically demarcate paved areas. We are proposing to allow runoff to sheet flow off of the paved surface and into several culverts and swales toward a detention pond in the center of the cul de sac, then finally to the back of the site. Therefore, curbing is not necessary for drainage design purposes. Furthermore, curbing would be contrary to the intended character of the proposed multi-family residential use. We are intending to maintain a rural feel to the site in keeping with surrounding properties and the existing use of the subject parcel. There is no curbing on High Street or any surrounding sites along High Street to the best of our knowledge. Therefore, we have no need for curbing and feel that it would be detrimental to the intended character of the property.

Section III, Article 8.06.K – Culvert Pipe: Acceptable pipe material for roadway drainage systems and driveway culverts is: Reinforced Concrete Pipe (RCP).

RCP is typically only used for wetland crossings. ADS-N12 HDPE pipe is industry standard for culverts underneath driveways and roadways. Local contractors are more used to installing ADS-N12 HDPE pipes and these are more readily available for construction. ADS-N12 is rated for H20 loading at a depth of as little as 1 foot, and we are proposing at least 3 feet of cover in all paved areas. ADS-N12 HDPE pipe is a sufficient construction material for the intended use we are proposing.



Thank you very much for your consideration. If you have any questions, or need further assistance, please contact our office.

Very truly yours, JØNES & BEACH ENGINEERS, INC. Joseph Coronati Vice President



DRAINAGE ANALYSIS

SEDIMENT AND EROSION CONTROL PLAN

"Beaver Meadows" 669 High Street Candia, NH 03034 Tax Map 405, Lot 48

Prepared for:

Bob Carr 17 Vassar Street Manchester, NH 03104



Prepared by: Jones & Beach Engineers, Inc. 85 Portsmouth Avenue P.O. Box 219 Stratham, NH 03885 (603) 772-4746 March 22, 2024 JBE Project No. 22201

EXECUTIVE SUMMARY

Our client, Bob Carr proposes to remove the existing residential structures and driveway located at 669 High Street in Candia, NH, and construct 3 residential duplex buildings for a total of six new dwelling units, as well as an associated shared access driveway, on the same parcel. A drainage analysis of the entire site as well as offsite contributing watershed area was conducted for the purpose of estimating the peak rate of stormwater runoff and to subsequently design adequate drainage structures. Two models were compiled, one for the area in its existing (pre-construction) condition, and a second for its proposed (post-construction) condition. The analysis was conducted using data for the 2 Year – 24 Hour (2.90"), 10 Year – 24 Hour (4.34"), 25 Year – 24 Hour (5.47"), 50 Year – 24 Hour (6.51") and 100 Year – 24 Hour (7.77") storm events using the USDA SCS TR-20 method within the HydroCAD Stormwater Modeling System environment. This data was taken from the Extreme Precipitation Tables developed by the Northeast Regional Climate Center (NRCC). A summary of the existing and proposed conditions peak rates of runoff in units of cubic feet per second (cfs) is as follows:

Analysis Point	2 Year		10 Year		25 Year		50 Year		100 Year	
	Pre	Post	Pre	Post	Pre	Post	Pre	Post	Pre	Post
Analysis Point #1	2.20	2.12	5.29	5.21	8.04	7.98	10.71	10.64	14.08	14.08
Analysis Point #2	0.49	0.44	1.26	1.14	1.97	1.78	2.65	2.40	3.52	3.18
Analysis Point #3	0.05	0.05	0.32	0.30	0.64	0.59	0.98	0.90	1.45	1.37
Analysis Point #4	0.86	0.63	2.66	2.00	4.65	3.31	6.50	4.63	8.82	6.33
Analysis Point #5	0.00	0.00	1.58	1.56	3.29	3.28	4.73	4.72	6.32	6.32

The subject parcel is located in the Residential Zoning District. The subject parcel currently consists of the aforementioned residential structures and driveway which are proposed to be demolished. Despite impervious surface existing on the subject parcel now, the proposed development results in an increase in impervious surface on the subject parcel. The addition of the proposed impervious surfaces causes an increase in the curve number (C_n) and a decrease in the time of concentration (T_c), the net result being a potential increase in peak rates of runoff from the site. In order to mitigate this potential, a stormwater management system has been designed, consisting of a central detention pond as well as several culverts and stone drip edges. Due to the use of these stormwater management features, the peak flow will be reduced toward all analysis points during all analyzed storm events in the proposed condition.

The use of Best Management Practices per the NHDES <u>Stormwater Manual</u> have been applied to the design of this stormwater management system and will be observed during all stages of construction. All land disturbed during construction will be stabilized within thirty days of groundbreaking and abutting property owners will suffer minimal adversity resultant to this development.
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Appendix II Proposed Conditions Analysis

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- Appendix VII Stormwater Operations and Maintenance Manual
- Appendix VIII Pre- and Post-Construction Watershed Plans

Drainage Analysis and Erosion and Sediment Control Plan

1.0 RAINFALL CHARACTERISTICS

This drainage report includes an existing conditions analysis of the area involved in the proposed development, as well as a proposed condition, or post-construction analysis, of the same area. These analyses were accomplished using the USDA SCS TR-20 Method within the HydroCAD 10.20-3c Stormwater Modeling System. The curve numbers were developed using the SCS TR-55 Runoff Curve numbers for Urban Areas. A Type III SCS 24-hour rainfall distribution was utilized in analyzing the data for the 2 Year – 24 Hour (2.90"), 10 Year – 24 Hour (4.34"), 25 Year – 24 Hour (5.47"), 50 Year – 24 Hour (6.51") and 100 Year – 24 Hour (7.77") storm events. This data was taken from the Extreme Precipitation Tables developed by the Northeast Regional Climate Center (NRCC).

2.0 EXISTING CONDITIONS ANALYSIS

In the existing condition, the front area of the subject parcel consists of the aforementioned residential structures and driveway as well as a system of trails. Behind the existing single-family residential site, there are many acres of woods that comprise the remainder of the subject parcel.

The existing topography and roof ridges divide the subject parcel and offsite contributing watershed areas into 7 subcatchments, draining toward 5 analysis points. The majority of the front area of the subject parcel, modelled as Subcatchment 1S, draining overland toward Analysis Point 1. Analysis Point 1 represents a large wetland complex located approximately 200 feet behind the developed portion of the subject parcel.

Subcatchment 2S represents the area north of AP1 which drains toward this same analysis point. It is modelled separately because it has a different time of concentration path and weighted CN value, and is separated physically from 1S by the wetland complex.

Subcatchment 3S represents the area in the southwest corner of the subject parcel which drains westerly toward Analysis Point 2 Analysis Point 2 represents Tax Map 404, Lot 112.

Subcatchment 4S is wooded with an 8' wide dirt trail running through it. All runoff from 4S drains toward Analysis Point 3, which is a point along the wooded trail immediately east of the subcatchment boundary. This subcatchment and analysis point were included only due to the addition of the proposed barn and dirt trail leading to it in this area.

Subcatchment 5S is mostly sandwiched between 1S and 3S. This represents the land area that drains toward Analysis Point 4. Analysis Point 4 is another wetland complex to the north of the wetland complex that is represented as Analysis Point 1. The buffer associated with this wetland complex lies just to the east of the proposed barn.

There is an isolated wetland located in the front of the property at the corner of the existing gravel driveway and High Street. This isolated wetland consists of a shallow depression with a berm and therefore it is modelled as Pond 1P. The land area draining toward Pond 1P is modelled as Subcatchment 6S. Since this is a wetland, the seasonal high water table was assumed to be 6" below surface for the purposes of modelling infiltration of surface water to groundwater. Infiltration was modelled in the pond and any overflow over the berm follows a path through Subcatchment 5S, modelled as Reach 1R, to Analysis Point 4.

Finally, there is another existing depression on the eastern edge of the property modelled as 2P. The land area draining toward 2P is modelled as Subcatchment 7S. Since this is a wetland, the seasonal high water table was assumed to be 6" below surface for the purposes of modelling infiltration of surface water to groundwater. Infiltration was modelled in the pond and any overflow over the berm flows directly to Analysis Point 5, which represents an offsite discharge point immediately adjacent to Pond 2P.

Existing soil types were determined via NRCS Web Soil Survey. Four soil types exist in the study area: Scituate-Newfields Complex (Symbol 446A, Hydrologic Soil Group C), Scituate-Newfields Complex "very stony" (Symbol 447A, Hydrologic Soil Group C), Ridgebury fine sandy loam (Symbol 657B, Hydrologic Soil Group D), and Chatfield-Hollis-Canton complex (Symbol 140B, Hydrologic Soil Group B). All proposed infiltration practices are proposed in locations represented as 446A or 447A. According to "Ksat Values for New Hampshire Soils," Special Publication No. 5 sponsored by the Society of Soil Scientists of Northern New England (SSSNNE), Newfields and Scituate soils have identical saturated hydraulic conductivity ranges in the B horizon. The saturated hydraulic conductivity (Ksat) value for these soils ranges from 0.6 to 6.0 inches/hour within both the B horizon. Scituate has a Ksat range of 0.06-2.0 in/hr in the C horizon, but there is also Newfields soil in this complex and infiltration is proposed into the B horizon. B horizon Ksat estimates are typically more accurate in our experience. Therefore, in accordance with standard engineering practice, the lowest published Ksat of 0.6 in/hr in the B horizon for these soil types was divided by two in order to determine an appropriate Ksat of **0.3 in/hr** to use for design.

3.0 PROPOSED CONDITIONS ANALYSIS

The addition of the proposed impervious paved areas and buildings causes an increase in the curve number (C_n) and a decrease in the time of concentration (T_c) , the result being a potential increase in peak rates of runoff from the site. A stormwater management system was designed in order to mitigate this potential. The proposed development, consisting of the aforementioned six (6) dwelling units in three buildings with an associated shared access driveways and individual unit driveways as well as stormwater management features divide the subject parcel into 21 subcatchments. Subcatchments 1S-7S are functionally the same in the proposed condition as they were in the existing condition, although the areas have been changed. Pond 1P, representing an isolated wetland in the front of the subject parcel, flows overland through 1R but the difference now is that it is captured into a culvert modelled as 3R and routed into the stormwater management system which outlets toward Analysis Point 1.

There is no 8S due to a subcatchment numbering error on our end, but rather than renumbering the remainder of the subcatchments we will keep going. Subcatchment 9S represents an area consisting of woods, grass, pavement and roof that drains into a culvert modelled as Reach 3R. Reach 3R outlets into the primary detention pond for the site, modelled as 3P, located in the cul-de-sac center island. The detention pond has an outlet control structure and is designed to capture and slowly release runoff directed toward it. Discharge from Pond 3P outlets into Reach 4R, representing a swale between Units 4 and 5.

Subcatchment 10S represents a large section of the proposed cul de sac as well as some driveway and roof areas which drain directly into Pond 3P.

Subcatchment 11S represents a stretch of the proposed access driveway which drains through a shallow swale into a plunge pool. The swale is modelled as part of the Tc path for the subcatchment and the plunge pool is modelled as 24P. The plunge pool has a culvert outlet which drains into 3P.

Subcatchments 12S-22S represent roof areas which drain directly into stone drip edges adjacent to the building foundations for infiltration of roof runoff. The seasonal high water table depths per the test pits informed us of the proper SHWT elevations to use for design.

Through the design of this stormwater management system, peak flows are reduced toward all five analysis points during all analyzed storm events and all applicable requirements of the Candia Major Site Plan Regulations Section 8.06 are met except that a waiver is requested from 8.06.K to allow ADS-N12 HDPE drainage pipes instead of RCP as is typical for small residential developments.

5.0 CONCLUSION

This proposed site development will have minimal adverse effect on abutting infrastructures, properties, and downstream wetlands by way of stormwater runoff or siltation. Appropriate steps will be taken to eliminate erosion and sedimentation; these will be accomplished through the construction of a drainage system consisting of a detention pond, swales, and stone drip edges, and temporary erosion control measures including but not limited to silt fence and the use of a stabilized construction entrance. Best Management Practices developed by the State of New Hampshire have been utilized in the design of this system and their application will be enforced throughout the construction process. Peak rates of runoff from the site will be reduced toward all analysis points during all analyzed storm events.

This project disturbs less than 100,000 S.F. and does <u>not</u> require a NHDES Alteration of Terrain Permit.

Respectfully Submitted, JONES & BEACH ENGINEERS, INC.

Medite

Daniel Meditz, P.E Project Engineer

APPENDIX I

EXISTING CONDITIONS DRAINAGE ANALYSIS

Summary 2 YEAR Complete 10 YEAR Summary 25 YEAR Complete 50 YEAR Complete 100 YEAR



22201-EXISTING Prepared by Jones & Beach Engineers Inc HydroCAD® 10.20-3c s/n 00762 © 2023 HydroCAD Software Solutions LLC

Area Listing (all nodes)

CN	Description	
	(subcatchment-numbers)	
74	>75% Grass cover, Good, HSG C (1S, 3S, 5S, 6S, 7S)	
80	>75% Grass cover, Good, HSG D (1S, 7S)	
82	Dirt roads, HSG B (2S, 4S, 5S)	
87	Dirt roads, HSG C (5S)	
89	Dirt roads, HSG D (5S)	
96	Gravel surface, HSG C (1S, 6S)	
98	Paved parking, HSG C (1S, 5S, 6S, 7S)	
98	Roofs, HSG C (1S, 7S)	
55	Woods, Good, HSG B (2S, 4S, 5S)	
70	Woods, Good, HSG C (1S, 3S, 5S, 6S, 7S)	
77	Woods, Good, HSG D (1S, 2S, 5S, 7S)	
70	TOTAL AREA	
	CN 74 80 82 87 89 96 98 98 55 70 77 77 70	

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Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
2.296	HSG B	2S, 4S, 5S
7.742	HSG C	1S, 3S, 5S, 6S, 7S
1.911	HSG D	1S, 2S, 5S, 7S
0.000	Other	
11.949	1	TOTAL AREA

	alne	Printed 3/22/2024
HydroCAD® 10.20-3c s/n 00762 © 2023 Hy	droCAD Software Solutions LLC	Page 4
Time span=0.00 Runoff by SCS Reach routing by Dyn-Stor-	0-24.00 hrs, dt=0.05 hrs, 481 points x 3 TR-20 method, UH=SCS, Weighted-CN Ind method - Pond routing by Dyn-Stor-In	d method
Subcatchment1S: 1S	Runoff Area=122,795 sf 2.52% Impervio Flow Length=438' Tc=27.3 min CN=74 R	us Runoff Depth>0.84" unoff=1.52 cfs 0.197 af
Subcatchment2S: 2S	Runoff Area=66,616 sf 0.00% Impervio Flow Length=290' Tc=18.2 min CN=71 R	us Runoff Depth>0.70" unoff=0.76 cfs 0.089 af
Subcatchment3S: 3S Flow Length=140	Runoff Area=43,497 sf 0.00% Impervio D' Slope=0.0123 '/' Tc=19.1 min CN=71 R	us Runoff Depth>0.70" unoff=0.49 cfs 0.058 af
Subcatchment4S: 4S	Runoff Area=32,528 sf 0.00% Impervio Flow Length=271' Tc=25.6 min CN=57 R	us Runoff Depth>0.21" unoff=0.05 cfs 0.013 af
Subcatchment5S: 5S	Runoff Area=153,606 sf 0.42% Impervio Flow Length=881' Tc=40.0 min CN=67 R	us Runoff Depth>0.53" unoff=0.86 cfs 0.155 af
Subcatchment6S: 6S	Runoff Area=16,669 sf 8.30% Impervio Flow Length=122' Tc=11.6 min CN=76 R	us Runoff Depth>0.95" unoff=0.33 cfs 0.030 af
Subcatchment7S: 7S	Runoff Area=84,800 sf 2.58% Impervio Flow Length=456' Tc=23.1 min CN=73 R	us Runoff Depth>0.79" unoff=1.04 cfs 0.128 af
Reach 1R: Flow Through 5S n=0.030 L=	Avg. Flow Depth=0.00' Max Vel=0.00 fps I =881.0' S=0.0254 '/' Capacity=37.95 cfs Ou	nflow=0.00 cfs 0.000 af utflow=0.00 cfs 0.000 af
Reach AP1: Analysis Point 1	O	Inflow=2.20 cfs 0.286 af utflow=2.20 cfs 0.286 af
Reach AP2: Analysis Point 2	O	Inflow=0.49 cfs 0.058 af utflow=0.49 cfs 0.058 af
Reach AP3: Analysis Point 3	O	Inflow=0.05 cfs 0.013 af utflow=0.05 cfs 0.013 af
Reach AP4: Analysis Point 4	O	Inflow=0.86 cfs 0.155 af utflow=0.86 cfs 0.155 af
Reach AP5: Analysis Point 5	O	Inflow=0.00 cfs 0.000 af utflow=0.00 cfs 0.000 af
Pond 1P: Isolated Wetland Discarded=0.02	Peak Elev=196.22' Storage=745 cf I cfs 0.018 af Primary=0.00 cfs 0.000 af Ou	nflow=0.33 cfs 0.030 af utflow=0.02 cfs 0.018 af
Pond 2P: Depression in Woods Discarded=0.09	Peak Elev=176.38' Storage=3,094 cf I cfs 0.078 af Primary=0.00 cfs 0.000 af Ou	nflow=1.04 cfs 0.128 af itflow=0.09 cfs 0.078 af

Total Runoff Area = 11.949 acRunoff Volume = 0.672 afAverage Runoff Depth = 0.67"98.60% Pervious = 11.781 ac1.40% Impervious = 0.168 ac

22201-EXISTING Prepared by Jones & Beach Engineers I HydroCAD® 10.20-3c s/n 00762 © 2023 Hydro	Type III 24-hr 10-YR 24HR Rainfall=4.34" nc Printed 3/22/2024 CAD Software Solutions LLC Page 5
Time span=0.00-2 Runoff by SCS TF Reach routing by Dyn-Stor-Inc	4.00 hrs, dt=0.05 hrs, 481 points x 3 -20 method, UH=SCS, Weighted-CN method - Pond routing by Dyn-Stor-Ind method
Subcatchment1S: 1S	Runoff Area=122,795 sf 2.52% Impervious Runoff Depth>1.84" low Length=438' Tc=27.3 min CN=74 Runoff=3.54 cfs 0.432 af
Subcatchment2S: 2S	Runoff Area=66,616 sf 0.00% Impervious Runoff Depth>1.62" low Length=290' Tc=18.2 min CN=71 Runoff=1.98 cfs 0.207 af
Subcatchment3S: 3S Flow Length=140'	Runoff Area=43,497 sf 0.00% Impervious Runoff Depth>1.62" Slope=0.0123 '/' Tc=19.1 min CN=71 Runoff=1.26 cfs 0.135 af
Subcatchment4S: 4S	Runoff Area=32,528 sf 0.00% Impervious Runoff Depth>0.77" low Length=271' Tc=25.6 min CN=57 Runoff=0.32 cfs 0.048 af
Subcatchment5S: 5S	Runoff Area=153,606 sf 0.42% Impervious Runoff Depth>1.34" low Length=881' Tc=40.0 min CN=67 Runoff=2.59 cfs 0.395 af
Subcatchment6S: 6S	Runoff Area=16,669 sf 8.30% Impervious Runoff Depth>2.00" low Length=122' Tc=11.6 min CN=76 Runoff=0.74 cfs 0.064 af
Subcatchment7S: 7S	Runoff Area=84,800 sf 2.58% Impervious Runoff Depth>1.77" low Length=456' Tc=23.1 min CN=73 Runoff=2.51 cfs 0.287 af
Reach 1R: Flow Through 5S A n=0.030 L=8	vg. Flow Depth=0.03' Max Vel=0.60 fps Inflow=0.40 cfs 0.014 af 1.0' S=0.0254 '/' Capacity=37.95 cfs Outflow=0.10 cfs 0.014 af
Reach AP1: Analysis Point 1	Inflow=5.29 cfs 0.639 af Outflow=5.29 cfs 0.639 af
Reach AP2: Analysis Point 2	Inflow=1.26 cfs 0.135 af Outflow=1.26 cfs 0.135 af
Reach AP3: Analysis Point 3	Inflow=0.32 cfs 0.048 af Outflow=0.32 cfs 0.048 af
Reach AP4: Analysis Point 4	Inflow=2.66 cfs 0.409 af Outflow=2.66 cfs 0.409 af
Reach AP5: Analysis Point 5	Inflow=1.58 cfs 0.128 af Outflow=1.58 cfs 0.128 af
Pond 1P: Isolated Wetland Discarded=0.03 ct	Peak Elev=196.44' Storage=1,191 cf Inflow=0.74 cfs 0.064 af s 0.029 af Primary=0.40 cfs 0.014 af Outflow=0.43 cfs 0.043 af
Pond 2P: Depression in Woods Discarded=0.10 cf	Peak Elev=176.50' Storage=3,960 cf Inflow=2.51 cfs 0.287 af 0.091 af Primary=1.58 cfs 0.128 af Outflow=1.68 cfs 0.219 af

Total Runoff Area = 11.949 acRunoff Volume = 1.567 afAverage Runoff Depth = 1.57"98.60% Pervious = 11.781 ac1.40% Impervious = 0.168 ac

22201-EXISTING	Type III 24-hr	10-YR 24HR Rail	nfall=4.34'
Prepared by Jones & Beach Engineers Inc		Printed	3/22/2024
HydroCAD® 10.20-3c s/n 00762 © 2023 HydroCAD Software So	olutions LLC		Page 6

Summary for Subcatchment 1S: 1S

Runoff = 3.54 cfs @ 12.40 hrs, Volume= Routed to Reach AP1 : Analysis Point 1 0.432 af, Depth> 1.84"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR 24HR Rainfall=4.34"

A	rea (sf)	CN	Description					
	2,882	98	Roofs, HSC	G C				
	210	98	98 Paved parking, HSG C					
	1,737	96	Gravel surfa	ace, HSG (
	58,443	70	Woods, Go	od, HSG C				
	35,755	74	>75% Gras	s cover, Go	bod, HSG C			
	23,726	77	Woods, Go	od, HSG D				
	42	80	>75% Gras	s cover, Go	ood, HSG D			
1	22,795	74	Weighted A	verage				
1	19,703		97.48% Pei	rvious Area				
	3,092		2.52% Impe	ervious Are	а			
Tc	Length	Slope	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)				
22.6	100	0.0200	0.07		Sheet Flow,			
					Woods: Light underbrush n= 0.400 P2= 2.90"			
0.4	18	0.0186	6 0.68		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
2.1	147	0.0544	1.17		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
0.5	45	0.0889	9 1.49		Shallow Concentrated Flow,			
	400				Woodland Kv= 5.0 fps			
1.4	103	0.0583	3 1.21		Shallow Concentrated Flow,			
0.0	05	0 0 0 0 0			Woodland Kv= 5.0 fps			
0.3	25	0.0800) 1.41		Shallow Concentrated Flow,			
					vvoodiand KV= 5.0 tps			
27.3	438	Fotal						

Summary for Subcatchment 2S: 2S

Runoff = 1.98 cfs @ 12.27 hrs, Volume= 0.207 af Routed to Reach AP1 : Analysis Point 1

0.207 af, Depth> 1.62"

Area (sf)	CN	Description
1,242	82	Dirt roads, HSG B
19,472	55	Woods, Good, HSG B
45,902	77	Woods, Good, HSG D
66,616 66,616	71	Weighted Average 100.00% Pervious Area

1	22201-l	EXISTIN	١G			Type III 24-hr 10-YR 24HR Rainfall=4.34
	Prepare	d by Jon	ies & Be	ach Engir	neers Inc	Printed 3/22/2024
ļ	HydroCA	D® 10.20	-3c s/n 00)762 © 202	23 HydroCA	D Software Solutions LLC Page 7
_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	12.3	82	0.0610	0.11		Sheet Flow,
	2.9	18	0.1111	0.10		Woods: Light underbrush n= 0.400 P2= 2.90" Sheet Flow,
	0.2	21	0.1111	1.67		Woods: Light underbrush n= 0.400 P2= 2.90" Shallow Concentrated Flow,
	0.4	30	0.0571	1.19		Woodland Kv= 5.0 fps Shallow Concentrated Flow,
	2.4	139	0.0367	0.96		Woodland KV= 5.0 fps Shallow Concentrated Flow, Woodland Kv= 5.0 fps
-	10.0		- ()			•

18.2 290 Total

Summary for Subcatchment 3S: 3S

1.26 cfs @ 12.28 hrs, Volume= Runoff = Routed to Reach AP2 : Analysis Point 2

0.135 af, Depth> 1.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR 24HR Rainfall=4.34"

A	rea (sf)	CN E	Description					
	33,751	70 V	70 Woods, Good, HSG C					
	9,746	74 >	75% Gras	s cover, Go	ood, HSG C			
	43,497	71 V	Veighted A	verage				
	43,497	1	00.00% Pe	ervious Are	а			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
10.6	81	0.0123	0.13		Sheet Flow,			
					Grass: Short n= 0.150 P2= 2.90"			
7.3	19	0.0123	0.04		Sheet Flow,			
					Woods: Light underbrush n= 0.400 P2= 2.90"			
1.2	40	0.0123	0.55		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
19.1	140	Total						

Summary for Subcatchment 4S: 4S

0.32 cfs @ 12.45 hrs, Volume= 0.048 af, Depth> 0.77" Runoff = Routed to Reach AP3 : Analysis Point 3

22201-EXISTING	
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Type III 24-hr 10-YR 24HR Rainfall=4.34" Printed 3/22/2024

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Α	rea (sf)	CN D	escription		
	1,810	82 D	irt roads, l	HSG B	
	30,718	55 V	Voods, Go	od, HSG B	
	32,528	57 V	Veighted A	verage	
	32,528	1	00.00% Pe	ervious Are	a
_					
Tc	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
5.3	30	0.0667	0.09		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
17.3	80	0.0250	0.08		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
2.8	113	0.0177	0.67		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.2	48	0.0625	4.03		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
25.6	271	Total			

Summary for Subcatchment 5S: 5S

Runoff = 2.59 cfs @ 12.60 hrs, Volume= 0.395 af, Depth> 1.34" Routed to Reach AP4 : Analysis Point 4

Area (sf)	CN	Description
2,174	82	Dirt roads, HSG B
44,614	55	Woods, Good, HSG B
649	98	Paved parking, HSG C
5,767	87	Dirt roads, HSG C
16,547	74	>75% Grass cover, Good, HSG C
80,332	70	Woods, Good, HSG C
817	89	Dirt roads, HSG D
2,706	77	Woods, Good, HSG D
153,606	67	Weighted Average
152,957		99.58% Pervious Area
649		0.42% Impervious Area
649		0.42% Impervious Area

Type III 24-hr 10-YR 24HR Rainfall=4.34" Printed 3/22/2024 re Solutions LLC Page 9

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Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
25.3	100	0.0150	0.07		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
2.7	100	0.0150	0.61		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
1.4	70	0.0286	0.85		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
1.0	176	0.0341	2.97		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
0.1	32	0.0625	4.03		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
0.4	29	0.0690	1.31		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
1.4	69	0.0290	0.85		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.6	39	0.0513	1.13		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.4	75	0.0333	2.94		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
6.7	191	0.0089	0.47		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
		— · ·			

40.0 881 Total

Summary for Subcatchment 6S: 6S

Runoff = 0.74 cfs @ 12.17 hrs, Volume= Routed to Pond 1P : Isolated Wetland 0.064 af, Depth> 2.00"

Area (sf)	CN	Description
1,383	98	Paved parking, HSG C
1,344	96	Gravel surface, HSG C
8,543	74	>75% Grass cover, Good, HSG C
5,399	70	Woods, Good, HSG C
16,669	76	Weighted Average
15,286		91.70% Pervious Area
1,383		8.30% Impervious Area

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(m	Tc in)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
10).7	76	0.0105	0.12		Sheet Flow,			
						Grass: Short n= 0.150 P2= 2.90"			
().3	11	0.0100	0.64		Sheet Flow,			
						Smooth surfaces n= 0.011 P2= 2.90"			
().2	13	0.0400	1.40		Shallow Concentrated Flow,			
				4.00		Short Grass Pasture Kv= 7.0 fps			
().4	22	0.0400	1.00		Shallow Concentrated Flow,			
						vvoodiand Kv = 5.0 lps			

Type III 24-hr 10-YR 24HR Rainfall=4.34"

11.6 122 Total

Summary for Subcatchment 7S: 7S

Runoff	=	2.51 cfs @) 12.34 hrs,	Volume=	0.287 af,	Depth> 1.77"
Routed	to Pond	2P : Depr	ession in Woo	ods		

Area (st) CN	Description
36	5 98	Roofs, HSG C
1,82	3 98	Paved parking, HSG C
38,38	0 70	Woods, Good, HSG C
34,17	9 74	>75% Grass cover, Good, HSG C
9,80	6 77	Woods, Good, HSG D
24	7 80	>75% Grass cover, Good, HSG D
84,80	0 73	Weighted Average
82,61	2	97.42% Pervious Area
2,18	8	2.58% Impervious Area

Type III 24-hr 10-YR 24HR Rainfall=4.34"Printed 3/22/2024olutions LLCPage 11

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Length	Slope	Velocity	Capacity	Description
(feet)	(ft/ft)	(ft/sec)	(cfs)	
13	0.0200	0.87		Sheet Flow,
				Smooth surfaces n= 0.011 P2= 2.90"
20	0.1200	0.24		Sheet Flow,
				Grass: Short n= 0.150 P2= 2.90"
39	0.0513	0.09		Sheet Flow,
				Woods: Light underbrush n= 0.400 P2= 2.90"
28	0.0260	0.06		Sheet Flow,
				Woods: Light underbrush n= 0.400 P2= 2.90"
127	0.0260	0.81		Shallow Concentrated Flow,
				Woodland Kv= 5.0 fps
75	0.1067	1.63		Shallow Concentrated Flow,
				Woodland Kv= 5.0 fps
56	0.0357	0.94		Shallow Concentrated Flow,
				Woodland Kv= 5.0 fps
22	0.0909	1.51		Shallow Concentrated Flow,
				Woodland Kv= 5.0 fps
76	0.0125	0.56		Shallow Concentrated Flow,
				Woodland Kv= 5.0 fps
	Length (feet) 13 20 39 28 127 75 56 22 76	Length (feet) Slope (ft/ft) 13 0.0200 20 0.1200 39 0.0513 28 0.0260 127 0.0260 75 0.1067 56 0.0357 22 0.0909 76 0.0125	Length (feet)Slope (ft/ft)Velocity (ft/sec)130.02000.87200.12000.24390.05130.09280.02600.061270.02600.81750.10671.63560.03570.94220.09091.51760.01250.56	Length (feet)Slope (ft/ft)Velocity (ft/sec)Capacity (cfs)130.02000.87200.12000.24390.05130.09280.02600.061270.02600.81750.10671.63560.03570.94220.09091.51760.01250.56

23.1 456 Total

Summary for Reach 1R: Flow Through 5S

[80] Warning: Exceeded Pond 1P by 0.10' @ 23.95 hrs (0.00 cfs 0.019 af)

Inflow Area = 0.383 ac, 8.30% Impervious, Inflow Depth = 0.43" for 10-YR 24HR event Inflow = 0.40 cfs @ 12.50 hrs, Volume= 0.014 af Outflow = 0.10 cfs @ 12.84 hrs, Volume= 0.014 af, Atten= 76%, Lag= 20.0 min Routed to Reach AP4 : Analysis Point 4

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 0.60 fps, Min. Travel Time= 24.3 min Avg. Velocity = 0.27 fps, Avg. Travel Time= 53.6 min

Peak Storage= 139 cf @ 12.84 hrs Average Depth at Peak Storage= 0.03', Surface Width= 7.52' Bank-Full Depth= 0.50' Flow Area= 10.0 sf, Capacity= 37.95 cfs

30.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight Length= 881.0' Slope= 0.0254 '/' Inlet Invert= 196.40', Outlet Invert= 174.00'

‡

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Summary for Reach AP1: Analysis Point 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	4.348 ac,	1.63% Impervious,	Inflow Depth > 1.	76" for 10-YR 24HR event
Inflow	=	5.29 cfs @	12.35 hrs, Volume	= 0.639 af	
Outflow	=	5.29 cfs @	12.35 hrs, Volume	= 0.639 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow A	Area	=	0.999 ac,	0.00% Impervious,	Inflow Depth >	1.62"	for 10-YR 24HR event
Inflow	=	=	1.26 cfs @	12.28 hrs, Volume	= 0.135 a	af	
Outflow	v =	=	1.26 cfs @	12.28 hrs, Volume	= 0.135 a	af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow Ar	ea =	0.747 ac,	0.00% Impervious,	Inflow Depth > 0.7	77" for 10-YR 24HR event
Inflow	=	0.32 cfs @	12.45 hrs, Volume	= 0.048 af	
Outflow	=	0.32 cfs @	12.45 hrs, Volume	= 0.048 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Analysis Point 4

[40] Hint: Not Described (Outflow=Inflow)

Inflow A	rea =	3.909 ac,	1.19% Impervious, I	Inflow Depth > 1.2	26" for 10-YR 24HR event
Inflow	=	2.66 cfs @	12.62 hrs, Volume=	= 0.409 af	
Outflow	=	2.66 cfs @	12.62 hrs, Volume=	= 0.409 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP5: Analysis Point 5

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	a =	1.947 ac,	2.58% Impervious,	Inflow Depth = 0.7	79" for 10-YR 24HR event
Inflow	=	1.58 cfs @	12.61 hrs, Volume	= 0.128 af	
Outflow	=	1.58 cfs @	12.61 hrs, Volume	= 0.128 af,	Atten= 0%, Lag= 0.0 min

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Pond 1P: Isolated Wetland

[93] Warning: Storage range exceeded by 0.03'

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=40)

Inflow Area	ı =	0.383 ac,	8.30% Imp	ervious,	Inflow Dept	th >	2.00"	for 1	10-YF	R 24HR	event
Inflow	=	0.74 cfs @	12.17 hrs,	Volume	= 0	.064 a	af				
Outflow	=	0.43 cfs @	12.50 hrs,	Volume	= 0	.043 a	af, Att	en= 4′	1%, I	Lag= 20).2 min
Discarded	=	0.03 cfs @	12.50 hrs,	Volume	= 0	.029 a	af				
Primary	=	0.40 cfs @	12.50 hrs,	Volume	= 0	.014 a	af				
Routed	to Reac	h 1R : Flow	Through 5S								

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 196.44' @ 12.50 hrs Surf.Area= 2,828 sf Storage= 1,191 cf

Plug-Flow detention time= 240.8 min calculated for 0.043 af (67% of inflow) Center-of-Mass det. time= 138.2 min (981.2 - 843.0)

Volume	Inve	ert Avai	I.Storage	Storage Description				
#1	195.3	0'	1,191 cf	Custom Stage D	ata (Irregular) List	ed below (Recalc)		
Elevatio	n	Surf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area		
(fee	et)	(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)		
195.3	30	235	72.0	0	0	235		
196.0)0	1,050	148.0	416	416	1,568		
196.4	10	2,828	211.0	747	1,163	3,369		
196.4	1	2,828	211.0	28	1,191	3,371		
Device	Routing	In	vert Outle	et Devices				
#1	Primary	196	6.40' 20.0	20.0' long x 6.0' breadth Broad-Crested Rectangular Weir				
			2 50			1.20 1.40 1.00 1.00	J 2.00	
			Coe	f (English) 2.37 2	251 270 268 2	68 2 67 2 65 2 65	2 65	
			2.65	2.66 2.66 2.67	2.69 2.72 2.76 2	.83	2.00	
#2	Discarde	d 195	.30' 0.30	0 in/hr Exfiltratio	n over Surface ar	ea		
			Con	ductivity to Ground	water Elevation =	194.80' Phase-In=	= 0.10'	

Discarded OutFlow Max=0.03 cfs @ 12.50 hrs HW=196.44' (Free Discharge) **2=Exfiltration** (Controls 0.03 cfs)

Primary OutFlow Max=0.38 cfs @ 12.50 hrs HW=196.44' TW=196.41' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir** (Weir Controls 0.38 cfs @ 0.45 fps)

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Summary for Pond 2P: Depression in Woods

Inflow Area	ı =	1.947 ac,	2.58% Impe	ervious,	Inflow D	epth >	1.77"	for '	10-Y	R 24H	R event
Inflow	=	2.51 cfs @	12.34 hrs,	Volume	=	0.287	af				
Outflow	=	1.68 cfs @	12.61 hrs,	Volume	=	0.219	af, At	ten= 33	3%,	Lag= 1	16.5 min
Discarded	=	0.10 cfs @	12.61 hrs,	Volume	=	0.091	af				
Primary	=	1.58 cfs @	12.61 hrs,	Volume	=	0.128	af				
Routed to Reach AP5 : Analysis Point 5											

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 176.50' @ 12.61 hrs Surf.Area= 7,514 sf Storage= 3,960 cf

Plug-Flow detention time= 152.4 min calculated for 0.218 af (76% of inflow) Center-of-Mass det. time= 66.7 min (926.8 - 860.1)

Volume	Invert	Avail.Sto	rage	Storage Description		
#1	175.70'	5,4	71 cf	Custom Stage Data	(Irregular)Listed	below (Recalc)
Elevatio	on Su	urf.Area F	Perim. (feet)	Inc.Store	Cum.Store	Wet.Area
175.7 176.0 176.4 176.7	70 10 10 70	2,764 3,841 7,514 7,514	204.0 265.0 341.0 341.0	0 986 2,230 2,254	0 986 3,217 5,471	2,764 5,042 8,709 8,811
Device	Routing	Invert	Outle	t Devices		
#1	Primary	176.40'	20.0' Head 2.50 Coef. 2.85	long x 2.0' breadth (feet) 0.20 0.40 0.6 3.00 3.50 (English) 2.54 2.61 3.07 3.20 3.32	Broad-Crested F 50 0.80 1.00 1.2 2.61 2.60 2.66	Rectangular Weir 0 1.40 1.60 1.80 2.00 2.70 2.77 2.89 2.88
#2	Discarded	175.70'	0.300 Cond) in/hr Exfiltration ov luctivity to Groundwat	ver Surface area ter Elevation = 175	5.20' Phase-In= 0.10'
Discard	ed OutFlow	/ Max=0.10 c	fs @ 12	2.61 hrs HW=176.50'	(Free Discharge	e)

1-2=Exfiltration (Controls 0.10 cfs)

Primary OutFlow Max=1.57 cfs @ 12.61 hrs HW=176.50' TW=0.00' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir**(Weir Controls 1.57 cfs @ 0.80 fps)

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Time span=0.00-24.00 hrs, dt=0 Runoff by SCS TR-20 method, U Reach routing by Dyn-Stor-Ind method - Po	.05 hrs, 481 points x 3 H=SCS, Weighted-CN nd routing by Dyn-Stor-Ind method
Subcatchment1S: 1SRunoff Area=1Flow Length=438	22,795 sf 2.52% Impervious Runoff Depth>2.73" 3' Tc=27.3 min CN=74 Runoff=5.32 cfs 0.641 af
Subcatchment2S: 2SRunoff Area=Flow Length=290	66,616 sf 0.00% Impervious Runoff Depth>2.47" ' Tc=18.2 min CN=71 Runoff=3.07 cfs 0.315 af
Subcatchment3S: 3S Runoff Area= Flow Length=140' Slope=0.0123 '/	43,497 sf 0.00% Impervious Runoff Depth>2.47" " Tc=19.1 min CN=71 Runoff=1.97 cfs 0.205 af
Subcatchment4S: 4SRunoff Area=Flow Length=271	32,528 sf 0.00% Impervious Runoff Depth>1.35" ' Tc=25.6 min CN=57 Runoff=0.64 cfs 0.084 af
Subcatchment5S: 5SRunoff Area=1Flow Length=881	53,606 sf 0.42% Impervious Runoff Depth>2.12" ' Tc=40.0 min CN=67 Runoff=4.23 cfs 0.622 af
Subcatchment6S: 6SRunoff Area=Flow Length=122	16,669 sf 8.30% Impervious Runoff Depth>2.92" 2' Tc=11.6 min CN=76 Runoff=1.08 cfs 0.093 af
Subcatchment7S: 7SRunoff Area=Flow Length=456	84,800 sf 2.58% Impervious Runoff Depth>2.64" 6' Tc=23.1 min CN=73 Runoff=3.81 cfs 0.429 af
Reach 1R: Flow Through 5S Avg. Flow Depth= n=0.030 L=881.0' S=0.0254	=0.06' Max Vel=0.96 fps Inflow=1.67 cfs 0.039 af '/' Capacity=37.95 cfs Outflow=0.44 cfs 0.039 af
Reach AP1: Analysis Point 1	Inflow=8.04 cfs 0.956 af Outflow=8.04 cfs 0.956 af
Reach AP2: Analysis Point 2	Inflow=1.97 cfs 0.205 af Outflow=1.97 cfs 0.205 af
Reach AP3: Analysis Point 3	Inflow=0.64 cfs 0.084 af Outflow=0.64 cfs 0.084 af
Reach AP4: Analysis Point 4	Inflow=4.65 cfs 0.661 af Outflow=4.65 cfs 0.661 af
Reach AP5: Analysis Point 5	Inflow=3.29 cfs 0.260 af Outflow=3.29 cfs 0.260 af
Pond 1P: Isolated Wetland Peak Elev=1 Discarded=0.03 cfs 0.031 af Prir	96.51' Storage=1,191 cf Inflow=1.08 cfs 0.093 af nary=1.67 cfs 0.039 af Outflow=1.70 cfs 0.070 af
Pond 2P: Depression in Woods Peak Elev=1 Discarded=0.10 cfs 0.096 af Prir	76.56' Storage=4,427 cf Inflow=3.81 cfs 0.429 af nary=3.29 cfs 0.260 af Outflow=3.39 cfs 0.355 af
Total Runoff Area = 11.949 ac Runoff Ve	olume = 2.389 af Average Runoff Depth = 2.4

Area = 11.949 ac Runoff Volume = 2.389 af Average Runoff Depth = 2.40" 98.60% Pervious = 11.781 ac 1.40% Impervious = 0.168 ac

22201-EXISTING	Type III 24-hr 50	-YR 24HR Rainfall=6.51"
HydroCAD® 10.20-3c s/n 00762 © 202	Ieers Inc 23 HydroCAD Software Solutions LLC	Printed 3/22/2024 Page 16
Time span Runoff by S Reach routing by Dyn-S	=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3 SCS TR-20 method, UH=SCS, Weighted-CN Stor-Ind method - Pond routing by Dyn-Sto	s N Ir-Ind method
Subcatchment1S: 1S	Runoff Area=122,795 sf 2.52% Impe Flow Length=438' Tc=27.3 min CN=74	rvious Runoff Depth>3.60" I Runoff=7.04 cfs 0.845 af
Subcatchment2S: 2S	Runoff Area=66,616 sf 0.00% Impe Flow Length=290' Tc=18.2 min CN=71	rvious Runoff Depth>3.30" Runoff=4.14 cfs 0.421 af
Subcatchment3S: 3S Flow Length	Runoff Area=43,497 sf 0.00% Impe =140' Slope=0.0123 '/' Tc=19.1 min CN=71	rvious Runoff Depth>3.30" Runoff=2.65 cfs 0.275 af
Subcatchment4S: 4S	Runoff Area=32,528 sf 0.00% Impe Flow Length=271' Tc=25.6 min CN=57	rvious Runoff Depth>1.98" ′ Runoff=0.98 cfs 0.123 af
Subcatchment5S: 5S	Runoff Area=153,606 sf 0.42% Impe Flow Length=881' Tc=40.0 min CN=67	rvious Runoff Depth>2.89" 7 Runoff=5.87 cfs 0.850 af
Subcatchment6S: 6S	Runoff Area=16,669 sf 8.30% Impe Flow Length=122' Tc=11.6 min CN=76	rvious Runoff Depth>3.82" 8 Runoff=1.42 cfs 0.122 af
Subcatchment7S: 7S	Runoff Area=84,800 sf 2.58% Impe Flow Length=456' Tc=23.1 min CN=73	rvious Runoff Depth>3.50" 3 Runoff=5.08 cfs 0.568 af
Reach 1R: Flow Through 5S n=0.03	Avg. Flow Depth=0.09' Max Vel=1.17 fp 0 L=881.0' S=0.0254 '/' Capacity=37.95 cfs	os Inflow=2.29 cfs 0.065 af Outflow=0.83 cfs 0.065 af
Reach AP1: Analysis Point 1		Inflow=10.71 cfs 1.266 af Outflow=10.71 cfs 1.266 af
Reach AP2: Analysis Point 2		Inflow=2.65 cfs 0.275 af Outflow=2.65 cfs 0.275 af
Reach AP3: Analysis Point 3		Inflow=0.98 cfs 0.123 af Outflow=0.98 cfs 0.123 af
Reach AP4: Analysis Point 4		Inflow=6.50 cfs 0.915 af Outflow=6.50 cfs 0.915 af
Reach AP5: Analysis Point 5		Inflow=4.73 cfs 0.394 af Outflow=4.73 cfs 0.394 af
Pond 1P: Isolated Wetland Discarded=	Peak Elev=196.54' Storage=1,191 o =0.03 cfs 0.032 af Primary=2.29 cfs 0.065 af	cf Inflow=1.42 cfs 0.122 af Outflow=2.32 cfs 0.096 af
Pond 2P: Depression in Woods Discarded=	Peak Elev=176.61' Storage=4,758 (=0.11 cfs 0.099 af Primary=4.73 cfs 0.394 af	cf Inflow=5.08 cfs 0.568 af Outflow=4.83 cfs 0.493 af

Total Runoff Area = 11.949 acRunoff Volume = 3.204 afAverage Runoff Depth = 3.22"98.60% Pervious = 11.781 ac1.40% Impervious = 0.168 ac

22201-EXISTING Prepared by Jones & Beach Engineer <u>HydroCAD® 10.20-3c s/n 00762 © 2023 Hy</u>	<i>Type III 24-hr 100-YF</i> s Inc ydroCAD Software Solutions LLC	R 24HR Rainfall=7.77" Printed 3/22/2024 Page 17
Time span=0.0 Runoff by SCS Reach routing by Dyn-Stor-	00-24.00 hrs, dt=0.05 hrs, 481 points x 3 TR-20 method, UH=SCS, Weighted-CN -Ind method - Pond routing by Dyn-Stor-In	nd method
Subcatchment1S: 1S	Runoff Area=122,795 sf 2.52% Impervio Flow Length=438' Tc=27.3 min CN=74 R	us Runoff Depth>4.70" Runoff=9.17 cfs 1.103 af
Subcatchment2S: 2S	Runoff Area=66,616 sf 0.00% Impervio Flow Length=290' Tc=18.2 min CN=71 R	us Runoff Depth>4.37" Runoff=5.49 cfs 0.556 af
Subcatchment3S: 3S Flow Length=14	Runoff Area=43,497 sf 0.00% Impervio 0' Slope=0.0123 '/' Tc=19.1 min CN=71 R	us Runoff Depth>4.36" Runoff=3.52 cfs 0.363 af
Subcatchment4S: 4S	Runoff Area=32,528 sf 0.00% Impervio Flow Length=271' Tc=25.6 min CN=57 R	us Runoff Depth>2.82" Runoff=1.45 cfs 0.176 af
Subcatchment5S: 5S	Runoff Area=153,606 sf 0.42% Impervio Flow Length=881' Tc=40.0 min CN=67 R	us Runoff Depth>3.90" Runoff=7.97 cfs 1.145 af
Subcatchment6S: 6S	Runoff Area=16,669 sf 8.30% Impervio Flow Length=122' Tc=11.6 min CN=76 R	us Runoff Depth>4.94" Runoff=1.83 cfs 0.158 af
Subcatchment7S: 7S	Runoff Area=84,800 sf 2.58% Impervio Flow Length=456' Tc=23.1 min CN=73 R	us Runoff Depth>4.59" Runoff=6.66 cfs 0.744 af
Reach 1R: Flow Through 5S n=0.030 L	Avg. Flow Depth=0.10' Max Vel=1.34 fps =881.0' S=0.0254 '/' Capacity=37.95 cfs Ou	Inflow=1.90 cfs 0.098 af utflow=1.27 cfs 0.098 af
Reach AP1: Analysis Point 1	lr Ou	nflow=14.08 cfs 1.660 af tflow=14.08 cfs 1.660 af
Reach AP2: Analysis Point 2	0	Inflow=3.52 cfs 0.363 af utflow=3.52 cfs 0.363 af
Reach AP3: Analysis Point 3	0	Inflow=1.45 cfs 0.176 af utflow=1.45 cfs 0.176 af
Reach AP4: Analysis Point 4	Ο	Inflow=8.82 cfs 1.243 af utflow=8.82 cfs 1.243 af
Reach AP5: Analysis Point 5	Ο	Inflow=6.32 cfs 0.565 af utflow=6.32 cfs 0.565 af
Pond 1P: Isolated Wetland Discarded=0.03	Peak Elev=196.54' Storage=1,191 cf 3 cfs 0.033 af Primary=1.90 cfs 0.098 af Ou	Inflow=1.83 cfs 0.158 af utflow=1.93 cfs 0.131 af
Pond 2P: Depression in Woods Discarded=0.1	Peak Elev=176.65' Storage=5,082 cf 1 cfs 0.104 af Primary=6.32 cfs 0.565 af Ou	Inflow=6.66 cfs 0.744 af utflow=6.43 cfs 0.669 af

Total Runoff Area = 11.949 acRunoff Volume = 4.245 afAverage Runoff Depth = 4.26"98.60% Pervious = 11.781 ac1.40% Impervious = 0.168 ac

22201-EXISTING	Type III 24-hr	50-YR 24HR Rail	nfall=6.51"
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Summary for Subcatchment 1S: 1S

7.04 cfs @ 12.38 hrs, Volume= Runoff = Routed to Reach AP1 : Analysis Point 1

0.845 af, Depth> 3.60"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YR 24HR Rainfall=6.51"

_	A	rea (sf)	CN	Description		
		2,882	98	Roofs, HSC	G C	
		210	98	Paved park	ing, HSG C)
		1,737	96	Gravel surfa	ace, HSG C	
		58,443	70	Woods, Go	od, HSG C	
		35,755	74	>75% Gras	s cover, Go	ood, HSG C
		23,726	77	Woods, Go	od, HSG D	
		42	80	>75% Gras	s cover, Go	ood, HSG D
	1	22,795	74	Weighted A	verage	
	1	19,703		97.48% Pei	rvious Area	
		3,092		2.52% Impe	ervious Area	а
	_				a 14	– 1 <i>– 1</i>
	IC	Length	Slop	e Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft	(ft/sec)	(CfS)	
	22.6	100	0.020	0 0.07		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 2.90"
	0.4	18	0.018	6 0.68		Shallow Concentrated Flow,
	.					Woodland Kv= 5.0 fps
	2.1	147	0.054	4 1.17		Shallow Concentrated Flow,
	0 5	45	0.000	o 4.40		Woodland Kv= 5.0 fps
	0.5	45	0.088	9 1.49		Shallow Concentrated Flow,
	4 4	100	0.050	0 4 0 4		Woodland KV= 5.0 fps
	1.4	103	0.058	3 1.21		Shallow Concentrated Flow,
	0.2	25	0 000	0 1 1 1		Shallow Concentrated Flow
	0.3	20	0.000	0 1.41		Woodland Ky= 5.0 fps
_	07.0	400	Tatal			
	// 5	438	inal			

27.3 438 l otal

Summary for Subcatchment 2S: 2S

4.14 cfs @ 12.26 hrs, Volume= Runoff = Routed to Reach AP1 : Analysis Point 1

0.421 af, Depth> 3.30"

Area (sf)	CN	Description
1,242	82	Dirt roads, HSG B
19,472	55	Woods, Good, HSG B
45,902	77	Woods, Good, HSG D
66,616 66,616	71	Weighted Average 100.00% Pervious Area

22201- Prepare <u>HydroCA</u>	EXISTIN d by Jon D® 10.20-	NG nes & Be -3c_s/n 00	ach Engir 1762 © 202	neers Inc 23 HydroCAI	Type III 24-hr 50-YR 24HR Rainfall=6.51" Printed 3/22/2024 D Software Solutions LLC Page 19
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.3	82	0.0610	0.11		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
2.9	18	0.1111	0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
0.2	21	0.1111	1.67		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.4	30	0.0571	1.19		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
2.4	139	0.0367	0.96		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps

18.2 290 Total

Summary for Subcatchment 3S: 3S

Runoff	=	2.65 cfs @	12.27 hrs,	Volume=					
Routed to Reach AP2 : Analysis Point 2									

0.275 af, Depth> 3.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YR 24HR Rainfall=6.51"

A	rea (sf)	CN E	Description		
	33,751	70 V	Voods, Go	od, HSG C	
	9,746	74 >	75% Gras	s cover, Go	ood, HSG C
	43,497	71 V	Veighted A	verage	
	43,497	1	00.00% Pe	ervious Are	a
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.6	81	0.0123	0.13		Sheet Flow,
					Grass: Short n= 0.150 P2= 2.90"
7.3	19	0.0123	0.04		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
1.2	40	0.0123	0.55		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
19.1	140	Total			

Summary for Subcatchment 4S: 4S

Runoff = 0.98 cfs @ 12.39 hrs, Volume= 0.123 af, Depth> 1.98" Routed to Reach AP3 : Analysis Point 3

Prepare	Printed 3/22/2024					
HydroCA	Page 20					
A	rea (sf)	CN E	Description			
	1,810	82 E	Dirt roads, I	HSG B		
	30,718	55 V	Voods, Go	od, HSG B		
	32,528 32,528	57 V 1	Veighted A 00.00% Pe	verage ervious Are	a	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
5.3	30	0.0667	0.09		Sheet Flow,	
17.3	80	0.0250	0.08		Woods: Light underbrush n= 0.400 P: Sheet Flow, Woods: Light underbrush n= 0.400 P:	2= 2.90"
2.8	113	0.0177	0.67		Shallow Concentrated Flow, Woodland Ky= 5.0 fps	2-2.90
0.2	48	0.0625	4.03		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps	
25.6	271	Total				

Type III 24-hr 50-YR 24HR Rainfall=6.51"

Summary for Subcatchment 5S: 5S

Runoff = 5.87 cfs @ 12.57 hrs, Volume= 0.850 af, Depth> 2.89" Routed to Reach AP4 : Analysis Point 4

Area (sf)	CN	Description
2,174	82	Dirt roads, HSG B
44,614	55	Woods, Good, HSG B
649	98	Paved parking, HSG C
5,767	87	Dirt roads, HSG C
16,547	74	>75% Grass cover, Good, HSG C
80,332	70	Woods, Good, HSG C
817	89	Dirt roads, HSG D
2,706	77	Woods, Good, HSG D
153,606	67	Weighted Average
152,957		99.58% Pervious Area
649		0.42% Impervious Area

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Tc (min)	Length	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
25.2	100	0.0150	0.07	(010)	Shoot Flow	
20.0	100	0.0150	0.07		Woods: Light underbrush n= 0.400	P2= 2.90"
2.7	100	0.0150	0.61		Shallow Concentrated Flow, Woodland Kv= 5.0 fps	
1.4	70	0.0286	0.85		Shallow Concentrated Flow, Woodland Ky= 5.0 fps	
1.0	176	0.0341	2.97		Shallow Concentrated Flow,	
0.1	32	0.0625	4.03		Shallow Concentrated Flow,	
0.4	29	0.0690	1.31		Unpaved Kv= 16.1 fps Shallow Concentrated Flow,	
1.4	69	0.0290	0.85		Woodland Kv= 5.0 fps Shallow Concentrated Flow,	
0.6	39	0 0513	1 13		Woodland Kv= 5.0 fps Shallow Concentrated Flow	
0.0		0.0010	0.04		Woodland Kv= 5.0 fps	
0.4	75	0.0333	2.94		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps	
6.7	191	0.0089	0.47		Shallow Concentrated Flow, Woodland Ky= 5.0 fps	

40.0 881 Total

Summary for Subcatchment 6S: 6S

Runoff = 1.42 cfs @ 12.16 hrs, Volume= Routed to Pond 1P : Isolated Wetland 0.122 af, Depth> 3.82"

Type III 24-hr 50-YR 24HR Rainfall=6.51"

Area (sf)	CN	Description
1,383	98	Paved parking, HSG C
1,344	96	Gravel surface, HSG C
8,543	74	>75% Grass cover, Good, HSG C
5,399	70	Woods, Good, HSG C
16,669	76	Weighted Average
15,286		91.70% Pervious Area
1,383		8.30% Impervious Area

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Tc (min)	Length	Slope	Velocity	Capacity	Description				
10.7	76	0.0105	0.10	(013)	Shoot Flow				
10.7	70	0.0105	0.12		Grass: Short $n=0.150$ P2= 2.90"				
0.3	11	0.0100	0.64		Sheet Flow,				
					Smooth surfaces n= 0.011 P2= 2.90"				
0.2	13	0.0400	1.40		Shallow Concentrated Flow,				
					Short Grass Pasture Kv= 7.0 fps				
0.4	22	0.0400	1.00		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				

Type III 24-hr 50-YR 24HR Rainfall=6.51"

11.6 122 Total

Summary for Subcatchment 7S: 7S

Runoff	=	5.08 cfs @	12.32 hrs,	Volume=	0.568 af,	Depth>	3.50"
Routed	to Pond	2P : Depress	sion in Woo	ods			

Area	a (sf)	CN	Description
	365	98	Roofs, HSG C
1	,823	98	Paved parking, HSG C
38	3,380	70	Woods, Good, HSG C
34	,179	74	>75% Grass cover, Good, HSG C
9	,806	77	Woods, Good, HSG D
	247	80	>75% Grass cover, Good, HSG D
84	,800	73	Weighted Average
82	2,612		97.42% Pervious Area
2	2,188		2.58% Impervious Area

Type III 24-hr 50-YR 24HR Rainfall=6.51"Printed 3/22/2024Solutions LLCPage 23

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Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.2	13	0.0200	0.87		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 2.90"
1.4	20	0.1200	0.24		Sheet Flow,
					Grass: Short n= 0.150 P2= 2.90"
7.3	39	0.0513	0.09		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
7.3	28	0.0260	0.06		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
2.6	127	0.0260	0.81		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.8	75	0.1067	1.63		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
1.0	56	0.0357	0.94		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.2	22	0.0909	1.51		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
2.3	76	0.0125	0.56		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps

23.1 456 Total

Summary for Reach 1R: Flow Through 5S

[80] Warning: Exceeded Pond 1P by 0.08' @ 12.40 hrs (1.18 cfs 0.047 af)

Inflow Are	a =	0.383 ac,	8.30% Impervious,	Inflow Depth =	2.03	" for 50-Y	R 24HR event
Inflow	=	2.29 cfs @	12.15 hrs, Volume	= 0.065	af		
Outflow	=	0.83 cfs @	12.38 hrs, Volume	= 0.065	af, A	tten= 64%,	Lag= 14.0 min
Routed	d to Rea	ach AP4 : Ana	lysis Point 4				

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 1.17 fps, Min. Travel Time= 12.6 min Avg. Velocity = 0.39 fps, Avg. Travel Time= 37.8 min

Peak Storage= 622 cf @ 12.38 hrs Average Depth at Peak Storage= 0.09', Surface Width= 12.40' Bank-Full Depth= 0.50' Flow Area= 10.0 sf, Capacity= 37.95 cfs

30.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight Length= 881.0' Slope= 0.0254 '/' Inlet Invert= 196.40', Outlet Invert= 174.00'

‡

22201-EXISTING	Type III 24-hr	50-YR 24HR Rainfall=6.51"
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Summary for Reach AP1: Analysis Point 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	a =	4.348 ac,	1.63% Impervious,	Inflow Depth > 3	3.49" for	50-YR 24HR event
Inflow	=	10.71 cfs @	12.33 hrs, Volume	= 1.266 a	af	
Outflow	=	10.71 cfs @	12.33 hrs, Volume	= 1.266 a	af, Atten=	0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow A	rea =	0.999 ac,	0.00% Impervious,	Inflow Depth > 3	3.30" for	50-YR 24HR event
Inflow	=	2.65 cfs @	12.27 hrs, Volume	= 0.275 a	af	
Outflow	=	2.65 cfs @	12.27 hrs, Volume	= 0.275 a	af, Atten=	0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow A	rea =	0.747 ac,	0.00% Impervious,	Inflow Depth > 1.	98" for 50-YR 24HR event
Inflow	=	0.98 cfs @	12.39 hrs, Volume	= 0.123 af	
Outflow	=	0.98 cfs @	12.39 hrs, Volume	= 0.123 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Analysis Point 4

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	ea =	3.909 ac,	1.19% Impervious,	Inflow Depth > 2.	81" for 50-YR 24HR event
Inflow	=	6.50 cfs @	12.55 hrs, Volume	= 0.915 af	
Outflow	=	6.50 cfs @	12.55 hrs, Volume	= 0.915 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP5: Analysis Point 5

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	ea =	1.947 ac,	2.58% Impervious,	Inflow Depth > 2.	43" for 50-YR 24HR event
Inflow	=	4.73 cfs @	12.40 hrs, Volume	= 0.394 af	
Outflow	=	4.73 cfs @	12.40 hrs, Volume	= 0.394 af,	Atten= 0%, Lag= 0.0 min

22201-EXISTING	Type III 24-hr 50-YR 24HR Rainfall=6.51"
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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Pond 1P: Isolated Wetland

[93] Warning: Storage range exceeded by 0.13'

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=57)

Inflow Area	=	0.383 ac,	8.30% Impe	rvious,	Inflow	Depth >	3.82'	' for 5	0-YR 24H	R event
Inflow	=	1.42 cfs @	12.16 hrs, \	Volume	=	0.122	af			
Outflow	=	2.32 cfs @	12.15 hrs, \	Volume	=	0.096	af, A	tten= 0%	6, Lag= 0.	0 min
Discarded	=	0.03 cfs @	12.25 hrs, \	Volume	=	0.032	af			
Primary	=	2.29 cfs @	12.15 hrs, \	Volume	=	0.065	af			
Routed	to Reac	h 1R : Flow	Through 5S							

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 196.54' @ 12.25 hrs Surf.Area= 2,828 sf Storage= 1,191 cf

Plug-Flow detention time= 127.8 min calculated for 0.096 af (79% of inflow) Center-of-Mass det. time= 49.9 min (874.3 - 824.4)

Volume	Inver	t Avail.S	Storage	Storage Description	n				
#1	195.30	' 1	,191 cf	Custom Stage Dat	ta (Irregular) Listed	below (Recalc)			
Elevatio (fee	on S et)	urf.Area (sɑ-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sg-ft)			
195.3 196.0 196.4 196.4	30 20 40 41	235 1,050 2,828 2,828	72.0 148.0 211.0 211.0	0 416 747 28	0 416 1,163 1,191	235 1,568 3,369 3,371			
Device	Routing	Inve	ert Outle	et Devices					
#1	Primary	196.4	0' 20.0 Head 2.50 Coet 2.65	' long x 6.0' bread d (feet) 0.20 0.40 (3.00 3.50 4.00 4. f. (English) 2.37 2.5 2.66 2.66 2.67 2.	th Broad-Crested 0.60 0.80 1.00 1.2 50 5.00 5.50 51 2.70 2.68 2.68 69 2.72 2.76 2.83	Rectangular Weir 20 1.40 1.60 1.80 2.0 2.67 2.65 2.65 2.65 3	00		
#2	Discarded	195.3	0' 0.30 Con	0 in/hr Exfiltration ductivity to Groundw	over Surface area vater Elevation = 19	4.80' Phase-In= 0.10	0'		
Discard	Discarded OutFlow Max=0.03 cfs @ 12.25 hrs HW=196.54' (Free Discharge)								

2=Exfiltration (Controls 0.03 cfs)

Primary OutFlow Max=2.26 cfs @ 12.15 hrs HW=196.54' TW=196.45' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir** (Weir Controls 2.26 cfs @ 0.82 fps)

22201-EXISTING	Type III 24-hr	50-YR 24HR Rail	nfall=6.51"
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Summary for Pond 2P: Depression in Woods

Inflow An Inflow Outflow Discarde Primary Route	rea = 5 = 5 ed = 6 = 2 ed to Reach	1.947 ac, 2 5.08 cfs @ 4.83 cfs @ 0.11 cfs @ 4.73 cfs @ 1 AP5 : Analy	2.58% In 12.32 hr 12.40 hr 12.40 hr 12.40 hr 12.40 hr vsis Poin	npervious, Inflow D s, Volume= s, Volume= s, Volume= s, Volume= t 5	epth > 3.50" for 0.568 af 0.493 af, Atten= 5 0.099 af 0.394 af	50-YR 24HR event 5%, Lag= 4.6 min				
Routing Peak Ele	Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 176.61' @ 12.40 hrs Surf.Area= 7,514 sf Storage= 4,758 cf									
Plug-Flo Center-c	w detention of-Mass det.	time= 87.3 r time= 30.2 r	nin calcı min (870	ulated for 0.492 af ().7 - 840.5)	87% of inflow)					
Volume	Invert	: Avail.St	orage	Storage Description	า					
#1	175.70	5,4	471 cf	Custom Stage Dat	ta (Irregular)Listed	below (Recalc)				
Elevatio	on S	urf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area				
(fee	et)	(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)				
175.7	0	2,764	204.0	0	0	2,764				
176.0	00	3,841	265.0	986	986	5,042				
176.4	10	7,514	341.0	2,230	3,217	8,709				
176.7	0	7,514	341.0	2,254	5,471	8,811				
Device	Routing	Inver	t Outle	t Devices						
#1	Primary	176.40	20.0' Head 2.50 Coef. 2.85	long x 2.0' breads (feet) 0.20 0.40 (3.00 3.50 (English) 2.54 2.6 3.07 3.20 3.32	th Broad-Crested F 0.60 0.80 1.00 1.2 01 2.61 2.60 2.66	Rectangular Weir 0 1.40 1.60 1.80 2.00 2.70 2.77 2.89 2.88				
#2	Discarded	175.70	Cond	uctivity to Groundw	over Surface area ater Elevation = 175	5.20' Phase-In= 0.10'				
Discarded OutFlow Max=0.11 cfs @ 12.40 hrs HW=176.61' (Free Discharge) 1 −2=Exfiltration (Controls 0.11 cfs)										

Primary OutFlow Max=4.73 cfs @ 12.40 hrs HW=176.61' TW=0.00' (Dynamic Tailwater) ☐ 1=Broad-Crested Rectangular Weir (Weir Controls 4.73 cfs @ 1.15 fps)

22201-EXISTING	Type III 24-hr	100-YR 24HR Rail	nfall=7.77"
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Summary for Subcatchment 1S: 1S

Runoff = 9.17 cfs @ 12.38 hrs, Volume= Routed to Reach AP1 : Analysis Point 1 1.103 af, Depth> 4.70"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR 24HR Rainfall=7.77"

A	rea (sf)	CN	Description		
	2,882	98 Roofs, HSG C			
	210	98	Paved park	ing, HSG C	
	1,737	96	Gravel surfa	ace, HSG (
	58,443	70	Woods, Go	od, HSG C	
	35,755	74	>75% Gras	s cover, Go	bod, HSG C
	23,726	77	Woods, Go	od, HSG D	
	42	80	>75% Gras	s cover, Go	ood, HSG D
1	22,795	74	Weighted A	verage	
1	19,703		97.48% Pei	rvious Area	
	3,092		2.52% Impe	ervious Are	а
Tc	Length	Slope	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	
22.6	100	0.0200	0.07		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
0.4	18	0.0186	6 0.68		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
2.1	147	0.0544	1.17		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.5	45	0.0889	9 1.49		Shallow Concentrated Flow,
	400				Woodland Kv= 5.0 fps
1.4	103	0.0583	3 1.21		Shallow Concentrated Flow,
	05	0 0 0 0 0			Woodland Kv= 5.0 fps
0.3	25	0.0800) 1.41		Shallow Concentrated Flow,
					vvoodiand KV= 5.0 tps
27.3	438	Fotal			

Summary for Subcatchment 2S: 2S

Runoff = 5.49 cfs @ 12.25 hrs, Volume= 0.556 Routed to Reach AP1 : Analysis Point 1

0.556 af, Depth> 4.37"

Area (st	f) CN	Description	
1,24	2 82	Dirt roads, HSG B	
19,47	2 55	Woods, Good, HSG B	
45,90	2 77	Woods, Good, HSG D	
66,61	6 71	Weighted Average	
66,61	6	100.00% Pervious Area	

22201-EXISTING	Type III 24-hr	100-YR 24HR Rainfall=7.77"
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		-

IC	Length	Siope	velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
12.3	82	0.0610	0.11		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
2.9	18	0.1111	0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
0.2	21	0.1111	1.67		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.4	30	0.0571	1.19		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
2.4	139	0.0367	0.96		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps

18.2 290 Total

Summary for Subcatchment 3S: 3S

Runoff = 3.52 cfs @ 12.26 hrs, Volume= Routed to Reach AP2 : Analysis Point 2 0.363 af, Depth> 4.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR 24HR Rainfall=7.77"

A	rea (sf)	CN I	Description					
	33,751	70	70 Woods, Good, HSG C					
	9,746	74 :	>75% Gras	s cover, Go	bod, HSG C			
	43,497	71	Weighted A	verage				
	43,497		100.00% Pe	ervious Are	a			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
10.6	81	0.0123	0.13		Sheet Flow,			
					Grass: Short n= 0.150 P2= 2.90"			
7.3	19	0.0123	0.04		Sheet Flow,			
					Woods: Light underbrush n= 0.400 P2= 2.90"			
1.2	40	0.0123	0.55		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
19.1	140	Total						

Summary for Subcatchment 4S: 4S

Runoff = 1.45 cfs @ 12.38 hrs, Volume= 0.176 af, Depth> 2.82" Routed to Reach AP3 : Analysis Point 3

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A	rea (sf)	CN E	Description				
	1,810	82 E	Dirt roads, I	HSG B			
	30,718	55 V	Voods, Go	od, HSG B			
	32,528	57 V	Veighted A	verage			
	32,528	1	00.00% Pe	ervious Are	a		
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
5.3	30	0.0667	0.09		Sheet Flow,		
					Woods: Light underbrush n= 0.400 P2= 2.90"		
17.3	80	0.0250	0.08		Sheet Flow,		
					Woods: Light underbrush n= 0.400 P2= 2.90"		
2.8	113	0.0177	0.67		Shallow Concentrated Flow,		
					Woodland Kv= 5.0 fps		
0.2	48	0.0625	4.03		Shallow Concentrated Flow,		
					Unpaved Kv= 16.1 fps		
25.6	271	Total					

Type III 24-hr 100-YR 24HR Rainfall=7.77"

Summary for Subcatchment 5S: 5S

Runoff = 7.97 cfs @ 12.56 hrs, Volume= 1.145 af, Depth> 3.90" Routed to Reach AP4 : Analysis Point 4

Area (sf)	CN	Description
2,174	82	Dirt roads, HSG B
44,614	55	Woods, Good, HSG B
649	98	Paved parking, HSG C
5,767	87	Dirt roads, HSG C
16,547	74	>75% Grass cover, Good, HSG C
80,332	70	Woods, Good, HSG C
817	89	Dirt roads, HSG D
2,706	77	Woods, Good, HSG D
153,606	67	Weighted Average
152,957		99.58% Pervious Area
649		0.42% Impervious Area

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HydroCA	D® 10.20-	-3c_s/n 00	0762 © 202	3 HydroCAI	D Software Solutions LLC Page 30		
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
25.3	100	0.0150	0.07		Sheet Flow,		
2.7	100	0.0150	0.61		Woods: Light underbrush n= 0.400 P2= 2.90" Shallow Concentrated Flow, Woodland Kv= 5.0 fps		
1.4	70	0.0286	0.85		Shallow Concentrated Flow,		
					Woodland Kv= 5.0 fps		
1.0	176	0.0341	2.97		Shallow Concentrated Flow,		
0.4	20	0.0005	4.00		Unpaved Kv= 16.1 fps		
0.1	32	0.0625	4.03		Shallow Concentrated Flow,		
0.4	29	0.0690	1.31		Shallow Concentrated Flow, Woodland Ky= 5.0 fps		
1.4	69	0.0290	0.85		Shallow Concentrated Flow,		
					Woodland Kv= 5.0 fps		
0.6	39	0.0513	1.13		Shallow Concentrated Flow,		
					Woodland Kv= 5.0 fps		
0.4	75	0.0333	2.94		Shallow Concentrated Flow,		
6.7	191	0.0089	0.47		Shallow Concentrated Flow, Woodland Kv= 5.0 fps		

40.0 881 Total

Summary for Subcatchment 6S: 6S

Runoff = 1.83 cfs @ 12.16 hrs, Volume= Routed to Pond 1P : Isolated Wetland 0.158 af, Depth> 4.94"

Type III 24-hr 100-YR 24HR Rainfall=7.77"

Area (sf)	CN	Description
1,383	98	Paved parking, HSG C
1,344	96	Gravel surface, HSG C
8,543	74	>75% Grass cover, Good, HSG C
5,399	70	Woods, Good, HSG C
16,669	76	Weighted Average
15,286		91.70% Pervious Area
1,383		8.30% Impervious Area

22201-	EXISTIN	۱G			Type III 24-hr 100-YR 24HR Rainfall=7.77
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τ.	1	01		O and it a	Description
IC	Length	Siope	velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.7	76	0.0105	0.12		Sheet Flow,
					Grass: Short n= 0.150 P2= 2.90"
0.3	11	0.0100	0.64		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 2.90"
0.2	13	0.0400	1.40		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.4	22	0.0400	1.00		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps

11.6 122 Total

Summary for Subcatchment 7S: 7S

Runoff	=	6.66 cfs @	12.32 hrs,	Volume=	0.744 af,	Depth> 4	4.59"
Routed	l to Pond	2P : Depres	sion in Woc	ods			

Area	a (sf)	CN	Description
	365	98	Roofs, HSG C
1	,823	98	Paved parking, HSG C
38	3,380	70	Woods, Good, HSG C
34	,179	74	>75% Grass cover, Good, HSG C
9	,806	77	Woods, Good, HSG D
	247	80	>75% Grass cover, Good, HSG D
84	,800	73	Weighted Average
82	2,612		97.42% Pervious Area
2	2,188		2.58% Impervious Area
22201-EXISTING

Type III 24-hr 100-YR 24HR Rainfall=7.77" Printed 3/22/2024 Solutions LLC Page 32

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Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.2	13	0.0200	0.87		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 2.90"
1.4	20	0.1200	0.24		Sheet Flow,
					Grass: Short n= 0.150 P2= 2.90"
7.3	39	0.0513	0.09		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
7.3	28	0.0260	0.06		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
2.6	127	0.0260	0.81		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.8	75	0.1067	1.63		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
1.0	56	0.0357	0.94		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.2	22	0.0909	1.51		Shallow Concentrated Flow,
• •					Woodland Kv= 5.0 fps
2.3	76	0.0125	0.56		Shallow Concentrated Flow,
					Woodland Kv= 5.0 tps

23.1 456 Total

Summary for Reach 1R: Flow Through 5S

[80] Warning: Exceeded Pond 1P by 0.04' @ 13.15 hrs (0.48 cfs 0.044 af)

Inflow Area = 0.383 ac, 8.30% Impervious, Inflow Depth = 3.07" for 100-YR 24HR event Inflow = 1.90 cfs @ 12.19 hrs, Volume= 0.098 af Outflow = 1.27 cfs @ 12.29 hrs, Volume= 0.098 af, Atten= 33%, Lag= 6.2 min Routed to Reach AP4 : Analysis Point 4

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 1.34 fps, Min. Travel Time= 11.0 min Avg. Velocity = 0.45 fps, Avg. Travel Time= 32.7 min

Peak Storage= 840 cf @ 12.29 hrs Average Depth at Peak Storage= 0.10', Surface Width= 13.71' Bank-Full Depth= 0.50' Flow Area= 10.0 sf, Capacity= 37.95 cfs

30.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight Length= 881.0' Slope= 0.0254 '/' Inlet Invert= 196.40', Outlet Invert= 174.00'

‡

22201-EXISTING	Type III 24-hr	100-YR 24HR Rainfall=7.77"
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Summary for Reach AP1: Analysis Point 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	a =	4.348 ac,	1.63% Impervious, I	nflow Depth > 4.58	" for 100-YR 24HR event
Inflow	=	14.08 cfs @	12.32 hrs, Volume=	1.660 af	
Outflow	=	14.08 cfs @	12.32 hrs, Volume=	: 1.660 af, A	tten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow A	Area =	0.999 ac,	0.00% Impervious,	Inflow Depth >	4.36"	for 100-YR 24HR event
Inflow	=	3.52 cfs @	12.26 hrs, Volume	= 0.363	af	
Outflow	/ =	3.52 cfs @	12.26 hrs, Volume	= 0.363	af, Att	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow Ar	ea =	0.747 ac,	0.00% Impervious,	Inflow Depth > 2.	82" for 100	-YR 24HR event
Inflow	=	1.45 cfs @	12.38 hrs, Volume	= 0.176 af		
Outflow	=	1.45 cfs @	12.38 hrs, Volume	= 0.176 af,	Atten= 0%,	Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Analysis Point 4

[40] Hint: Not Described (Outflow=Inflow)

Inflow A	rea =	3.909 ac,	1.19% Impervious,	Inflow Depth > 3.82	2" for 100-YR 24HR event
Inflow	=	8.82 cfs @	12.53 hrs, Volume=	= 1.243 af	
Outflow	=	8.82 cfs @	12.53 hrs, Volume=	= 1.243 af, <i>i</i>	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP5: Analysis Point 5

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	1.947 ac,	2.58% Impervious, Inf	flow Depth > 3.48"	for 100-YR 24HR event
Inflow	=	6.32 cfs @	12.38 hrs, Volume=	0.565 af	
Outflow	=	6.32 cfs @	12.38 hrs, Volume=	0.565 af, Atte	en= 0%, Lag= 0.0 min

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Pond 1P: Isolated Wetland

[93] Warning: Storage range exceeded by 0.13'

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=77)

Inflow Area =	=	0.383 ac,	8.30% Imp	ervious,	Inflow	Depth >	4.94	" for 10	00-YR 24	HR event
Inflow =	:	1.83 cfs @	12.16 hrs,	Volume	=	0.158	af			
Outflow =	:	1.93 cfs @	12.19 hrs,	Volume	=	0.131	af, A	tten= 0%	, Lag= 1	1.8 min
Discarded =	:	0.03 cfs @	12.20 hrs,	Volume	=	0.033	af			
Primary =	:	1.90 cfs @	12.19 hrs,	Volume	=	0.098	af			
Routed to	Reacl	n 1R : Flow	Through 5S							

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 196.54' @ 12.20 hrs Surf.Area= 2,828 sf Storage= 1,191 cf

Plug-Flow detention time= 102.9 min calculated for 0.131 af (83% of inflow) Center-of-Mass det. time= 35.3 min (852.4 - 817.1)

Volume	Inve	rt Avai	I.Storage	Storage Descript	ion				
#1	195.3	0'	1,191 cf	Custom Stage Data (Irregular)Listed below (Recalc)					
Elevatior (feet	n :	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)			
195.30 196.00 196.40 196.4	0 0 0 1	235 1,050 2,828 2,828	72.0 148.0 211.0 211.0	0 416 747 28	0 416 1,163 1,191	235 1,568 3,369 3,371			
Device	Routing	In	vert Outle	et Devices					
#1	Primary	196	.40' 20.0 Head 2.50 Coel 2.65	 10' 20.0' long x 6.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.37 2.51 2.70 2.68 2.68 2.67 2.65 2.65 2.65 2.65 2.66 2.66 2.67 2.69 2.72 2.76 2.83 					
#2	Discardeo	d 195	.30' 0.30 Con	0 in/hr Exfiltratio ductivity to Ground	n over Surface a dwater Elevation =	r ea 194.80' Phase-In	= 0.10'		
Discarded OutFlow Max=0.03 cfs @ 12.20 hrs HW=196.54' (Free Discharge) ←2=Exfiltration (Controls 0.03 cfs)									

Primary OutFlow Max=1.83 cfs @ 12.19 hrs HW=196.54' TW=196.49' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir** (Weir Controls 1.83 cfs @ 0.65 fps)

22201-EXISTING	Type III 24-hr	100-YR 24HR Rainfall=7.77'
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Summary for Pond 2P: Depression in Woods

Inflow An Inflow Outflow Discarde Primary Route	rea = = (= (ed = (= (ed to Reach	1.947 ac, 5.66 cfs @ 5.43 cfs @ 0.11 cfs @ 6.32 cfs @ AP5 : Analy	2.58% Ir 12.32 hi 12.38 hi 12.38 hi 12.38 hi 12.38 hi ysis Poir	mpervious, Inflow I rs, Volume= rs, Volume= rs, Volume= rs, Volume= nt 5	Depth > 4.59" for 0.744 af 0.669 af, Atten= 3 0.104 af 0.565 af	100-YR 24HR event 3%, Lag= 3.6 min					
Routing Peak Ele	Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 176.65' @ 12.38 hrs Surf.Area= 7,514 sf Storage= 5,082 cf										
Plug-Flo Center-c	w detention of-Mass det.	time= 72.7 time= 25.6	min calc min (85	ulated for 0.668 af 8.5 - 832.9)	(90% of inflow)						
Volume	Invert	Avail.S	torage	Storage Description	on						
#1	175.70	5,	471 cf	Custom Stage Da	ata (Irregular)Listed	below (Recalc)					
Elevatio	on S	urf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area					
(fee	et)	(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)					
175.7	0	2,764	204.0	0	0	2,764					
176.0	00	3,841	265.0	986	986	5,042					
176.4	10	7,514	341.0	2,230	3,217	8,709					
176.7	' 0	7,514	341.0	2,254	5,471	8,811					
Device	Routing	Inve	rt Outle	et Devices							
#1	#1 Primary 176.40' 20.0' long x 2.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88 2.85 3.07 3.20 3.32										
#2	Discarded	175.70)' 0.30 Cond	0 in/hr Exfiltration ductivity to Groundy	over Surface area water Elevation = 17	5.20' Phase-In= 0.10'					
Discarded OutFlow Max=0.11 cfs @ 12.38 hrs HW=176.65' (Free Discharge) 2=Exfiltration (Controls 0.11 cfs)											

Primary OutFlow Max=6.29 cfs @ 12.38 hrs HW=176.65' TW=0.00' (Dynamic Tailwater) ☐ 1=Broad-Crested Rectangular Weir (Weir Controls 6.29 cfs @ 1.27 fps)

APPENDIX II

PROPOSED CONDITIONS DRAINAGE ANALYSIS

Summary 2 YEAR Complete 10 YEAR Summary 25 YEAR Complete 50 YEAR Complete 100 YEAR



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Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
0.137	61	>75% Grass cover, Good, HSG B (4S)
2.950	74	>75% Grass cover, Good, HSG C (1S, 3S, 5S, 6S, 7S, 9S, 10S, 11S)
0.007	80	>75% Grass cover, Good, HSG D (1S, 7S)
0.131	82	Dirt roads, HSG B (2S, 4S, 5S, 21S)
0.092	87	Dirt roads, HSG C (5S)
0.019	89	Dirt roads, HSG D (5S)
0.447	98	Paved parking, HSG C (1S, 6S, 7S, 9S, 10S, 11S)
0.092	98	Roofs, HSG B (19S, 20S)
0.178	98	Roofs, HSG C (1S, 7S, 9S, 10S, 12S, 13S, 14S, 15S, 16S, 17S, 18S, 22S)
0.020	98	Water Surface, HSG B (19S, 20S, 21S)
0.028	98	Water Surface, HSG C (12S, 13S, 14S, 15S, 16S, 17S, 18S, 22S)
1.917	55	Woods, Good, HSG B (2S, 4S, 5S)
4.046	70	Woods, Good, HSG C (1S, 3S, 5S, 6S, 7S, 9S)
1.885	77	Woods, Good, HSG D (1S, 2S, 5S, 7S)
11.949	72	TOTAL AREA

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Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
2.296	HSG B	2S, 4S, 5S, 19S, 20S, 21S
7.742	HSG C	1S, 3S, 5S, 6S, 7S, 9S, 10S, 11S, 12S, 13S, 14S, 15S, 16S, 17S, 18S, 22S
1.911	HSG D	1S, 2S, 5S, 7S
0.000	Other	
11.949		TOTAL AREA

Subcatchment15S: Unit 4

Subcatchment16S: Unit 3

Subcatchment17S: Units 1&2

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<u>- 194100, 20 10, 20 00 0, 10</u>	Time enen=0.00.24.00		5 bro 19	1	into v 2				<u>190 -</u>
Reach routi	Runoff by SCS TR-20 m	nis, al-0.0 nethod, UH	=SCS, W	l po leigh by C	ited-CN	-Ind m	nethod		
					yn-otor		- "		
Subcatchment1S: 1S	Rui	noff Area=9	7,026 sf	2.11 ^o	% Imper	vious	Runoff	Depth>().79"
	Flow Le	ength=320'	Tc=19.9	min	CN=73	Runc	off=1.27	cfs 0.14	47 af
Subcatchment2S: 2S	Rui	noff Area=60	6,576 sf	0.00 ⁰	% Imper	vious	Runoff	Depth>().70"
	Flow Le	ength=290'	Tc=18.2	min	CN=71	Runc	off=0.76	cfs 0.08	89 af
Subcatchment3S: 3S	Rui	noff Area=3	9,339 sf	0.00 ⁰	% Imper	vious	Runoff	Depth>().70"
	Flow Length=140' Slope	=0.0123 '/'	Tc=19.1	min	CN=71	Runc	ff=0.44	cfs_0.0	53 af
Subcatchment4S: 4S	Rui	noff Area=2	7,185 sf	0.00 ⁰	% Imper	vious	Runoff	Depth>().24"
	Flow Le	ength=194'	Tc=23.6	min	CN=58	Runc	off=0.05	cfs_0.0	12 af
Subcatchment5S: 5S	Runo	off Area=11	3,462 sf	0.00 ⁰	% Imper	vious	Runoff	Depth>().49"
	Flow Le	ength=602'	Tc=32.4	min	CN=66	Runc	off=0.63	cfs 0.1)	07 af
Subcatchment6S: 6S	Runo	off Area=13	,598 sf 2	21.51	% Imper	vious	Runoff	Depth> [,]	1.06"
	Flow Length=92' Slop	e=0.0217 '/'	' Tc=9.3	min	CN=78	Runc	off=0.33	cfs 0.02	27 af
Subcatchment7S: 7S	Rui	noff Area=8	4,203 sf	3.46º	% Imper	vious	Runoff	Depth>().79"
	Flow Le	ength=456'	Tc=23.1	min	CN=73	Runc	off=1.04	cfs 0.12	27 af
Subcatchment9S: 9S	Rui	noff Area=4	1,089 sf	6.98º	% Imper	vious	Runoff	Depth>().89"
	Flow Le	ength=211'	Tc=22.8	min	CN=75	Runc	off=0.59	cfs_0.0 ⁻	70 af
Subcatchment10S: 10S	Runo	off Area=17	,686 sf 5 Tc=6.0	57.92° min	% Imper CN=88	vious Runc	Runoff off=0.81	Depth>´ cfs_0.0	1.73" 58 af
Subcatchment11S: 11S	Rui	noff Area=9	,293 sf 1	8.90 ⁰	% Imper	vious	Runoff	Depth> [,]	1.11"
	Flow Le	ength=194'	Tc=10.2	min	CN=79	Runc	off=0.23	cfs 0.02	20 af
Subcatchment12S: Unit	s 5&6 Ru	noff Area=9	994 sf 10 Tc=6.0	0.00° min	% Imper CN=98	vious Runc	Runoff off=0.06	Depth>2 cfs 0.0	2.67" 05 af
Subcatchment13S: Unit	5 Ru	noff Area=5	580 sf 10 Tc=6.0	0.00° min	% Imper CN=98	vious Runc	Runoff off=0.04	Depth>2 cfs_0.0	2.67" 03 af

Subcatchment14S: Units 3&4Runoff Area=1,046 sf 100.00% Impervious Runoff Depth>2.67"Tc=6.0 min CN=98 Runoff=0.07 cfs 0.005 af

Runoff Area=498 sf 100.00% Impervious Runoff Depth>2.67" Tc=6.0 min CN=98 Runoff=0.03 cfs 0.003 af

Runoff Area=518 sf 100.00% Impervious Runoff Depth>2.67" Tc=6.0 min CN=98 Runoff=0.03 cfs 0.003 af

Runoff Area=1,046 sf 100.00% Impervious Runoff Depth>2.67" Tc=6.0 min CN=98 Runoff=0.07 cfs 0.005 af

22201-PROPOSED Prepared by Jones & Beach Engine HydroCAD® 10.20-3c s/n 00762 © 2023	Type III 24-hr 2-YR 24HR Rainfall=2.90"ers IncPrinted 3/22/2024HydroCAD Software Solutions LLCPage 5
Subcatchment18S: Unit 1	Runoff Area=498 sf 100.00% Impervious Runoff Depth>2.67" Tc=6.0 min CN=98 Runoff=0.03 cfs 0.003 af
Subcatchment19S: 19S	Runoff Area=2,375 sf 100.00% Impervious Runoff Depth>2.67" Tc=6.0 min CN=98 Runoff=0.15 cfs 0.012 af
Subcatchment20S: 20S	Runoff Area=2,375 sf 100.00% Impervious Runoff Depth>2.67" Tc=6.0 min CN=98 Runoff=0.15 cfs 0.012 af
Subcatchment21S: Gravel Trail	Runoff Area=574 sf 15.85% Impervious Runoff Depth>1.50" Tc=6.0 min CN=85 Runoff=0.02 cfs 0.002 af
Subcatchment22S: Unit 2	Runoff Area=518 sf 100.00% Impervious Runoff Depth>2.67" Tc=6.0 min CN=98 Runoff=0.03 cfs 0.003 af
Reach 1R: Flow Through 9S n=0.030	Avg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af L=140.0' S=0.0329 '/' Capacity=43.14 cfs Outflow=0.00 cfs 0.000 af
Reach 3R: Culvert 15.0" Round Pipe n=0.01	Avg. Flow Depth=0.31' Max Vel=3.11 fps Inflow=0.74 cfs 0.090 af 2 L=49.0' S=0.0061 '/' Capacity=5.48 cfs Outflow=0.74 cfs 0.090 af
Reach 4R: Swale n=0.030	Avg. Flow Depth=0.08' Max Vel=1.83 fps Inflow=0.18 cfs 0.125 af L=120.0' S=0.0517 '/' Capacity=30.09 cfs Outflow=0.18 cfs 0.125 af
Reach 5R: Flow Through 1S n=0.030	Avg. Flow Depth=0.04' Max Vel=0.93 fps Inflow=0.18 cfs 0.125 af L=191.0' S=0.0497 '/' Capacity=53.08 cfs Outflow=0.18 cfs 0.124 af
Reach 6R: Flow Through 5S n=0.030	Avg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af L=600.0' S=0.0367 '/' Capacity=45.58 cfs Outflow=0.00 cfs 0.000 af
Reach AP1: Analysis Point 1	Inflow=2.12 cfs 0.361 af Outflow=2.12 cfs 0.361 af
Reach AP2: Analysis Point 2	Inflow=0.44 cfs 0.053 af Outflow=0.44 cfs 0.053 af
Reach AP3: Analysis Point 3	Inflow=0.05 cfs 0.012 af Outflow=0.05 cfs 0.012 af
Reach AP4: Analysis Point 4	Inflow=0.63 cfs 0.107 af Outflow=0.63 cfs 0.107 af
Reach AP5: Analysis Point 5	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Pond 1P: Isolated Wetland Discarded=0	Peak Elev=196.19' Storage=682 cf Inflow=0.33 cfs 0.027 af .02 cfs 0.017 af Primary=0.00 cfs 0.000 af Outflow=0.02 cfs 0.017 af
Pond 2P: Depression in Woods Discarded=0	Peak Elev=176.38' Storage=3,070 cf Inflow=1.04 cfs 0.127 af .09 cfs 0.077 af Primary=0.00 cfs 0.000 af Outflow=0.09 cfs 0.077 af

22201-PROPOSED Type III 24-hr2-YR 24HR Rainfall=2.90"Prepared by Jones & Beach Engineers IncPrinted 3/22/2024HydroCAD® 10.20-3cs/n 00762© 2023 HydroCAD Software Solutions LLCPage 6						all=2.90" /22/2024
Pond 3P: Center of Cu	Il De Sac	Peak	Elev=191.62'	Storage=3,011	cf Inflow=1.25 cfs Outflow=0.18 cfs	0.148 af 0.125 af
Pond 4P: Drip Edge	Discarded=0.02 cfs(Peak 0.005 af	Elev=190.99' Secondary=0.	Storage=0.002 a 00 cfs 0.000 af	af Inflow=0.06 cfs Outflow=0.02 cfs	0.005 af 0.005 af
Pond 5P: Drip Edge	Discarded=0.01 cfs(Peak 0.003 af	Elev=190.42' Secondary=0.	Storage=0.001 a 00 cfs 0.000 af	af Inflow=0.04 cfs Outflow=0.01 cfs	0.003 af 0.003 af
Pond 6P: Drip Edge	Discarded=0.04 cfs(Peak 0.005 af	Elev=188.99' Secondary=0.	Storage=0.001 a 00 cfs 0.000 af	af Inflow=0.07 cfs Outflow=0.04 cfs	0.005 af 0.005 af
Pond 7P: Drip Edge	Discarded=0.00 cfs(Peak 0.002 af	Elev=189.54' Secondary=0.	Storage=0.001 a 00 cfs 0.000 af	af Inflow=0.03 cfs Outflow=0.00 cfs	0.003 af 0.002 af
Pond 8P: Drip Edge	Discarded=0.01 cfs(Peak 0.003 af	Elev=188.40' Secondary=0.	Storage=0.001 a 00 cfs 0.000 af	af Inflow=0.03 cfs Outflow=0.01 cfs	0.003 af 0.003 af
Pond 10P: Drip Edge	Discarded=0.01 cfs(Peak 0.005 af	Elev=193.84' Secondary=0.	Storage=0.002 a 00 cfs 0.000 af	af Inflow=0.07 cfs Outflow=0.01 cfs	0.005 af 0.005 af
Pond 11P: Drip Edge	Discarded=0.01 cfs(Peak 0.003 af	Elev=194.26' Secondary=0.	Storage=0.001 a 00 cfs 0.000 af	af Inflow=0.03 cfs Outflow=0.01 cfs	0.003 af 0.003 af
Pond 20P: Barn	Discarded=0.03 cfs(Peak 0.012 af	Elev=169.52' Secondary=0.	Storage=0.005 00 cfs 0.000 af	af Inflow=0.15 cfs Outflow=0.03 cfs	0.012 af 0.012 af
Pond 22P: Barn	Discarded=0.03 cfs(Peak 0.012 af	Elev=169.52' Secondary=0.	Storage=0.005 00 cfs 0.000 af	af Inflow=0.15 cfs Outflow=0.03 cfs	0.012 af 0.012 af
Pond 23P: Drip Edge	Discarded=0.00 cfs(Peak 0.001 af	Elev=169.77' Secondary=0.	Storage=0.001 a 00 cfs 0.000 af	af Inflow=0.02 cfs Outflow=0.00 cfs	0.002 af 0.001 af
Pond 24P: Plunge Poo	ol with Culvert Outle 15.0" Round	e t Pe d Culvert	eak Elev=193.2 n=0.012 L=50	2' Storage=15 .0' S=0.0100 '/'	cf Inflow=0.23 cfs Outflow=0.23 cfs	0.020 af 0.020 af
Pond 25P: Drip Edge	Discarded=0.01 cfs(Peak 0.003 af	Elev=194.49' Secondary=0.	Storage=0.001 a 00 cfs 0.000 af	af Inflow=0.03 cfs Outflow=0.01 cfs	0.003 af 0.003 af
Total R	unoff Area = 11.949	ac Ru	noff Volume	= 0.766 af Av	erage Runoff De	epth = 0.77"

93.60% Pervious = 11.184 ac 6.40% Impervious = 0.764 ac

22201-PROPOSED	Type III 24-hr	10-YR 24HR Rainfall=4.34"
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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: 1S	Runoff Area=97,026 sf 2.11% Impervious Runoff Depth>1.77" Flow Length=320' Tc=19.9 min CN=73 Runoff=3.05 cfs 0.328 af
Subcatchment2S: 2S	Runoff Area=66,576 sf 0.00% Impervious Runoff Depth>1.62" Flow Length=290' Tc=18.2 min CN=71 Runoff=1.98 cfs 0.207 af
Subcatchment3S: 3S Flow Leng	Runoff Area=39,339 sf 0.00% Impervious Runoff Depth>1.62" gth=140' Slope=0.0123 '/' Tc=19.1 min CN=71 Runoff=1.14 cfs 0.122 af
Subcatchment4S: 4S	Runoff Area=27,185 sf 0.00% Impervious Runoff Depth>0.82" Flow Length=194' Tc=23.6 min CN=58 Runoff=0.30 cfs 0.043 af
Subcatchment5S: 5S	Runoff Area=113,462 sf 0.00% Impervious Runoff Depth>1.28" Flow Length=602' Tc=32.4 min CN=66 Runoff=2.00 cfs 0.279 af
Subcatchment6S: 6S	Runoff Area=13,598 sf 21.51% Impervious Runoff Depth>2.16" ength=92' Slope=0.0217 '/' Tc=9.3 min CN=78 Runoff=0.69 cfs 0.056 af
Subcatchment7S: 7S	Runoff Area=84,203 sf 3.46% Impervious Runoff Depth>1.77" Flow Length=456' Tc=23.1 min CN=73 Runoff=2.49 cfs 0.285 af
Subcatchment9S: 9S	Runoff Area=41,089 sf 6.98% Impervious Runoff Depth>1.92" Flow Length=211' Tc=22.8 min CN=75 Runoff=1.34 cfs 0.151 af
Subcatchment10S: 10S	Runoff Area=17,686 sf 57.92% Impervious Runoff Depth>3.04" Tc=6.0 min CN=88 Runoff=1.40 cfs 0.103 af
Subcatchment11S: 11S	Runoff Area=9,293 sf 18.90% Impervious Runoff Depth>2.24" Flow Length=194' Tc=10.2 min CN=79 Runoff=0.48 cfs 0.040 af
Subcatchment12S: Units 5&6	Runoff Area=994 sf 100.00% Impervious Runoff Depth>4.10" Tc=6.0 min CN=98 Runoff=0.09 cfs 0.008 af
Subcatchment13S: Unit 5	Runoff Area=580 sf 100.00% Impervious Runoff Depth>4.10" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af
Subcatchment14S: Units 3&4	Runoff Area=1,046 sf 100.00% Impervious Runoff Depth>4.10" Tc=6.0 min CN=98 Runoff=0.10 cfs 0.008 af
Subcatchment15S: Unit 4	Runoff Area=498 sf 100.00% Impervious Runoff Depth>4.10" Tc=6.0 min CN=98 Runoff=0.05 cfs 0.004 af
Subcatchment16S: Unit 3	Runoff Area=518 sf 100.00% Impervious Runoff Depth>4.10" Tc=6.0 min CN=98 Runoff=0.05 cfs 0.004 af
Subcatchment17S: Units 1&2	Runoff Area=1,046 sf 100.00% Impervious Runoff Depth>4.10" Tc=6.0 min CN=98 Runoff=0.10 cfs 0.008 af

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Subcatchment18S: Unit 1	Runoff Area=498 sf 100.00% Impervious Runoff Depth>4.10" Tc=6.0 min CN=98 Runoff=0.05 cfs 0.004 af
Subcatchment19S: 19S	Runoff Area=2,375 sf 100.00% Impervious Runoff Depth>4.10" Tc=6.0 min CN=98 Runoff=0.23 cfs 0.019 af
Subcatchment20S: 20S	Runoff Area=2,375 sf 100.00% Impervious Runoff Depth>4.10" Tc=6.0 min CN=98 Runoff=0.23 cfs 0.019 af
Subcatchment21S: Gravel Trail	Runoff Area=574 sf 15.85% Impervious Runoff Depth>2.76" Tc=6.0 min CN=85 Runoff=0.04 cfs 0.003 af
Subcatchment22S: Unit 2	Runoff Area=518 sf 100.00% Impervious Runoff Depth>4.10" Tc=6.0 min CN=98 Runoff=0.05 cfs 0.004 af
Reach 1R: Flow Through 9S n=0.030	Avg. Flow Depth=0.03' Max Vel=0.66 fps Inflow=0.13 cfs 0.008 af L=140.0' S=0.0329 '/' Capacity=43.14 cfs Outflow=0.10 cfs 0.008 af
Reach 3R: Culvert 15.0" Round Pipe n=0.01	Avg. Flow Depth=0.47' Max Vel=3.90 fps Inflow=1.65 cfs 0.199 af 2 L=49.0' S=0.0061 '/' Capacity=5.48 cfs Outflow=1.65 cfs 0.199 af
Reach 4R: Swale n=0.030	Avg. Flow Depth=0.11' Max Vel=2.18 fps Inflow=0.31 cfs 0.249 af L=120.0' S=0.0517 '/' Capacity=30.09 cfs Outflow=0.31 cfs 0.249 af
Reach 5R: Flow Through 1S n=0.030	Avg. Flow Depth=0.05' Max Vel=1.10 fps Inflow=0.31 cfs 0.249 af L=191.0' S=0.0497 '/' Capacity=53.08 cfs Outflow=0.31 cfs 0.248 af
Reach 6R: Flow Through 5S n=0.030	Avg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af L=600.0' S=0.0367 '/' Capacity=45.58 cfs Outflow=0.00 cfs 0.000 af
Reach AP1: Analysis Point 1	Inflow=5.21 cfs 0.784 af Outflow=5.21 cfs 0.784 af
Reach AP2: Analysis Point 2	Inflow=1.14 cfs 0.122 af Outflow=1.14 cfs 0.122 af
Reach AP3: Analysis Point 3	Inflow=0.30 cfs 0.043 af Outflow=0.30 cfs 0.043 af
Reach AP4: Analysis Point 4	Inflow=2.00 cfs 0.279 af Outflow=2.00 cfs 0.279 af
Reach AP5: Analysis Point 5	Inflow=1.56 cfs 0.126 af Outflow=1.56 cfs 0.126 af
Pond 1P: Isolated Wetland Discarded=0	Peak Elev=196.43' Storage=1,191 cf Inflow=0.69 cfs 0.056 af .03 cfs 0.028 af Primary=0.13 cfs 0.008 af Outflow=0.17 cfs 0.037 af
Pond 2P: Depression in Woods Discarded=0	Peak Elev=176.50' Storage=3,954 cf Inflow=2.50 cfs 0.285 af .10 cfs 0.091 af Primary=1.56 cfs 0.126 af Outflow=1.66 cfs 0.217 af

22201-PROPOSED Type III 24-hr10-YR24HR Rainfall=4.34"Prepared by Jones & Beach Engineers IncPrinted 3/22/2024HydroCAD® 10.20-3cs/n 00762© 2023 HydroCAD Software Solutions LLCPage 9						fall=4.34" 3/22/2024 Page 9
Pond 3P: Center of Cu	Il De Sac	Peak	: Elev=192.99'	Storage=6,702	2 cf Inflow=2.50 cfs Outflow=0.31 cfs	0.302 af 0.249 af
Pond 4P: Drip Edge	Discarded=0.03 cfs	Peak 0.008 af	Elev=191.50' Secondary=0	Storage=0.002 .02 cfs 0.000 a	2 af Inflow=0.09 cfs f Outflow=0.04 cfs	0.008 af 0.008 af
Pond 5P: Drip Edge	Discarded=0.02 cfs	Peak 0.005 af	Elev=190.70' Secondary=0	Storage=0.001 .00 cfs 0.000 a	af Inflow=0.06 cfs f Outflow=0.02 cfs	0.005 af 0.005 af
Pond 6P: Drip Edge	Discarded=0.05 cfs	Peak 0.008 af	Elev=189.24' Secondary=0	Storage=0.001 .00 cfs 0.000 a	af Inflow=0.10 cfs f Outflow=0.05 cfs	0.008 af 0.008 af
Pond 7P: Drip Edge	Discarded=0.00 cfs	Peak 0.002 af	Elev=190.52' Secondary=0	Storage=0.002 .00 cfs 0.000 a	2 af Inflow=0.05 cfs f Outflow=0.00 cfs	0.004 af 0.002 af
Pond 8P: Drip Edge	Discarded=0.01 cfs	Peak 0.004 af	Elev=188.84' Secondary=0	Storage=0.001 .00 cfs 0.000 a	af Inflow=0.05 cfs f Outflow=0.01 cfs	0.004 af 0.004 af
Pond 10P: Drip Edge	Discarded=0.02 cfs	Peak 0.008 af	Elev=194.43' Secondary=0	Storage=0.003 .00 cfs 0.000 a	8 af Inflow=0.10 cfs f Outflow=0.02 cfs	0.008 af 0.008 af
Pond 11P: Drip Edge	Discarded=0.02 cfs	Peak 0.004 af	Elev=194.56' Secondary=0	Storage=0.001 .00 cfs 0.000 a	af Inflow=0.05 cfs f Outflow=0.02 cfs	0.004 af 0.004 af
Pond 20P: Barn	Discarded=0.04 cfs	Peak 0.018 af	Elev=170.29' Secondary=0	Storage=0.007 .00 cfs 0.000 a	′ af Inflow=0.23 cfs f Outflow=0.04 cfs	0.019 af 0.018 af
Pond 22P: Barn	Discarded=0.04 cfs	Peak 0.018 af	Elev=170.29' Secondary=0	Storage=0.007 .00 cfs 0.000 a	′ af Inflow=0.23 cfs f Outflow=0.04 cfs	0.019 af 0.018 af
Pond 23P: Drip Edge	Discarded=0.00 cfs	Peak 0.002 af	Elev=170.56' Secondary=0	Storage=0.002 .00 cfs 0.000 a	2 af Inflow=0.04 cfs f Outflow=0.00 cfs	0.003 af 0.002 af
Pond 24P: Plunge Poc	ol with Culvert Outle 15.0" Roun	et Pe d Culvert	eak Elev=193. n=0.012 L=50	32' Storage=25).0' S=0.0100 '	5 cf Inflow=0.48 cfs /' Outflow=0.48 cfs	0.040 af 0.040 af
Pond 25P: Drip Edge	Discarded=0.01 cfs	Peak 0.004 af	Elev=194.90' Secondary=0	Storage=0.001 .00 cfs 0.000 a	af Inflow=0.05 cfs f Outflow=0.01 cfs	0.004 af 0.004 af
Total R	unoff Area = 11.94	9 ac Ru 93.60%	noff Volume Pervious =	= 1.698 af A 11.184 ac 6	verage Runoff Do 5.40% Impervious	epth = 1.70" = 0.764 ac

22201-PROPOSED	Type III 24-hr	10-YR 24HR Rai	nfall=4.34'
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Summary for Subcatchment 1S: 1S

Runoff = 3.05 cfs @ 12.29 hrs, Volume= 0. Routed to Reach AP1 : Analysis Point 1

0.328 af, Depth> 1.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR 24HR Rainfall=4.34"

A	rea (sf)	CN	Description		
	930	98	Roofs, HSC	G C	
	1,120	98	Paved park	ing, HSG C	
	47,794	70	Woods, Go	od, HSG C	
	23,377	74	>75% Gras	s cover, Go	bod, HSG C
	23,763	77	Woods, Go	od, HSG D	
	42	80	>75% Gras	s cover, Go	ood, HSG D
	97,026	73	Weighted A	verage	
	94,976		97.89% Pe	rvious Area	
	2,050		2.11% Impe	ervious Are	a
Tc	Length	Slope	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
16.6	100	0.0433	0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
1.4	113	0.0708	1.33		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
1.4	70	0.0286	0.85		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.5	37	0.0541	1.16		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
19.9	320	Total			

Summary for Subcatchment 2S: 2S

Runoff = 1.98 cfs @ 12.27 hrs, Volume= 0.207 af, Depth> 1.62" Routed to Reach AP1 : Analysis Point 1

Area (sf)	CN	Description
1,242	82	Dirt roads, HSG B
19,492	55	Woods, Good, HSG B
45,842	77	Woods, Good, HSG D
66,576 66,576	71	Weighted Average 100.00% Pervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.3	82	0.0610	0.11		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
2.9	18	0.1111	0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
0.2	21	0.1111	1.67		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.4	30	0.0571	1.19		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
2.4	139	0.0367	0.96		Shallow Concentrated Flow,

18.2 290 Total

Summary for Subcatchment 3S: 3S

Woodland Kv= 5.0 fps

Runoff	=	1.14 cfs @	12.28 hrs,	Volume=
Route	d to R	leach AP2 : Anal	ysis Point 2	

0.122 af, Depth> 1.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR 24HR Rainfall=4.34"

A	rea (sf)	CN E	Description						
	27,514	70 V) Woods, Good, HSG C						
	11,825	74 >	75% Gras	s cover, Go	ood, HSG C				
	39,339	71 V	Veighted A	verage					
	39,339	1	00.00% Pe	ervious Are	a				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
10.6	81	0.0123	0.13		Sheet Flow,				
					Grass: Short n= 0.150 P2= 2.90"				
7.3	19	0.0123	0.04		Sheet Flow,				
					Woods: Light underbrush n= 0.400 P2= 2.90"				
1.2	40	0.0123	0.55		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
19.1	140	Total							

Summary for Subcatchment 4S: 4S

Runoff = 0.30 cfs @ 12.41 hrs, Volume= 0.043 af, Depth> 0.82" Routed to Reach AP3 : Analysis Point 3

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A	rea (sf)	CN E	Description						
	1,810	82 E	2 Dirt roads, HSG B						
	19,394	55 V	Voods, Go	od, HSG B					
	5,981	61 >	75% Gras	s cover, Go	ood, HSG B				
	27,185	58 V	Veighted A	verage					
	27,185	1	00.00% P	ervious Are	а				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
9.6	49	0.0408	0.09		Sheet Flow,				
					Woods: Light underbrush n= 0.400 P2= 2.90"				
12.8	51	0.0213	0.07		Sheet Flow,				
					Woods: Light underbrush n= 0.400 P2= 2.90"				
1.0	43	0.0213	0.73		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
0.2	51	0.0588	3.90		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
23.6	194	Total							

Summary for Subcatchment 5S: 5S

Runoff = 2.00 cfs @ 12.50 hrs, Volume= Routed to Reach AP4 : Analysis Point 4 0.279 af, Depth> 1.28"

Area (sf)	CN	Description
2,174	82	Dirt roads, HSG B
44,614	55	Woods, Good, HSG B
4,013	87	Dirt roads, HSG C
9,149	74	>75% Grass cover, Good, HSG C
49,989	70	Woods, Good, HSG C
817	89	Dirt roads, HSG D
2,706	77	Woods, Good, HSG D
113,462	66	Weighted Average
113,462		100.00% Pervious Area

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Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
21.0	100	0.0239	0.08		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
0.4	17	0.0239	0.77		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.8	48	0.0417	1.02		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
1.2	94	0.0638	1.26		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
2.9	116	0.0172	0.66		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.6	51	0.0784	1.40		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
5.5	176	0.0114	0.53		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
32.4	602	Total			

Summary for Subcatchment 6S: 6S

Runoff	=	0.69 cfs @	12.14 hrs,	Volume=
Route	d to Po	ond 1P : Isolate	d Wetland	

0.056 af, Depth> 2.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR 24HR Rainfall=4.34"

Α	rea (sf)	CN	Description						
	2,925	98	Paved park	ing, HSG C	;				
	5,274	74	>75% Ġras	s cover, Go	ood, HSG C				
	5,399	70	Woods, Go	od, HSG C					
	13,598	78	Weighted A	verage					
	10,673		78.49% Pervious Area						
	2,925		21.51% Imp	pervious Ar	ea				
Tc	Length	Slope	e Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)) (ft/sec)	(cfs)					
9.3	92	0.0217	0.16		Sheet Flow,				
					Grass: Short	n= 0.150	P2= 2.90"		

Summary for Subcatchment 7S: 7S

Runoff	=	2.49 cfs @	12.34 hrs,	Volume=	0.285 af,	Depth>	1.77"
Routed	to Pond	2P : Depres	sion in Woo	ods			

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Δ	rea (sf)	CN F)escription		
/	808	08 5	Poofe HSG		
	2 014	98 F	Paved nark	ing HSG (
	37 527	70 V	Voods Go	nd HSG C	
	33.711	74 >	75% Gras	s cover. Go	ood, HSG C
	9,806	77 V	Voods, Go	od, HSG D	
	247	80 >	75% Gras	s cover, Go	bod, HSG D
	84,203	73 V	Veighted A	verage	
	81,291	9	6.54% Pei	vious Area	
	2,912	3	.46% Impe	ervious Are	а
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.2	13	0.0200	0.87		Sheet Flow,
	00	0 4000	0.04		Smooth surfaces $n = 0.011 P2 = 2.90"$
1.4	20	0.1200	0.24		Sheet Flow,
7 2	20	0.0512	0.00		Grass: Short n= 0.150 P2= 2.90
1.5	39	0.0515	0.09		Woods: Light underbrush n= 0.400 P2= 2.00"
73	28	0 0260	0.06		Sheet Flow
7.0	20	0.0200	0.00		Woods: Light underbrush $n=0.400$ P2= 2.90"
2.6	127	0.0260	0.81		Shallow Concentrated Flow.
		0.0200			Woodland $Kv = 5.0 \text{ fps}$
0.8	75	0.1067	1.63		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
1.0	56	0.0357	0.94		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.2	22	0.0909	1.51		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
2.3	76	0.0125	0.56		Shallow Concentrated Flow,
					vvoodiand KV= 5.0 fps
23.1	456	l otal			

Summary for Subcatchment 9S: 9S

Runoff = 1.34 cfs @ 12.33 hrs, Volume= 0.151 af, Depth> 1.92" Routed to Reach 3R : Culvert

Area (sf)	CN	Description
704	98	Roofs, HSG C
2,162	98	Paved parking, HSG C
8,023	70	Woods, Good, HSG C
30,200	74	>75% Grass cover, Good, HSG C
41,089	75	Weighted Average
38,223		93.02% Pervious Area
2,866		6.98% Impervious Area

22201-	PROPO	SED			Type III 24-hr 10-YR 24HR Rainfall=4.34
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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
20.7	100	0.0248	0.08		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
0.4	21	0.0248	0.79		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
1.7	90	0.0167	0.90		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
00.0	044	Tatal			

22.8 211 Total

Summary for Subcatchment 10S: 10S

Runoff = 1.40 cfs @ 12.09 hrs, Volume= 0.103 af, Depth> 3.04" Routed to Pond 3P : Center of Cul De Sac

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR 24HR Rainfall=4.34"

Area	a (sf)	CN	Description					
	728	98	Roofs, HSC	ЭС				
9	9,516	98	Paved park	ing, HSG C	С			
7	,442	74	>75% Ġras	s cover, Go	Good, HSG C			
17	7,686	88	Weighted A	verage				
7	' ,442		42.08% Pervious Area					
10),244		57.92% Imp	pervious Are	rea			
Tc L	ength.	Slope	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)				
6.0					Direct Entry,			

Summary for Subcatchment 11S: 11S

Runoff = 0.48 cfs @ 12.15 hrs, Volume= 0.040 af, Depth> 2.24" Routed to Pond 24P : Plunge Pool with Culvert Outlet

Are	a (sf)	CN	Description			
	1,756	98	Paved parking, HSG C			
	7,537	74	>75% Grass cover, Good, HSG C			
	9,293	79	Weighted Average			
	7,537		81.10% Pervious Area			
	1,756		18.90% Impervious Area			

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Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(CIS)					
9.7	73	0.0123	0.13		Sheet Flow,				
					Grass: Short n= 0.150 P2= 2.90"				
0.5	121	0.0165	4.25	17.00	Trap/Vee/Rect Channel Flow.				
					Bot W=1 00' D=1 00' Z= 3 0 '/' Top W=7 00'				
					n= 0.030 Stream, clean & straight				
10.2	194	Total							
	Summary for Subcatchment 12S: Units 5&6								
Runoff Route	Runoff = 0.09 cfs @ 12.09 hrs, Volume= 0.008 af, Depth> 4.10" Routed to Pond 4P : Drip Edge								

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR 24HR Rainfall=4.34"

A	rea (sf)	CN	Description				
	838	98	Roofs, HSC	G C			
	156	98	Water Surfa	ace, HSG C			
	994	98	Weighted A	verage			
	994		100.00% Impervious Area				
Tc	Length	Slop	e Velocity	Capacity	Description		
(min)	(feet)	(ft/f) (ft/sec)	(cfs)			
6.0					Direct Entry,		

Summary for Subcatchment 13S: Unit 5

Runoff = 0.06 cfs @ 12.09 hrs, Volume= 0.005 af, Depth> 4.10" Routed to Pond 5P : Drip Edge

A	rea (sf)	CN	Description		
	395	98	Roofs, HSC	G C	
	185	98	Water Surfa	ace, HSG C	C
	580	98	Weighted A	verage	
	580		100.00% In	npervious A	Area
Tc	Length	Slop	e Velocity	Capacity	Description
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)	
6.0					Direct Entry,

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Summary for Subcatchment 14S: Units 3&4

Runoff = 0.10 cfs @ 12.09 hrs, Volume= 0.008 af, Depth> 4.10" Routed to Pond 6P : Drip Edge

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR 24HR Rainfall=4.34"

Ar	ea (sf)	CN	Description				
	838	98	Roofs, HSG	G C			
	208	98	Water Surfa	ace, HSG C			
	1,046	98	Weighted A	verage			
	1,046		100.00% In	npervious A	rea		
Tc	Length	Slop	e Velocity	Capacity	Description		
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)			
6.0					Direct Entry,		
	Summary for Subcatchment 15S: Unit 4						

Runoff = 0.05 cfs @ 12.09 hrs, Volume= 0.004 af, Depth> 4.10" Routed to Pond 7P : Drip Edge

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR 24HR Rainfall=4.34"

A	rea (sf)	CN	Description					
	395	98	Roofs, HSG	S C				
	103	98	Water Surfa	ace, HSG C	C			
	498	98	Weighted Average					
	498		100.00% Im	npervious A	Area			
Tc	Length	Slope	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)				
6.0					Direct Entry,			

Summary for Subcatchment 16S: Unit 3

Runoff = 0.05 cfs @ 12.09 hrs, Volume= 0.004 af, Depth> 4.10" Routed to Pond 8P : Drip Edge

Α	rea (sf)	CN	Description
	395	98	Roofs, HSG C
	123	98	Water Surface, HSG C
	518	98	Weighted Average
	518		100.00% Impervious Area

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Tc (min)	Length (feet)	Slop (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Descripti	on			
6.0					Direct E	ntry,			
Summary for Subcatchment 17S: Units 1&2									
Runoff Route	= ed to Pone	0.10 d 10P :	cfs @ 12.09 Drip Edge	9 hrs, Volu	ime=	0.008 af, [Depth> 4.10"		
Runoff b Type III	y SCS TF 24-hr 10-	R-20 m YR 24I	ethod, UH=S HR Rainfall=	CS, Weigł 4.34"	nted-CN, T	ime Span= 0.0)0-24.00 hrs, d	t= 0.05 hrs	
A	rea (sf)	CN	Description						
	838 208	98 98	Roofs, HSG Water Surfa	i C ice, HSG C)				
	1,046 1,046	98	Weighted A 100.00% Im	verage Ipervious A	Area				
Tc (min)	Length (feet)	Slop (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Descripti	on			
6.0					Direct E	ntry,			
			Summ	ary for S	ubcatch	ment 18S:	Unit 1		
Runoff Route	= ed to Pone	0.05 d 11P :	cfs @ 12.09 Drip Edge	9 hrs, Volu	ime=	0.004 af, [Depth> 4.10"		
Runoff b Type III	y SCS TF 24-hr 10-	R-20 m YR 24I	ethod, UH=S HR Rainfall=	6CS, Weigł 4.34"	nted-CN, T	ïme Span= 0.0	00-24.00 hrs, d	t= 0.05 hrs	
А	rea (sf)	CN	Description						
	395	98	Roofs, HSG	i C					
	103	98	Water Surfa	ice, HSG C)				
	498 498	98	Weighted A 100.00% Im	verage Ipervious A	Area				

TcLengthSlopeVelocityCapacityDescription(min)(feet)(ft/ft)(ft/sec)(cfs)

6.0

Direct Entry,

Summary for Subcatchment 19S: 19S

Runoff = 0.23 cfs @ 12.09 hrs, Volume= 0.019 af, Depth> 4.10" Routed to Pond 20P : Barn

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Α	rea (sf)	CN	Description		
	1,995	98	Roofs, HSC	βB	
	380	98	Water Surfa	ace, HSG E	3
	2,375	98	Weighted A	verage	
	2,375		100.00% In	npervious A	Area
Tc	Length	Slop	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	
6.0					Direct Entry,

Summary for Subcatchment 20S: 20S

Runoff = 0.23 cfs @ 12.09 hrs, Volume= 0.019 af, Depth> 4.10" Routed to Pond 22P : Barn

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR 24HR Rainfall=4.34"

A	rea (sf)	CN	Description					
	1,995	98	Roofs, HSG	βB				
	380	98	Water Surfa	ace, HSG B	3			
	2,375	98	Weighted A	verage				
	2,375		100.00% Impervious Area					
Tc	Length	Slop	e Velocity	Capacity	Description			
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)				
6.0					Direct Entry,			
					•			

Summary for Subcatchment 21S: Gravel Trail

Runoff = 0.04 cfs @ 12.09 hrs, Volume= 0.003 af, Depth> 2.76" Routed to Pond 23P : Drip Edge

A	rea (sf)	CN	Description		
	483	82	Dirt roads,	HSG B	
	91	98	Water Surfa	ace, HSG B	3
	574	85	Weighted A	verage	
	483		84.15% Pe	rvious Area	3
	91		15.85% Imp	pervious Ar	rea
То	Longth	Slop		Capacity	Description
UT (mim)	Lengin	210p		Capacity	Description
<u>(min)</u>	(ieel)	(11/11) (it/sec)	(CIS)	
6.0					Direct Entry,

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Summary for Subcatchment 22S: Unit 2

Runoff = 0.05 cfs @ 12.09 hrs, Volume= Routed to Pond 25P : Drip Edge 0.004 af, Depth> 4.10"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR 24HR Rainfall=4.34"

Ar	ea (sf)	CN	Description		
	395	98	Roofs, HSC	G C	
	123	98	Water Surfa	ace, HSG C	C
	518	98	Weighted A	verage	
	518		100.00% In	npervious A	Area
Tc	Length	Slop	e Velocity	Capacity	Description
(min)	(feet)	(ft/f	i) (ft/sec)	(cfs)	
6.0					Direct Entry,
					-

Summary for Reach 1R: Flow Through 9S

[80] Warning: Exceeded Pond 1P by 0.08' @ 21.70 hrs (0.00 cfs 0.001 af)

 Inflow Area =
 0.312 ac, 21.51% Impervious, Inflow Depth =
 0.32" for 10-YR 24HR event

 Inflow =
 0.13 cfs @
 12.62 hrs, Volume=
 0.008 af

 Outflow =
 0.10 cfs @
 12.69 hrs, Volume=
 0.008 af, Atten= 29%, Lag= 4.4 min

 Routed to Reach 3R : Culvert
 Culvert
 0.008 af, Atten= 29%, Lag= 4.4 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 0.66 fps, Min. Travel Time= 3.5 min Avg. Velocity = 0.37 fps, Avg. Travel Time= 6.4 min

Peak Storage= 20 cf @ 12.69 hrs Average Depth at Peak Storage= 0.03', Surface Width= 7.32' Bank-Full Depth= 0.50' Flow Area= 10.0 sf, Capacity= 43.14 cfs

30.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight Length= 140.0' Slope= 0.0329 '/' Inlet Invert= 196.40', Outlet Invert= 191.80'

‡

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Summary for Reach 3R: Culvert

[52] Hint: Inlet/Outlet conditions not evaluated[62] Hint: Exceeded Reach 1R OUTLET depth by 0.47' @ 12.30 hrs

Inflow Area = 1.469 ac, 11.80% Impervious, Inflow Depth > 1.62" for 10-YR 24HR event Inflow = 1.65 cfs @ 12.29 hrs, Volume= 0.199 af Outflow = 1.65 cfs @ 12.30 hrs, Volume= 0.199 af, Atten= 0%, Lag= 0.2 min Routed to Pond 3P : Center of Cul De Sac

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 3.90 fps, Min. Travel Time= 0.2 min Avg. Velocity = 1.66 fps, Avg. Travel Time= 0.5 min

Peak Storage= 21 cf @ 12.30 hrs Average Depth at Peak Storage= 0.47', Surface Width= 1.21' Bank-Full Depth= 1.25' Flow Area= 1.2 sf, Capacity= 5.48 cfs

15.0" Round Pipe n= 0.012 Length= 49.0' Slope= 0.0061 '/' Inlet Invert= 191.80', Outlet Invert= 191.50'



Summary for Reach 4R: Swale

Inflow Area = 1.875 ac, 21.79% Impervious, Inflow Depth > 1.60" for 10-YR 24HR event Inflow = 0.31 cfs @ 14.01 hrs, Volume= 0.249 af Outflow = 0.31 cfs @ 14.02 hrs, Volume= 0.249 af, Atten= 0%, Lag= 0.6 min Routed to Reach 5R : Flow Through 1S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 2.18 fps, Min. Travel Time= 0.9 min Avg. Velocity = 1.63 fps, Avg. Travel Time= 1.2 min

Peak Storage= 17 cf @ 14.02 hrs Average Depth at Peak Storage= 0.11', Surface Width= 1.65' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 30.09 cfs

1.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight Side Slope Z-value= 3.0 '/' Top Width= 7.00' Length= 120.0' Slope= 0.0517 '/' Inlet Invert= 189.70', Outlet Invert= 183.50'



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30.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight Length= 600.0' Slope= 0.0367 '/' Inlet Invert= 196.00', Outlet Invert= 174.00'



Summary for Reach AP1: Analysis Point 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow A	rea =	5.631 ac,	8.09% Impervious,	Inflow Depth > 1	.67" for 10-YR 24HR event
Inflow	=	5.21 cfs @	12.28 hrs, Volume	= 0.784 at	
Outflow	=	5.21 cfs @	12.28 hrs, Volume	= 0.784 at	, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow A	rea =	0.903 ac,	0.00% Impervious,	Inflow Depth > 1	1.62'	' for 10-YR 24HR event
Inflow	=	1.14 cfs @	12.28 hrs, Volume	= 0.122 a	f	
Outflow	=	1.14 cfs @	12.28 hrs, Volume	= 0.122 a	f, A	tten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow A	rea	=	0.624 ac,	0.00% Impervious,	Inflow Depth >	0.82"	for 10-YR 24HR event
Inflow	-	=	0.30 cfs @	12.41 hrs, Volume	= 0.043 a	af	
Outflow	=	=	0.30 cfs @	12.41 hrs, Volume	= 0.043 a	af, Atter	n= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Analysis Point 4

[40] Hint: Not Described (Outflow=Inflow)

Inflow Ar	ea =	2.605 ac,	0.00% Impervious,	Inflow Depth > 1.2	28" for 10-YR 24HR event
Inflow	=	2.00 cfs @	12.50 hrs, Volume	= 0.279 af	
Outflow	=	2.00 cfs @	12.50 hrs, Volume	= 0.279 af,	Atten= 0%, Lag= 0.0 min

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP5: Analysis Point 5

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	ea =	1.933 ac,	3.46% Impervious,	Inflow Depth = 0.3	78" for 10-YR 24HR event
Inflow	=	1.56 cfs @	12.61 hrs, Volume	= 0.126 af	
Outflow	=	1.56 cfs @	12.61 hrs, Volume	= 0.126 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Pond 1P: Isolated Wetland

[93] Warning: Storage range exceeded by 0.02' [87] Warning: Oscillations may require smaller dt or Finer Routing (severity=26)

Inflow Area	ı =	0.312 ac,	21.51% Imp	ervious,	Inflow Depth	> 2.1	6" for	10-Y	R 24HR e	event
Inflow	=	0.69 cfs @	12.14 hrs,	Volume	= 0.0	56 af				
Outflow	=	0.17 cfs @	12.62 hrs,	Volume	= 0.0	37 af,	Atten=	76%,	Lag= 28.	8 min
Discarded	=	0.03 cfs @	12.67 hrs,	Volume	= 0.0	28 af			-	
Primary	=	0.13 cfs @	12.62 hrs,	Volume	= 0.0	08 af				
Routed	to Reac	h 1R : Flow	[,] Through 9S	i						

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 196.43' @ 12.67 hrs Surf.Area= 2,828 sf Storage= 1,191 cf

Plug-Flow detention time= 272.8 min calculated for 0.037 af (65% of inflow) Center-of-Mass det. time= 168.8 min (1,004.5 - 835.7)

Volume	Inve	ert Avai	I.Storage	Storage Description	n		
#1	195.3	80'	1,191 cf	Custom Stage Dat	ta (Irregular) Listed	below (Recalc)	
Elevatio (fee	on et)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
195.3 196.0 196.4 196.4	30 00 40 41	235 1,050 2,828 2,828	72.0 148.0 211.0 211.0	0 416 747 28	0 416 1,163 1,191	235 1,568 3,369 3,371	
Device	Routing	In	vert Outle	et Devices			
#1	Primary	196	.40' 20.0 Head 2.50 Coel 2.65	' long x 6.0' breadt d (feet) 0.20 0.40 (3.00 3.50 4.00 4. f. (English) 2.37 2.5 2.66 2.66 2.67 2.	th Broad-Crested 0.60 0.80 1.00 1.2 50 5.00 5.50 51 2.70 2.68 2.68 69 2.72 2.76 2.83	Rectangular Weir 20 1.40 1.60 1.80 2.67 2.65 2.65 2	2.00 65
#2	Discarde	d 195	.30' 0.30 Con	0 in/hr Exfiltration ductivity to Groundw	over Surface area vater Elevation = 19	4.80' Phase-In=	0.10'

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Discarded OutFlow Max=0.03 cfs @ 12.67 hrs HW=196.43' (Free Discharge) **2=Exfiltration** (Controls 0.03 cfs)

Primary OutFlow Max=0.13 cfs @ 12.62 hrs HW=196.43' TW=196.42' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir**(Weir Controls 0.13 cfs @ 0.23 fps)

Summary for Pond 2P: Depression in Woods

Inflow Area	a =	1.933 ac,	3.46% Impe	ervious,	Inflow I	Depth >	1.7	7" for	10-Y	R 24H	R event
Inflow	=	2.50 cfs @	12.33 hrs,	Volume	=	0.285	af				
Outflow	=	1.66 cfs @	12.61 hrs,	Volume	=	0.217	af, /	Atten= 3	34%,	Lag= 1	16.7 min
Discarded	=	0.10 cfs @	12.61 hrs,	Volume	=	0.091	af				
Primary	=	1.56 cfs @	12.61 hrs,	Volume	=	0.126	af				
Routed	to Reac	h AP5 : Anal	ysis Point 5								

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 176.50' @ 12.61 hrs Surf.Area= 7,514 sf Storage= 3,954 cf

Plug-Flow detention time= 154.0 min calculated for 0.217 af (76% of inflow) Center-of-Mass det. time= 67.5 min (927.5 - 860.0)

Volume	Inve	ert Avai	I.Storage	Storage Descriptio	n		
#1	175.7	'0'	5,471 cf	Custom Stage Da	ta (Irregular) Listed be	low (Recalc)	
Elevatio (fee	on t)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
175.7	0	2,764	204.0	0	0	2,764	
176.0	0	3,841	265.0	986	986	5,042	
176.4	-0	7,514	341.0	2,230	3,217	8,709	
176.7	0	7,514	341.0	2,254	5,471	8,811	
Device	Routing	In	vert Outle	et Devices			
#1	Primary	176	.40' 20.0 Head 2.50	long x 2.0' bread d (feet) 0.20 0.40 3.00 3.50 f (English) 2.54 2.0	th Broad-Crested Re 0.60 0.80 1.00 1.20	ctangular Weir 1.40 1.60 1.80 2.00	
#2	Discarde	d 175	2.85 5.70' 0.30 Cond	3.07 3.20 3.32 0 in/hr Exfiltration ductivity to Groundw	over Surface area vater Elevation = 175.2	20' Phase-In= 0.10'	

Discarded OutFlow Max=0.10 cfs @ 12.61 hrs HW=176.50' (Free Discharge) **2=Exfiltration** (Controls 0.10 cfs)

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Summary for Pond 3P: Center of Cul De Sac

[63] Warning: Exceeded Reach 3R INLET depth by 1.02' @ 14.25 hrs

 Inflow Area =
 1.875 ac, 21.79% Impervious, Inflow Depth > 1.93" for 10-YR 24HR event

 Inflow =
 2.50 cfs @ 12.12 hrs, Volume=
 0.302 af

 Outflow =
 0.31 cfs @ 14.01 hrs, Volume=
 0.249 af, Atten= 88%, Lag= 113.2 min

 Primary =
 0.31 cfs @ 14.01 hrs, Volume=
 0.249 af

 Routed to Reach 4R : Swale
 0.249 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 192.99' @ 14.01 hrs Surf.Area= 3,113 sf Storage= 6,702 cf

Plug-Flow detention time= 258.8 min calculated for 0.249 af (83% of inflow) Center-of-Mass det. time= 189.1 min (1,022.5 - 833.4)

Volume	Invert	Avail.Stor	age Storage D	escription		
#1	190.00' 16,171 cf		1 cf Custom S	Stage Data (Pris	matic)Listed below (F	Recalc)
Elevation (feet)	Su	rf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
190.00 191.00 192.00 194.00		1,491 1,934 2,483 3,751	0 1,713 2,209 6,234	0 1,713 3,921 10,155		
195.00 195.40		4,514 4,903	4,133 1,883	14,288 16,171		
Device R	Routing	Invert	Outlet Devices			
#1 P	rimary	190.00'	15.0" Round C L= 47.0' CPP, Inlet / Outlet Inv n= 0.012. Flow	Culvert projecting, no he vert= 190.00' / 18 Area= 1.23 sf	eadwall, Ke= 0.900 39.70' S= 0.0064 '/'	Cc= 0.900
#2 D #3 D #4 D)evice 1)evice 1)evice 1	190.00' 191.30' 193.40'	2.0" Vert. Orific 2.0" Vert. Orific 2.0" Vert. Orific	ce/Grate $C = 0.1$ ce/Grate $C = 0.1$ ce/Grate $C = 0.1$	600Limited to weir600Limited to weir600Limited to weir	flow at low heads flow at low heads flow at low heads
#5 D #6 D)evice 1)evice 1	193.65' 194.45'	0.7" W x 9.6" H Limited to weir f 12.0" Horiz. Or Limited to weir f	I Vert. Orifice/G flow at low heads ifice/Grate C= flow at low heads	i rate C= 0.600 s 0.600 s	
Primary O	utFlow Ma	ax=0.31 cfs @	0 14.01 hrs HW	=192.99' TW=18	89.81' (Dynamic Tai	lwater)

1=Culvert (Passes 0.31 cts of 7.18 cts potential flow)

-2=Orifice/Grate (Orifice Controls 0.18 cfs @ 8.21 fps)

-3=Orifice/Grate (Orifice Controls 0.13 cfs @ 6.11 fps)

-4=Orifice/Grate (Controls 0.00 cfs)

-5=Orifice/Grate (Controls 0.00 cfs)

-6=Orifice/Grate (Controls 0.00 cfs)

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Summary for Pond 4P: Drip Edge

Inflow Ar	rea =	0.023 ac,100.0	00% Impervious, Inflow Depth > 4.10" for 10-YR 24HR event
Inflow	=	0.09 cfs @ 12	0.008 at
Discarde	- = bd	0.04 CIS (U) 12 0.03 cfs (0) 12	1.31 ms, volume = 0.006 al, Allen = 57%, Lag = 13.6 mm
Seconda	irv =	0.00 cfs @ 12	2.31 hrs Volume= 0.000 af
Route	ed to Pond	2P : Depressio	n in Woods
Routing I	by Dyn-Sto	r-Ind method, 7	Fime Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3
Peak Ele	ev= 191.50'	@ 12.30 hrs	Surf.Area= 0.004 ac Storage= 0.002 af
Plug-Flov	w detentior	i time= 55.9 mii	n calculated for 0.008 af (99% of inflow)
Center-o	f-Mass det	. time= 49.8 mi	n (799.8 - 750.0)
Volume	Inver	t Avail.Stora	ge Storage Description
#1	189.90	' 0.002	af 3.00'W x 52.00'L x 1.60'H Prismatoid
			0.006 af Overall x 40.0% Voids
Device	Routing	Invert	Outlet Devices
#0	Secondary	/ 191.50'	Automatic Storage Overflow (Discharged without head)
#1	Discarded	189.90'	0.300 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 189.83' Phase-In= 0.10'
Discarde	ed OutFlow	v Max=0.03 cfs	@ 12.30 hrs HW=191.50' (Free Discharge)
Seconda	ary OutFlo	w Max=0.00 cf	s @ 12.31 hrs HW=191.50' TW=176.30' (Dynamic Tailwater)
		S	ummary for Pond 5P: Drip Edge
Inflow Ar	ea =	0.013 ac,100.0	00% Impervious, Inflow Depth > 4.10" for 10-YR 24HR event
Inflow	=	0.06 cfs 🤵 12	.09 hrs, Volume= 0.005 af
Outflow	=	0.02 cfs 🧕 12	.42 hrs, Volume= 0.005 af, Atten= 71%, Lag= 19.8 min
Discarde	ed =	0.02 cfs @ 12	2.42 hrs, Volume= 0.005 af
Seconda	iry =	0.00 cfs @ 0	0.00 hrs, Volume= 0.000 af
Route	ed to Reach	n 4R : Swale	
Routing I	by Dyn-Sto	r-Ind method, I	Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3
Peak Ele	ev= 190.70	@ 12.42 hrs	Sun Area= 0.004 ac Storage= 0.001 al
Plug-Flo	w detention	time=54.7 mi	a calculated for 0.004 af (99% of inflow)
Center-o	f-Mass det	time= 47 3 mi	n (7974 - 7500)
Volume	Inver	t Avail.Stora	ge Storage Description
#1	189.90	' 0.003	af 4.50'W x 41.00'L x 1.60'H Prismatoid
			0.007 af Overall x 40.0% Voids
Device	Routing	Invert	Outlet Devices
#0	Secondary	/ 191.50'	Automatic Storage Overflow (Discharged without head)
#1	Discarded	189.90'	0.300 in/hr Exfiltration over Surface area

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	Conductivity to Groundwater Elevation = 189.83' Phase-In= 0.10'
Discarded OutFlow Max=0.	02 cfs @ 12.42 hrs HW=190.70' (Free Discharge) 0.02 cfs)
Secondary OutFlow Max=0	.00 cfs @ 0.00 hrs HW=189.90' TW=189.70' (Dynamic Tailwater)
	Summary for Pond 6P: Drip Edge
Inflow Area = 0.024 ac, Inflow = 0.10 cfs (Outflow = 0.05 cfs (Discarded = 0.05 cfs (Secondary = 0.00 cfs (Routed to Reach 5R : Flor	(100.00% Impervious, Inflow Depth > 4.10" for 10-YR 24HR event (2) 12.09 hrs, Volume= 0.008 af (2) 12.22 hrs, Volume= 0.008 af, Atten= 46%, Lag= 8.0 min (2) 12.22 hrs, Volume= 0.008 af (2) 12.22 hrs, Volume= 0.008 af (2) 0.00 hrs, Volume= 0.008 af (2) 0.00 hrs, Volume= 0.008 af (2) 0.00 hrs, Volume= 0.000 af (3) 0.000 hrs, Volume= 0.000 af (4) 0.000 hrs, Volume= 0.000 af (4) 0.000 hrs, Volume= 0.000 af
Routing by Dyn-Stor-Ind meth Peak Elev= 189.24' @ 12.22 Plug-Flow detention time= 21 Center-of-Mass det. time= 17	hod, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 hrs Surf.Area= 0.005 ac Storage= 0.001 af I.8 min calculated for 0.008 af (99% of inflow) 7.5 min (767.5 - 750.0)
Volume Invert Avail.	Storage Storage Description
#1 188.52'	0.002 af 4.00'W x 52.00'L x 1.20'H Prismatoid 0.006 af Overall x 40.0% Voids
Device Routing In	vert Outlet Devices
#0 Secondary 189 #1 Discarded 188	 Automatic Storage Overflow (Discharged without head) 0.300 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 188.50' Phase-In= 0.10'
Discarded OutFlow Max=0. ☐_1=Exfiltration (Controls	05 cfs @ 12.22 hrs HW=189.24' (Free Discharge) 0.05 cfs)
Secondary OutFlow Max=0	.00 cfs @ 0.00 hrs HW=188.52' TW=183.50' (Dynamic Tailwater)
coordination wax-0	
	Summary for Pond 7P: Drip Edge

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 190.52' @ 15.03 hrs Surf.Area= 0.002 ac Storage= 0.002 af

Plug-Flow detention time= 315.9 min calculated for 0.002 af (57% of inflow) Center-of-Mass det. time= 202.4 min (952.5 - 750.0)

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Volume Invert Avail.Storage Storage Description
#1 188.00 0.004 at 2.50 W X 41.00 L X 4.00 H Prismatold 0.009 af Overall x 40.0% Voids
Device Routing Invert Outlet Devices
#0Secondary192.00'Automatic Storage Overflow (Discharged without head)#1Discarded188.00'0.300 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 186.50'Phase-In= 0.10'
Discarded OutFlow Max=0.00 cfs @ 15.03 hrs HW=190.52' (Free Discharge)
Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=188.00' TW=189.70' (Dynamic Tailwater)
Summary for Pond 8P: Drip Edge
Inflow Area = 0.012 ac,100.00% Impervious, Inflow Depth > 4.10" for 10-YR 24HR event Inflow = 0.05 cfs @ 12.09 hrs, Volume= 0.004 af Outflow = 0.01 cfs @ 12.48 hrs, Volume= 0.004 af, Atten= 77%, Lag= 23.4 min Discarded = 0.01 cfs @ 12.48 hrs, Volume= 0.004 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Routed to Reach AP1 : Analysis Point 1 0.000 af 0.000 af
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 188.84' @ 12.48 hrs Surf.Area= 0.003 ac Storage= 0.001 af
Plug-Flow detention time= 74.4 min calculated for 0.004 af (99% of inflow) Center-of-Mass det. time= 66.9 min (816.9 - 750.0)
Volume Invert Avail.Storage Storage Description
#1 187.60' 0.003 af 3.00'W x 41.00'L x 2.40'H Prismatoid 0.007 af Overall x 40.0% Voids
Device Routing Invert Outlet Devices
#0Secondary #1190.00'Automatic Storage Overflow (Discharged without head)#1Discarded187.60'0.300 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 187.50'Phase-In= 0.10'
Discarded OutFlow Max=0.01 cfs @ 12.48 hrs HW=188.84' (Free Discharge) -1=Exfiltration (Controls 0.01 cfs)
Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=187.60' TW=0.00' (Dynamic Tailwater)
Summary for Pond 10P: Drip Edge
Inflow Area = 0.024 ac,100.00% Impervious, Inflow Depth > 4.10" for 10-YR 24HR event Inflow = 0.10 cfs @ 12.09 hrs, Volume= 0.008 af Outflow = 0.02 cfs @ 12.52 hrs, Volume= 0.008 af, Atten= 80%, Lag= 25.8 min Discarded = 0.00 cfs @ 12.52 hrs, Volume= 0.008 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routed to Reach 3R : Culvert

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Routing	by Dyn-Stor-I	nd method, ⁻	Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3			
Peak El	ev= 194.43' @) 12.52 hrs	Surf.Area= 0.005 ac Storage= 0.003 af			
Plug-Flo	ow detention ti	me= 95.8 mi	in calculated for 0.008 af (99% of inflow)			
Center-o	of-Mass det. ti	me= 88.0 mi	in(838.1-750.0)			
volume #1			age Storage Description			
<i>#</i> I	192.00	0.000	0.015 af Overall x 40.0% Voids			
Device	Routing	Invert	Outlet Devices			
#0	Secondary	196.00'	Automatic Storage Overflow (Discharged without head)0.300 in/hr Exfiltration over Surface areaConductivity to Groundwater Elevation = 192.67'Phase-In= 0.10'			
#1	Discarded	192.80'				
Discard	Discarded OutFlow Max=0.02 cfs @ 12.52 hrs HW=194.43' (Free Discharge)					
¹ —1=Ex	1=Exfiltration (Controls 0.02 cfs)					
Second	lary OutFlow	Max=0.00 ct	fs @ 0.00 hrs HW=192.80' TW=191.80' (Dynamic Tailwater)			

Summary for Pond 11P: Drip Edge

Inflow Area =	0.011 ac,10	0.00% Impervious,	Inflow Depth > 4.	10" for 10-YR 24HR event
Inflow =	0.05 cfs @	12.09 hrs, Volume	e= 0.004 af	
Outflow =	0.02 cfs @	12.27 hrs, Volume	e= 0.004 af,	Atten= 55%, Lag= 10.9 min
Discarded =	0.02 cfs @	12.27 hrs, Volume	e= 0.004 af	-
Secondary =	0.00 cfs @	0.00 hrs, Volume	e= 0.000 af	
Routed to Reac	h 3R : Culve	ert		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 194.56' @ 12.27 hrs Surf.Area= 0.002 ac Storage= 0.001 af

Plug-Flow detention time= 28.9 min calculated for 0.004 af (99% of inflow) Center-of-Mass det. time= 23.8 min (773.9 - 750.0)

Volume	Invert	Avail.Storag	ge Storage Description		
#1	193.70'	0.002	af 2.50'W x 41.00'L x 2.30'H Prismatoid 0.005 af Overall x 40.0% Voids		
Device	Routing	Invert	Outlet Devices		
#0	Secondary	196.00'	Automatic Storage Overflow (Discharged without head)		
#1	Discarded	193.70'	0.300 in/hr Exfiltration over Surface area		
			Conductivity to Groundwater Elevation = 193.67' Phase-In= 0.10'		
Discarded OutFlow Max=0.02 cfs @ 12.27 hrs HW=194.56' (Free Discharge)					

1=Exfiltration (Controls 0.02 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=193.70' TW=191.80' (Dynamic Tailwater)

22201-PROPOSED	Type III 24-hr	10-YR 24HR Rail	nfall=4.34'
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Summary for Pond 20P: Barn

Inflow A	rea =	0.055 ac,100.0	0% Impervious, Inflow Depth > 4.10" for 10-YR 24HR event		
Inflow	=	0.23 cfs @ 12.	09 hrs, Volume= 0.019 at		
Discord	=	0.04 CIS @ 12.	54 hrs, Volume= 0.018 al, Allen= 82%, Lag= 27.2 min 54 hrs, Volume= 0.018 af		
Second	eu – arv –	0.04 CIS @ 12.	00 brs Volume = 0.000 af		
Rout	Pouted to Pooch AP2 : Apolycic Point 2				
Rout		TAI 0 . Analysis			
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 170 29' @ 12 54 hrs_Surf Area= 0.009 ac_Storage= 0.007 af					
Plug-Flow detention time= 113.1 min calculated for 0.018 af (99% of inflow) Center-of-Mass det. time= 105.2 min (855.2 - 750.0)					
Volume	Inver	t Avail.Storag	ge Storage Description		
#1	168.15	0.013	af 4.00'W x 95.00'L x 3.85'H Prismatoid 0.034 af Overall x 40.0% Voids		
Device	Routing	Invert	Outlet Devices		
#0	Secondary	/ 172.00'	Automatic Storage Overflow (Discharged without head)		
#1	Discarded	168.15'	0.300 in/hr Exfiltration over Surface area		
			Conductivity to Groundwater Elevation = 168.00' Phase-In= 0.10'		
Discarded OutFlow Max=0.04 cfs @ 12.54 hrs HW=170.29' (Free Discharge)					
Second	Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=168.15' TW=0.00' (Dynamic Tailwater)				
Summary for Pond 22P: Barn					
			•		
Inflow A	rea =	0.055 ac,100.0	0% Impervious, Inflow Depth > 4.10" for 10-YR 24HR event		
Inflow	=	0.23 cfs @ 12.	09 hrs, Volume= 0.019 af		
Outflow	=	0.04 cfs @ 12.	54 hrs, Volume= 0.018 af, Atten= 82%, Lag= 27.2 min		
Discarde	ed =	0.04 cfs @ 12.	54 hrs, Volume= 0.018 af		
Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af					
Rout	ed to Reach	n AP3 : Analysis	Point 3		
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3					
Peak El	ev= 170.29	@ 12.54 hrs S	Surf.Area= 0.009 ac Storage= 0.007 at		
Plug-Flow detention time= 113.1 min calculated for 0.018 af (99% of inflow) Center-of-Mass det. time= 105.2 min (855.2 - 750.0)					
<u>Volum</u> e	Inver	t Avail.Storac	ge Storage Description		
#1	168.15	0.013	af 4.00'W x 95.00'L x 3.85'H Prismatoid 0.034 af Overall x 40.0% Voids		
Device	Routing	Invert	Outlet Devices		
#0	Secondary	/ 172.00'	Automatic Storage Overflow (Discharged without head)		
#1	Discarded	168.15'	0.300 in/hr Exfiltration over Surface area		
22201-PROPOSED	Type III 24-hr	10-YR 24HR Rainfall=4.34"			
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Conductivity to Groundwater Elevation = 168.00' Phase-In= 0.10'

Discarded OutFlow Max=0.04 cfs @ 12.54 hrs HW=170.29' (Free Discharge) **1=Exfiltration** (Controls 0.04 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=168.15' TW=0.00' (Dynamic Tailwater)

Summary for Pond 23P: Drip Edge

Inflow Ar Inflow Outflow Discarde Seconda Route	ea = = = ed = iry = ed to React	0.013 ac, 15.85 0.04 cfs @ 12. 0.00 cfs @ 14. 0.00 cfs @ 14. 0.00 cfs @ 0. n AP3 : Analysis	5% Impervious, Inflow Depth > 2.76" for 10-YR 24HR event 09 hrs, Volume= 0.003 af 69 hrs, Volume= 0.002 af, Atten= 95%, Lag= 156.0 min 69 hrs, Volume= 0.002 af 00 hrs, Volume= 0.000 af Point 3			
Routing I Peak Ele	by Dyn-Sto ev= 170.56'	r-Ind method, Ti @ 14.69 hrs S	ime Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Surf.Area= 0.003 ac Storage= 0.002 af			
Plug-Flov Center-o	w detentior f-Mass det	n time= 311.5 mi . time= 215.7 mi	n calculated for 0.002 af (69% of inflow) n(1,028.3 - 812.6)			
volume	Inver	t Avall.Storag	e Storage Description			
#1	169.00	' 0.003 a	af 3.00'W x 40.00'L x 3.00'H Prismatoid 0.008 af Overall x 40.0% Voids			
Device	Routina	Invert	Outlet Devices			
#0 #1	Secondary Discarded	y 172.00' 169.00'	Automatic Storage Overflow (Discharged without head) 0.300 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 168.00' Phase-In= 0.10'			
Discarded OutFlow Max=0.00 cfs @ 14.69 hrs HW=170.56' (Free Discharge) ←1=Exfiltration (Controls 0.00 cfs)						
Seconda	Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=169.00' TW=0.00' (Dynamic Tailwater)					
	Summary for Pond 24P: Plunge Pool with Culvert Outlet					

Inflow Area	a =	0.213 ac, 1	8.90% Imperv	vious, Inflow	Depth >	2.24"	for 10-Y	'R 24HR event
Inflow	=	0.48 cfs @	12.15 hrs, Vo	olume=	0.040	af		
Outflow	=	0.48 cfs @	12.16 hrs, Vo	olume=	0.040 a	af, Atte	n= 0%, I	_ag= 0.6 min
Primary	=	0.48 cfs @	12.16 hrs, Vo	olume=	0.040 a	af		
Routed	to Reac	h 3R : Culve	rt					

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 193.32' @ 12.16 hrs Surf.Area= 106 sf Storage= 25 cf

Plug-Flow detention time= 2.1 min calculated for 0.040 af (100% of inflow) Center-of-Mass det. time= 1.4 min (835.0 - 833.6)

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Volume	Invert	Avail Stor	age Storad	e Description				
#1	193.00'	47	5 cf Custo	m Stage Data	(Prismatic)	Listed below	w (Recalc)	
Elevation	5 Su	rf Area	Inc Store	Cum Stor				
(feet	i Su)	(sɑ-ft)	(cubic-feet)	(cubic-fee	et)			
193.00)	51	0	(00.010 100	0			
194.00)	222	137	13	37			
195.00)	455	339	47	'5			
Device	Routing	Invert	Outlet Devi	ces				
#1	Primary	193.00'	15.0" Rou	nd Culvert				
			L= 50.0' C	PP, square edg	e headwall	Ke= 0.500)	
			Inlet / Outle n=0.012 F	t Invert= 193.00 low Area= 1 23)' / 192.50' } sf	S= 0.0100	'/' Cc= 0.9	000
				101171100 1.20				
Primary 1=Cul	OutFlow Ma vert (Inlet C	ax=0.47 cfs @ Controls 0.47	0 12.16 hrs cfs @ 1.92 f	HW=193.32' T\ bs)	W=192.23'	(Dynamic	Tailwater)	
		S	ummary fo	or Pond 25P:	: Drip Edg	je		
Inflow Are	ea = 0	.012 ac,100.0	0% Impervio	ous, Inflow Dep	oth > 4.10"	for 10-Y	R 24HR eve	ent
nflow	= 0.	05 cfs @ 12	2.09 hrs, Vol	ume= 0).004 af			
Dutflow	= 0.	01 cfs @ 12	2.44 hrs, Vol	ume= 0).004 af, At	ten= 73%,	Lag= 21.3 i	min
Discardeo Secondai	u = 0. 1 = 0.	01 CTS @ 12	2.44 Nrs, Vol 100 brs Vol	ume= 0 ume= 0).004 af) 000 af			
Route	d to Reach	SR : Flow Thr	ough 5S					
Douting k	NU DUD Stor	Ind mothod]	Time Span-	0 00 24 00 bra	dt- 0.05 hr	o / 2		
Peak Ele	v= 194.90' @	0 12.44 hrs	Surf.Area= 0	.003 ac Storad	de= 0.001 a	s/S f		
			-					
Plug-Flov	v detention t	ime= 61.8 mii ime= 54.7 mii	n calculated	for 0.004 af (99	% of inflow			
Senter-Or	-111855 UCL 1	1116- 34.7 111	11 (004.7 - 7.	50.0)				
Volume	Invert	Avail.Stora	ge Storage	Description				
#1	193.75'	0.003	af 3.00'W 0.006 a	x 41.00'L x 2.2 f Overall x 40.0	2 5'H Prisma 0% Voids	toid		
Device	Routing	Invert	Outlet Devi	ces				
#0	Secondary	196.00'	Automatic	Storage Overf	low (Discha	arged witho	ut head)	
#1	Discarded	193.75'	0.300 in/hr Conductivity	Exfiltration ov to Groundwate	er Surface er Elevation	area = 193.67'	Phase-In:	= 0.10'
	d OutFlow	Max=0.01 cfs	s @ 12.44 hr	s HW=194.90'	(Free Disc	harge)		
Discarde └──1=Exf	iltration (C	ontrols 0.01 d	cfs)		·	5 /		
Qiscarde ──1=Exf	iltration (C	ontrols 0.01 c	ofs)			3,		

22201-PROPOSED	Type III 24-hr	25-YR 24HR Rail	nfall=5.47"
Prepared by Jones & Beach Engineers Inc		Printed	3/22/2024
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			-

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: 1S	Runoff Area=97,026 sf 2.11% Impervious Runoff Depth>2.64" Flow Length=320' Tc=19.9 min CN=73 Runoff=4.64 cfs 0.491 af
Subcatchment2S: 2S	Runoff Area=66,576 sf 0.00% Impervious Runoff Depth>2.47" Flow Length=290' Tc=18.2 min CN=71 Runoff=3.07 cfs 0.314 af
Subcatchment3S: 3S Flow Lengt	Runoff Area=39,339 sf 0.00% Impervious Runoff Depth>2.47" h=140' Slope=0.0123 '/' Tc=19.1 min CN=71 Runoff=1.78 cfs 0.186 af
Subcatchment4S: 4S	Runoff Area=27,185 sf 0.00% Impervious Runoff Depth>1.43" Flow Length=194' Tc=23.6 min CN=58 Runoff=0.59 cfs 0.074 af
Subcatchment5S: 5S	Runoff Area=113,462 sf 0.00% Impervious Runoff Depth>2.04" Flow Length=602' Tc=32.4 min CN=66 Runoff=3.31 cfs 0.443 af
Subcatchment6S: 6S Flow Ler	Runoff Area=13,598 sf 21.51% Impervious Runoff Depth>3.11" ngth=92' Slope=0.0217 '/' Tc=9.3 min CN=78 Runoff=1.00 cfs 0.081 af
Subcatchment7S: 7S	Runoff Area=84,203 sf 3.46% Impervious Runoff Depth>2.64" Flow Length=456' Tc=23.1 min CN=73 Runoff=3.78 cfs 0.426 af
Subcatchment9S: 9S	Runoff Area=41,089 sf 6.98% Impervious Runoff Depth>2.82" Flow Length=211' Tc=22.8 min CN=75 Runoff=1.99 cfs 0.222 af
Subcatchment10S: 10S	Runoff Area=17,686 sf 57.92% Impervious Runoff Depth>4.11" Tc=6.0 min CN=88 Runoff=1.86 cfs 0.139 af
Subcatchment11S: 11S	Runoff Area=9,293 sf 18.90% Impervious Runoff Depth>3.20" Flow Length=194' Tc=10.2 min CN=79 Runoff=0.69 cfs 0.057 af
Subcatchment12S: Units 5&6	Runoff Area=994 sf 100.00% Impervious Runoff Depth>5.23" Tc=6.0 min CN=98 Runoff=0.12 cfs 0.010 af
Subcatchment13S: Unit 5	Runoff Area=580 sf 100.00% Impervious Runoff Depth>5.23" Tc=6.0 min CN=98 Runoff=0.07 cfs 0.006 af
Subcatchment14S: Units 3&4	Runoff Area=1,046 sf 100.00% Impervious Runoff Depth>5.23" Tc=6.0 min CN=98 Runoff=0.13 cfs 0.010 af
Subcatchment15S: Unit 4	Runoff Area=498 sf 100.00% Impervious Runoff Depth>5.23" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af
Subcatchment16S: Unit 3	Runoff Area=518 sf 100.00% Impervious Runoff Depth>5.23" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af
Subcatchment17S: Units 1&2	Runoff Area=1,046 sf 100.00% Impervious Runoff Depth>5.23" Tc=6.0 min CN=98 Runoff=0.13 cfs 0.010 af

22201-PROPOSED Prepared by Jones & Beach Engine HydroCAD® 10.20-3c s/n 00762 © 2023	Type III 24-hr 25-YR 24HR Rainfall=5.47"ers IncPrinted 3/22/2024HydroCAD Software Solutions LLCPage 35
Subcatchment18S: Unit 1	Runoff Area=498 sf 100.00% Impervious Runoff Depth>5.23" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af
Subcatchment19S: 19S	Runoff Area=2,375 sf 100.00% Impervious Runoff Depth>5.23" Tc=6.0 min CN=98 Runoff=0.29 cfs 0.024 af
Subcatchment20S: 20S	Runoff Area=2,375 sf 100.00% Impervious Runoff Depth>5.23" Tc=6.0 min CN=98 Runoff=0.29 cfs 0.024 af
Subcatchment21S: Gravel Trail	Runoff Area=574 sf 15.85% Impervious Runoff Depth>3.80" Tc=6.0 min CN=85 Runoff=0.06 cfs 0.004 af
Subcatchment22S: Unit 2	Runoff Area=518 sf 100.00% Impervious Runoff Depth>5.23" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af
Reach 1R: Flow Through 9S n=0.030	Avg. Flow Depth=0.07' Max Vel=1.20 fps Inflow=1.36 cfs 0.030 af L=140.0' S=0.0329 '/' Capacity=43.14 cfs Outflow=0.70 cfs 0.030 af
Reach 3R: Culvert 15.0" Round Pipe n=0.01	Avg. Flow Depth=0.68' Max Vel=4.62 fps Inflow=3.14 cfs 0.308 af 2 L=49.0' S=0.0061 '/' Capacity=5.48 cfs Outflow=3.16 cfs 0.308 af
Reach 4R: Swale n=0.030	Avg. Flow Depth=0.14' Max Vel=2.52 fps Inflow=0.50 cfs 0.363 af L=120.0' S=0.0517 '/' Capacity=30.09 cfs Outflow=0.50 cfs 0.363 af
Reach 5R: Flow Through 1S n=0.030	Avg. Flow Depth=0.06' Max Vel=1.27 fps Inflow=0.50 cfs 0.363 af L=191.0' S=0.0497 '/' Capacity=53.08 cfs Outflow=0.50 cfs 0.362 af
Reach 6R: Flow Through 5S n=0.030	Avg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af L=600.0' S=0.0367 '/' Capacity=45.58 cfs Outflow=0.00 cfs 0.000 af
Reach AP1: Analysis Point 1	Inflow=7.98 cfs 1.167 af Outflow=7.98 cfs 1.167 af
Reach AP2: Analysis Point 2	Inflow=1.78 cfs 0.186 af Outflow=1.78 cfs 0.186 af
Reach AP3: Analysis Point 3	Inflow=0.59 cfs 0.074 af Outflow=0.59 cfs 0.074 af
Reach AP4: Analysis Point 4	Inflow=3.31 cfs 0.443 af Outflow=3.31 cfs 0.443 af
Reach AP5: Analysis Point 5	Inflow=3.28 cfs 0.258 af Outflow=3.28 cfs 0.258 af
Pond 1P: Isolated Wetland Discarded=0	Peak Elev=196.51' Storage=1,191 cf Inflow=1.00 cfs 0.081 af .03 cfs 0.030 af Primary=1.36 cfs 0.030 af Outflow=1.39 cfs 0.059 af
Pond 2P: Depression in Woods Discarded=0	Peak Elev=176.56' Storage=4,425 cf Inflow=3.81 cfs 0.427 af .10 cfs 0.095 af Primary=3.28 cfs 0.258 af Outflow=3.38 cfs 0.353 af

22201-PROPOSED Prepared by Jones & <u>HydroCAD® 10.20-3c</u> s/	Beach Engineers n 00762 © 2023 Hydr	Inc roCAD So	Type III 24-hr 25-YR	24HR Rainfa Printed 3/	all=5.47" 22/2024 Page <u>36</u>
Pond 3P: Center of Cu	Il De Sac	Peak I	Elev=194.03' Storage=10,272 cf Ir Ou	nflow=3.98 cfs tflow=0.50 cfs	0.448 af 0.363 af
Pond 4P: Drip Edge	Discarded=0.03 cfs	Peak 0.009 af	Elev=191.50' Storage=0.002 af Ir Secondary=0.08 cfs 0.001 af Out	nflow=0.12 cfs flow=0.10 cfs(0.010 af 0.010 af
Pond 5P: Drip Edge	Discarded=0.02 cfs	Peak 0.006 af	Elev=190.92' Storage=0.002 af Ir Secondary=0.00 cfs 0.000 af Out	nflow=0.07 cfs flow=0.02 cfs(0.006 af 0.006 af
Pond 6P: Drip Edge	Discarded=0.07 cfs	Peak 0.010 af	Elev=189.44' Storage=0.002 af Ir Secondary=0.00 cfs 0.000 af Out	nflow=0.13 cfs flow=0.07 cfs(0.010 af 0.010 af
Pond 7P: Drip Edge	Discarded=0.00 cfs	Peak 0.003 af	Elev=191.31' Storage=0.003 af Ir Secondary=0.00 cfs 0.000 af Out	nflow=0.06 cfs flow=0.00 cfs(0.005 af 0.003 af
Pond 8P: Drip Edge	Discarded=0.01 cfs	Peak 0.005 af	Elev=189.19' Storage=0.002 af Ir Secondary=0.00 cfs 0.000 af Out	nflow=0.06 cfs flow=0.01 cfs(0.005 af 0.005 af
Pond 10P: Drip Edge	Discarded=0.02 cfs	Peak 0.010 af	Elev=194.89' Storage=0.004 af Ir Secondary=0.00 cfs 0.000 af Out	nflow=0.13 cfs flow=0.02 cfs(0.010 af 0.010 af
Pond 11P: Drip Edge	Discarded=0.03 cfs	Peak 0.005 af	Elev=194.80' Storage=0.001 af Ir Secondary=0.00 cfs 0.000 af Out	nflow=0.06 cfs flow=0.03 cfs(0.005 af 0.005 af
Pond 20P: Barn	Discarded=0.05 cfs	Peak 0.023 af	Elev=170.90' Storage=0.010 af Ir Secondary=0.00 cfs 0.000 af Out	nflow=0.29 cfs flow=0.05 cfs(0.024 af 0.023 af
Pond 22P: Barn	Discarded=0.05 cfs	Peak 0.023 af	Elev=170.90' Storage=0.010 af Ir Secondary=0.00 cfs 0.000 af Out	nflow=0.29 cfs flow=0.05 cfs(0.024 af 0.023 af
Pond 23P: Drip Edge	Discarded=0.00 cfs	Peak 0.003 af	Elev=171.23' Storage=0.002 af Ir Secondary=0.00 cfs 0.000 af Out	nflow=0.06 cfs flow=0.00 cfs(0.004 af 0.003 af
Pond 24P: Plunge Poo	ol with Culvert Outle 15.0" Round	et Pe d Culvert	eak Elev=193.39' Storage=33 cf Ir n=0.012 L=50.0' S=0.0100 '/' Out	nflow=0.69 cfs tflow=0.69 cfs	0.057 af 0.057 af
Pond 25P: Drip Edge	Discarded=0.02 cfs	Peak 0.005 af	Elev=195.22' Storage=0.002 af Ir Secondary=0.00 cfs 0.000 af Out	nflow=0.06 cfs flow=0.02 cfs(0.005 af 0.005 af
Total R	unoff Area = 11.949	ac Ru	noff Volume = 2.541 af Averag	ge Runoff Der	oth = 2.55"

93.60% Pervious = 11.184 ac 6.40% Impervious = 0.764 ac

22201-PROPOSED	Type III 24-hr	50-YR 24HR Rainfall=6.51"
Prepared by Jones & Beach Engineers Inc		Printed 3/22/2024
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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: 1S	Runoff Area=97,026 sf 2.11% Impervious Runoff Depth>3.50" Flow Length=320' Tc=19.9 min CN=73 Runoff=6.17 cfs 0.650 af
Subcatchment2S: 2S	Runoff Area=66,576 sf 0.00% Impervious Runoff Depth>3.30" Flow Length=290' Tc=18.2 min CN=71 Runoff=4.14 cfs 0.421 af
Subcatchment3S: 3S Flow Length=14	Runoff Area=39,339 sf 0.00% Impervious Runoff Depth>3.30" 0' Slope=0.0123 '/' Tc=19.1 min CN=71 Runoff=2.40 cfs 0.249 af
Subcatchment4S: 4S	Runoff Area=27,185 sf 0.00% Impervious Runoff Depth>2.07" Flow Length=194' Tc=23.6 min CN=58 Runoff=0.90 cfs 0.108 af
Subcatchment5S: 5S	Runoff Area=113,462 sf 0.00% Impervious Runoff Depth>2.80" Flow Length=602' Tc=32.4 min CN=66 Runoff=4.63 cfs 0.609 af
Subcatchment6S: 6S Flow Length=	Runoff Area=13,598 sf 21.51% Impervious Runoff Depth>4.03" 92' Slope=0.0217 '/' Tc=9.3 min CN=78 Runoff=1.29 cfs 0.105 af
Subcatchment7S: 7S	Runoff Area=84,203 sf 3.46% Impervious Runoff Depth>3.50" Flow Length=456' Tc=23.1 min CN=73 Runoff=5.05 cfs 0.564 af
Subcatchment9S: 9S	Runoff Area=41,089 sf 6.98% Impervious Runoff Depth>3.70" Flow Length=211' Tc=22.8 min CN=75 Runoff=2.62 cfs 0.291 af
Subcatchment10S: 10S	Runoff Area=17,686 sf 57.92% Impervious Runoff Depth>5.11" Tc=6.0 min CN=88 Runoff=2.29 cfs 0.173 af
Subcatchment11S: 11S	Runoff Area=9,293 sf 18.90% Impervious Runoff Depth>4.13" Flow Length=194' Tc=10.2 min CN=79 Runoff=0.89 cfs 0.073 af
Subcatchment12S: Units 5&6	Runoff Area=994 sf 100.00% Impervious Runoff Depth>6.27" Tc=6.0 min CN=98 Runoff=0.14 cfs 0.012 af
Subcatchment13S: Unit 5	Runoff Area=580 sf 100.00% Impervious Runoff Depth>6.27" Tc=6.0 min CN=98 Runoff=0.08 cfs 0.007 af
Subcatchment14S: Units 3&4	Runoff Area=1,046 sf 100.00% Impervious Runoff Depth>6.27" Tc=6.0 min CN=98 Runoff=0.15 cfs 0.013 af
Subcatchment15S: Unit 4	Runoff Area=498 sf 100.00% Impervious Runoff Depth>6.27" Tc=6.0 min CN=98 Runoff=0.07 cfs 0.006 af
Subcatchment16S: Unit 3	Runoff Area=518 sf 100.00% Impervious Runoff Depth>6.27" Tc=6.0 min CN=98 Runoff=0.07 cfs 0.006 af
Subcatchment17S: Units 1&2	Runoff Area=1,046 sf 100.00% Impervious Runoff Depth>6.27" Tc=6.0 min CN=98 Runoff=0.15 cfs 0.013 af

22201-PROPOSED Prepared by Jones & Beach Engine HydroCAD® 10.20-3c s/n 00762 © 2023	Type III 24-hr 50-YR 24HR Rainfall=6.51"ers IncPrinted 3/22/2024HydroCAD Software Solutions LLCPage 38
Subcatchment18S: Unit 1	Runoff Area=498 sf 100.00% Impervious Runoff Depth>6.27" Tc=6.0 min CN=98 Runoff=0.07 cfs 0.006 af
Subcatchment19S: 19S	Runoff Area=2,375 sf 100.00% Impervious Runoff Depth>6.27" Tc=6.0 min CN=98 Runoff=0.34 cfs 0.028 af
Subcatchment20S: 20S	Runoff Area=2,375 sf 100.00% Impervious Runoff Depth>6.27" Tc=6.0 min CN=98 Runoff=0.34 cfs 0.028 af
Subcatchment21S: Gravel Trail	Runoff Area=574 sf 15.85% Impervious Runoff Depth>4.78" Tc=6.0 min CN=85 Runoff=0.07 cfs 0.005 af
Subcatchment22S: Unit 2	Runoff Area=518 sf 100.00% Impervious Runoff Depth>6.27" Tc=6.0 min CN=98 Runoff=0.07 cfs 0.006 af
Reach 1R: Flow Through 9S n=0.030	Avg. Flow Depth=0.10' Max Vel=1.45 fps Inflow=2.18 cfs 0.051 af L=140.0' S=0.0329 '/' Capacity=43.14 cfs Outflow=1.35 cfs 0.051 af
Reach 3R: Culvert 15.0" Round Pipe n=0.01	Avg. Flow Depth=0.83' Max Vel=4.92 fps Inflow=4.15 cfs 0.415 af 2 L=49.0' S=0.0061 '/' Capacity=5.48 cfs Outflow=4.23 cfs 0.415 af
Reach 4R: Swale n=0.030	Avg. Flow Depth=0.24' Max Vel=3.36 fps Inflow=1.37 cfs 0.483 af L=120.0' S=0.0517 '/' Capacity=30.09 cfs Outflow=1.37 cfs 0.483 af
Reach 5R: Flow Through 1S n=0.030	Avg. Flow Depth=0.09' Max Vel=1.72 fps Inflow=1.37 cfs 0.483 af L=191.0' S=0.0497 '/' Capacity=53.08 cfs Outflow=1.37 cfs 0.482 af
Reach 6R: Flow Through 5S n=0.030	Avg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af L=600.0' S=0.0367 '/' Capacity=45.58 cfs Outflow=0.00 cfs 0.000 af
Reach AP1: Analysis Point 1	Inflow=10.64 cfs 1.552 af Outflow=10.64 cfs 1.552 af
Reach AP2: Analysis Point 2	Inflow=2.40 cfs 0.249 af Outflow=2.40 cfs 0.249 af
Reach AP3: Analysis Point 3	Inflow=0.90 cfs 0.108 af Outflow=0.90 cfs 0.108 af
Reach AP4: Analysis Point 4	Inflow=4.63 cfs 0.609 af Outflow=4.63 cfs 0.609 af
Reach AP5: Analysis Point 5	Inflow=4.72 cfs 0.392 af Outflow=4.72 cfs 0.392 af
Pond 1P: Isolated Wetland Discarded=0	Peak Elev=196.56' Storage=1,191 cf Inflow=1.29 cfs 0.105 af .03 cfs 0.032 af Primary=2.18 cfs 0.051 af Outflow=2.21 cfs 0.081 af
Pond 2P: Depression in Woods Discarded=0	Peak Elev=176.61' Storage=4,758 cf Inflow=5.08 cfs 0.566 af .11 cfs 0.099 af Primary=4.72 cfs 0.392 af Outflow=4.83 cfs 0.491 af

22201-PROPOSED Prepared by Jones & <u>HydroCAD® 10.20-3c</u> s/	Beach Engineers n 00762 © 2023 Hydr	Inc roCAD Sc	Type III 24-hr 50-	YR 24HR Rainf Printed 3	ā ll=6 .51" /22/2024 <u>Page 39</u>
Pond 3P: Center of Cu	Il De Sac	Peak I	Elev=194.61' Storage=12,602 c	f Inflow=5.75 cfs Outflow=1.37 cfs	0.588 af 0.483 af
Pond 4P: Drip Edge	Discarded=0.03 cfs	Peak 0.010 af	Elev=191.50' Storage=0.002 a Secondary=0.12 cfs 0.002 af	f Inflow=0.14 cfs Outflow=0.14 cfs	0.012 af 0.012 af
Pond 5P: Drip Edge	Discarded=0.02 cfs	Peak 0.007 af	Elev=191.13' Storage=0.002 a Secondary=0.00 cfs 0.000 af	f Inflow=0.08 cfs Outflow=0.02 cfs	0.007 af 0.007 af
Pond 6P: Drip Edge	Discarded=0.08 cfs	Peak 0.012 af	Elev=189.62' Storage=0.002 a Secondary=0.00 cfs 0.000 af	f Inflow=0.15 cfs Outflow=0.08 cfs	0.013 af 0.012 af
Pond 7P: Drip Edge	Discarded=0.00 cfs	Peak 0.003 af	Elev=192.00' Storage=0.004 a Secondary=0.00 cfs 0.000 af	f Inflow=0.07 cfs Outflow=0.00 cfs	0.006 af 0.003 af
Pond 8P: Drip Edge	Discarded=0.02 cfs	Peak 0.006 af	Elev=189.52' Storage=0.002 a Secondary=0.00 cfs 0.000 af	f Inflow=0.07 cfs Outflow=0.02 cfs	0.006 af 0.006 af
Pond 10P: Drip Edge	Discarded=0.03 cfs	Peak 0.012 af	Elev=195.32' Storage=0.005 a Secondary=0.00 cfs 0.000 af	f Inflow=0.15 cfs Outflow=0.03 cfs	0.013 af 0.012 af
Pond 11P: Drip Edge	Discarded=0.03 cfs	Peak 0.006 af	Elev=195.02' Storage=0.001 a Secondary=0.00 cfs 0.000 af	f Inflow=0.07 cfs Outflow=0.03 cfs	0.006 af 0.006 af
Pond 20P: Barn	Discarded=0.06 cfs	Peak 0.028 af	Elev=171.46' Storage=0.012 a Secondary=0.00 cfs 0.000 af	f Inflow=0.34 cfs Outflow=0.06 cfs	0.028 af 0.028 af
Pond 22P: Barn	Discarded=0.06 cfs	Peak 0.028 af	Elev=171.46' Storage=0.012 a Secondary=0.00 cfs 0.000 af	f Inflow=0.34 cfs Outflow=0.06 cfs	0.028 af 0.028 af
Pond 23P: Drip Edge	Discarded=0.00 cfs	Peak 0.003 af	Elev=171.87' Storage=0.003 a Secondary=0.00 cfs 0.000 af	f Inflow=0.07 cfs Outflow=0.00 cfs	0.005 af 0.003 af
Pond 24P: Plunge Poo	ol with Culvert Outle 15.0" Round	e t Pe d Culvert	eak Elev=193.44' Storage=39 c n=0.012 L=50.0' S=0.0100 '/'	f Inflow=0.89 cfs Outflow=0.88 cfs	0.073 af 0.073 af
Pond 25P: Drip Edge	Discarded=0.02 cfs	Peak 0.006 af	Elev=195.52' Storage=0.002 a Secondary=0.00 cfs 0.000 af	f Inflow=0.07 cfs Outflow=0.02 cfs	0.006 af 0.006 af
Total R	unoff Area = 11.949	ac Ru	noff Volume = 3.372 af Ave	erage Runoff De	pth = 3.39"

93.60% Pervious = 11.184 ac 6.40% Impervious = 0.764 ac

22201-PROPOSED	Type III 24-hr	100-YR 24HR Rainfall=7.77"
Prepared by Jones & Beach Engineers Inc		Printed 3/22/2024
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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: 1S	Runoff Area=97,026 sf 2.11% Impervious Runoff Depth>4.59" Flow Length=320' Tc=19.9 min CN=73 Runoff=8.11 cfs 0.852 af
Subcatchment2S: 2S	Runoff Area=66,576 sf 0.00% Impervious Runoff Depth>4.37" Flow Length=290' Tc=18.2 min CN=71 Runoff=5.49 cfs 0.556 af
Subcatchment3S: 3S Flow Length=14	Runoff Area=39,339 sf 0.00% Impervious Runoff Depth>4.36")' Slope=0.0123 '/' Tc=19.1 min CN=71 Runoff=3.18 cfs 0.328 af
Subcatchment4S: 4S	Runoff Area=27,185 sf 0.00% Impervious Runoff Depth>2.93" Flow Length=194' Tc=23.6 min CN=58 Runoff=1.31 cfs 0.152 af
Subcatchment5S: 5S	Runoff Area=113,462 sf 0.00% Impervious Runoff Depth>3.79" Flow Length=602' Tc=32.4 min CN=66 Runoff=6.33 cfs 0.823 af
Subcatchment6S: 6S Flow Length=	Runoff Area=13,598 sf 21.51% Impervious Runoff Depth>5.17" 92' Slope=0.0217 '/' Tc=9.3 min CN=78 Runoff=1.65 cfs 0.135 af
Subcatchment7S: 7S	Runoff Area=84,203 sf 3.46% Impervious Runoff Depth>4.59" Flow Length=456' Tc=23.1 min CN=73 Runoff=6.61 cfs 0.739 af
Subcatchment9S: 9S	Runoff Area=41,089 sf 6.98% Impervious Runoff Depth>4.81" Flow Length=211' Tc=22.8 min CN=75 Runoff=3.40 cfs 0.378 af
Subcatchment10S: 10S	Runoff Area=17,686 sf 57.92% Impervious Runoff Depth>6.34" Tc=6.0 min CN=88 Runoff=2.80 cfs 0.214 af
Subcatchment11S: 11S	Runoff Area=9,293 sf 18.90% Impervious Runoff Depth>5.29" Flow Length=194' Tc=10.2 min CN=79 Runoff=1.13 cfs 0.094 af
Subcatchment12S: Units 5&6	Runoff Area=994 sf 100.00% Impervious Runoff Depth>7.53" Tc=6.0 min CN=98 Runoff=0.17 cfs 0.014 af
Subcatchment13S: Unit 5	Runoff Area=580 sf 100.00% Impervious Runoff Depth>7.53" Tc=6.0 min CN=98 Runoff=0.10 cfs 0.008 af
Subcatchment14S: Units 3&4	Runoff Area=1,046 sf 100.00% Impervious Runoff Depth>7.53" Tc=6.0 min CN=98 Runoff=0.18 cfs 0.015 af
Subcatchment15S: Unit 4	Runoff Area=498 sf 100.00% Impervious Runoff Depth>7.53" Tc=6.0 min CN=98 Runoff=0.09 cfs 0.007 af
Subcatchment16S: Unit 3	Runoff Area=518 sf 100.00% Impervious Runoff Depth>7.53" Tc=6.0 min CN=98 Runoff=0.09 cfs 0.007 af
Subcatchment17S: Units 1&2	Runoff Area=1,046 sf 100.00% Impervious Runoff Depth>7.53" Tc=6.0 min CN=98 Runoff=0.18 cfs 0.015 af

22201-PROPOSED Prepared by Jones & Beach Engine HydroCAD® 10.20-3c s/n 00762 © 2023	Type III 24-hr 100-YR 24HR Rainfall=7.77"ers IncPrinted 3/22/2024HydroCAD Software Solutions LLCPage 41
Subcatchment18S: Unit 1	Runoff Area=498 sf 100.00% Impervious Runoff Depth>7.53" Tc=6.0 min CN=98 Runoff=0.09 cfs 0.007 af
Subcatchment19S: 19S	Runoff Area=2,375 sf 100.00% Impervious Runoff Depth>7.53" Tc=6.0 min CN=98 Runoff=0.41 cfs 0.034 af
Subcatchment20S: 20S	Runoff Area=2,375 sf 100.00% Impervious Runoff Depth>7.53" Tc=6.0 min CN=98 Runoff=0.41 cfs 0.034 af
Subcatchment21S: Gravel Trail	Runoff Area=574 sf 15.85% Impervious Runoff Depth>5.99" Tc=6.0 min CN=85 Runoff=0.09 cfs 0.007 af
Subcatchment22S: Unit 2	Runoff Area=518 sf 100.00% Impervious Runoff Depth>7.53" Tc=6.0 min CN=98 Runoff=0.09 cfs 0.007 af
Reach 1R: Flow Through 9S n=0.030	Avg. Flow Depth=0.11' Max Vel=1.57 fps Inflow=1.91 cfs 0.078 af L=140.0' S=0.0329 '/' Capacity=43.14 cfs Outflow=1.61 cfs 0.078 af
Reach 3R: Culvert 15.0" Round Pipe n=0.01	Avg. Flow Depth=1.01' Max Vel=5.09 fps Inflow=5.37 cfs 0.550 af 12 L=49.0' S=0.0061 '/' Capacity=5.48 cfs Outflow=5.40 cfs 0.550 af
Reach 4R: Swale n=0.030	Avg. Flow Depth=0.37' Max Vel=4.29 fps Inflow=3.39 cfs 0.644 af L=120.0' S=0.0517 '/' Capacity=30.09 cfs Outflow=3.39 cfs 0.643 af
Reach 5R: Flow Through 1S n=0.030	Avg. Flow Depth=0.14' Max Vel=2.28 fps Inflow=3.39 cfs 0.644 af L=191.0' S=0.0497 '/' Capacity=53.08 cfs Outflow=3.39 cfs 0.643 af
Reach 6R: Flow Through 5S n=0.030	Avg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.000 af L=600.0' S=0.0367 '/' Capacity=45.58 cfs Outflow=0.00 cfs 0.000 af
Reach AP1: Analysis Point 1	Inflow=14.08 cfs 2.050 af Outflow=14.08 cfs 2.050 af
Reach AP2: Analysis Point 2	Inflow=3.18 cfs 0.328 af Outflow=3.18 cfs 0.328 af
Reach AP3: Analysis Point 3	Inflow=1.37 cfs 0.154 af Outflow=1.37 cfs 0.154 af
Reach AP4: Analysis Point 4	Inflow=6.33 cfs 0.823 af Outflow=6.33 cfs 0.823 af
Reach AP5: Analysis Point 5	Inflow=6.32 cfs 0.563 af Outflow=6.32 cfs 0.563 af
Pond 1P: Isolated Wetland Discarded=0	Peak Elev=196.55' Storage=1,191 cf Inflow=1.65 cfs 0.135 af 0.03 cfs 0.033 af Primary=1.91 cfs 0.078 af Outflow=1.94 cfs 0.109 af
Pond 2P: Depression in Woods Discarded=0	Peak Elev=176.65' Storage=5,082 cf Inflow=6.66 cfs 0.742 af .11 cfs 0.104 af Primary=6.32 cfs 0.563 af Outflow=6.43 cfs 0.667 af

22201-PROPOSEDType III 24-hr100-YR24HR Rainfall=7.77"Prepared by Jones & Beach Engineers IncPrinted 3/22/2024HydroCAD® 10.20-3cs/n 00762© 2023 HydroCAD Software Solutions LLCPage 42						
Pond 3P: Center of Cu	Il De Sac	Peak I	Elev=194.93' Stora	age=13,965 c	f Inflow=7.27 cfs Outflow=3.38 cfs	0.765 af 0.643 af
Pond 4P: Drip Edge	Discarded=0.03 cfs	Peak 0.011 af	Elev=191.50' Stor Secondary=0.14 c	rage=0.002 a cfs_0.003 af	f Inflow=0.17 cfs Outflow=0.16 cfs	0.014 af 0.014 af
Pond 5P: Drip Edge	Discarded=0.03 cfs	Peak 0.008 af	Elev=191.39' Stor Secondary=0.00 c	rage=0.003 a cfs_0.000 af	f Inflow=0.10 cfs Outflow=0.03 cfs	0.008 af 0.008 af
Pond 6P: Drip Edge	Discarded=0.09 cfs	Peak 0.015 af	Elev=189.72' Stor Secondary=0.03 c	rage=0.002 a cfs_0.000 af	f Inflow=0.18 cfs Outflow=0.12 cfs	0.015 af 0.015 af
Pond 7P: Drip Edge	Discarded=0.00 cfs	Peak 0.003 af	Elev=192.00' Stor Secondary=0.03 c	rage=0.004 a cfs_0.001 af	f Inflow=0.09 cfs Outflow=0.03 cfs	0.007 af 0.004 af
Pond 8P: Drip Edge	Discarded=0.02 cfs	Peak 0.007 af	Elev=189.91' Stor Secondary=0.00 c	rage=0.003 a cfs_0.000 af	f Inflow=0.09 cfs Outflow=0.02 cfs	0.007 af 0.007 af
Pond 10P: Drip Edge	Discarded=0.04 cfs	Peak 0.015 af	Elev=195.84' Stor Secondary=0.00 c	rage=0.006 a cfs_0.000 af	f Inflow=0.18 cfs Outflow=0.04 cfs	0.015 af 0.015 af
Pond 11P: Drip Edge	Discarded=0.04 cfs	Peak 0.007 af	Elev=195.28' Stor Secondary=0.00 c	rage=0.001 a cfs_0.000 af	f Inflow=0.09 cfs Outflow=0.04 cfs	0.007 af 0.007 af
Pond 20P: Barn	Discarded=0.07 cfs	Peak 0.033 af	Elev=172.00' Stor Secondary=0.05 c	rage=0.013 a cfs_0.000 af	f Inflow=0.41 cfs Outflow=0.12 cfs	0.034 af 0.034 af
Pond 22P: Barn	Discarded=0.07 cfs	Peak 0.033 af	Elev=172.00' Stor Secondary=0.05 c	rage=0.013 a cfs_0.000 af	f Inflow=0.41 cfs Outflow=0.12 cfs	0.034 af 0.034 af
Pond 23P: Drip Edge	Discarded=0.00 cfs	Peak 0.003 af	Elev=172.00' Stor Secondary=0.02 c	rage=0.003 a cfs_0.001 af	f Inflow=0.09 cfs Outflow=0.03 cfs	0.007 af 0.004 af
Pond 24P: Plunge Poo	ol with Culvert Outle 15.0" Roun	et Po d Culvert	eak Elev=193.51' \$ n=0.012 L=50.0'	Storage=48 c S=0.0100 '/'	f Inflow=1.13 cfs Outflow=1.12 cfs	0.094 af 0.094 af
Pond 25P: Drip Edge	Discarded=0.02 cfs	Peak 0.007 af	Elev=195.88' Stor Secondary=0.00 c	rage=0.002 a cfs_0.000 af	f Inflow=0.09 cfs Outflow=0.02 cfs	0.007 af 0.007 af
Total R	unoff Area = 11.94	9 ac Ru 93.60%	noff Volume = 4. Pervious = 11.1	.429 af Ave 84 ac 6.4	erage Runoff De 0% Impervious	pth = 4.45" = 0.764 ac

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Summary for Subcatchment 1S: 1S

Runoff = 6.17 cfs @ 12.28 hrs, Volume= Routed to Reach AP1 : Analysis Point 1 0.650 af, Depth> 3.50"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YR 24HR Rainfall=6.51"

Ar	rea (sf)	CN	Description		
	930	98	Roofs, HSC	ЭС	
	1,120	98	8 Paved parking, HSG C		
	47,794	70	Woods, Go	od, HSG C	
	23,377	74	>75% Gras	s cover, Go	bod, HSG C
	23,763	77	Woods, Go	od, HSG D	
	42	80	>75% Gras	s cover, Go	bod, HSG D
1	97,026	73	Weighted A	verage	
	94,976		97.89% Pe	rvious Area	
	2,050		2.11% Impe	ervious Are	а
Tc	Length	Slope	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	
16.6	100	0.0433	3 0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
1.4	113	0.0708	3 1.33		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
1.4	70	0.0286	6 0.85		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.5	37	0.054 <i>°</i>	1 1.16		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
19.9	320	Total			

Summary for Subcatchment 2S: 2S

Runoff = 4.14 cfs @ 12.26 hrs, Volume= 0.421 af, Depth> 3.30" Routed to Reach AP1 : Analysis Point 1

Area (sf)	CN	Description
1,242	82	Dirt roads, HSG B
19,492	55	Woods, Good, HSG B
45,842	77	Woods, Good, HSG D
66,576 66,576	71	Weighted Average 100.00% Pervious Area

22201-PROPOSED	Type III 24-hr	50-YR 24HR Rainfall=6.51"
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Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
12.3	82	0.0610	0.11		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
2.9	18	0.1111	0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
0.2	21	0.1111	1.67		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.4	30	0.0571	1.19		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
2.4	139	0.0367	0.96		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps

18.2 290 Total

Summary for Subcatchment 3S: 3S

Runoff = 2.40 cfs @ 12.27 hrs, Volume= Routed to Reach AP2 : Analysis Point 2 0.249 af, Depth> 3.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YR 24HR Rainfall=6.51"

A	rea (sf)	CN E	Description				
	27,514	70 V	70 Woods, Good, HSG C				
	11,825	74 >	75% Gras	s cover, Go	ood, HSG C		
	39,339	71 V	Veighted A	verage			
	39,339	1	00.00% Pe	ervious Are	а		
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
10.6	81	0.0123	0.13		Sheet Flow,		
					Grass: Short n= 0.150 P2= 2.90"		
7.3	19	0.0123	0.04		Sheet Flow,		
					Woods: Light underbrush n= 0.400 P2= 2.90"		
1.2	40	0.0123	0.55		Shallow Concentrated Flow,		
					Woodland Kv= 5.0 fps		
19.1	140	Total					

Summary for Subcatchment 4S: 4S

Runoff = 0.90 cfs @ 12.36 hrs, Volume= 0.108 af, Depth> 2.07" Routed to Reach AP3 : Analysis Point 3

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_	A	rea (sf)	CN I	Description		
		1,810	82 I	Dirt roads, I	HSG B	
		19,394	55	Noods, Go	od, HSG B	
_		5,981	61 3	>75% Gras	s cover, Go	ood, HSG B
		27,185	58	Neighted A	verage	
		27,185		100.00% P	ervious Are	а
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	9.6	49	0.0408	0.09		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 2.90"
	12.8	51	0.0213	0.07		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 2.90"
	1.0	43	0.0213	0.73		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.2	51	0.0588	3.90		Shallow Concentrated Flow,
_						Unpaved Kv= 16.1 tps
	23.6	194	Total			

Summary for Subcatchment 5S: 5S

Runoff = 4.63 cfs @ 12.47 hrs, Volume= Routed to Reach AP4 : Analysis Point 4 0.609 af, Depth> 2.80"

Area (sf)	CN	Description
2,174	82	Dirt roads, HSG B
44,614	55	Woods, Good, HSG B
4,013	87	Dirt roads, HSG C
9,149	74	>75% Grass cover, Good, HSG C
49,989	70	Woods, Good, HSG C
817	89	Dirt roads, HSG D
2,706	77	Woods, Good, HSG D
113,462	66	Weighted Average
113,462		100.00% Pervious Area
113,462 113,462	66	Weighted Average 100.00% Pervious Area

22201-PROPOSED	Type III 24-hr	50-YR 24HR Rainfall=6.51"
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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
21.0	100	0.0239	0.08		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
0.4	17	0.0239	0.77		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.8	48	0.0417	1.02		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
1.2	94	0.0638	1.26		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
2.9	116	0.0172	0.66		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.6	51	0.0784	1.40		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
5.5	176	0.0114	0.53		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps

32.4 602 Total

Summary for Subcatchment 6S: 6S

Runoff	=	1.29 cfs @	12.13 hrs,	Volume=
Routed	d to F	ond 1P : Isolated	Wetland	

0.105 af, Depth> 4.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YR 24HR Rainfall=6.51"

A	rea (sf)	CN	Description					
	2,925	98	Paved park	ing, HSG C	;			
	5,274	74	>75% Gras	s cover, Go	ood, HSG C			
	5,399	70	Woods, Go	od, HSG C				
	13,598	78	Weighted Average					
	10,673		78.49% Pervious Area					
	2,925		21.51% Impervious Area					
_				• •				
Tc	Length	Slope	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)				
9.3	92	0.0217	7 0.16		Sheet Flow,			
					Grass: Short	n= 0.150	P2= 2.90"	

Summary for Subcatchment 7S: 7S

Runoff	=	5.05 cfs @	12.32 hrs,	Volume=	0.564 af,	Depth> 3.50"
Routed	to Pond	2P: Depres	sion in Woo	ods		

22201- Prepare	PROPO	SED les & Be	ach Engir	neers Inc	Type III 24-hr 50-YR 24HR Rainfall=6.51" Printed 3/22/2024 D Software Solutions II C
<u>i tydroch</u>	00 10.20	00 3/11 00	<u> </u>		
Α	rea (sf)	CN E	Description		
	898	98 F	Roofs, HSG	ЭC	
	2,014	98 F	Paved park	ing, HSG C	
	37,527	70 V	Voods, Go	od, HSG C	
	33,711	74 >	75% Gras	s cover, Go	bod, HSG C
	9,806	77 V	Voods, Go	od, HSG D	
	247	< 08	-75% Gras	s cover, Go	bod, HSG D
	84,203	73 V	Veighted A	verage	
	81,291	9	6.54% Pei	vious Area	
	2,912	3	5.46% Impe	ervious Are	а
Тс	Longth	Slone	Velocity	Canacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Description
0.2	13	0 0200	0.87	(010)	Sheet Flow
0.2	10	0.0200	0.07		Smooth surfaces $n=0.011$ P2= 2.90"
1.4	20	0.1200	0.24		Sheet Flow.
					Grass: Short n= 0.150 P2= 2.90"
7.3	39	0.0513	0.09		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
7.3	28	0.0260	0.06		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
2.6	127	0.0260	0.81		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.8	75	0.1067	1.63		Shallow Concentrated Flow,
1.0	50	0 0057	0.04		Woodland KV= 5.0 fps
1.0	50	0.0357	0.94		Shallow Concentrated Flow,
0.2	22	0 0000	1 5 1		Shallow Concentrated Flow
0.2	22	0.0303	1.01		Woodland $K_{V} = 5.0 \text{ fps}$
23	76	0.0125	0.56		Shallow Concentrated Flow
2.0	. 0	510120	0.00		Woodland Kv= 5.0 fps
23.1	456	Total			

Summary for Subcatchment 9S: 9S

Runoff = 2.62 cfs @ 12.32 hrs, Volume= 0.291 af, Depth> 3.70" Routed to Reach 3R : Culvert

Area (sf)	CN	Description			
704	98	Roofs, HSG C			
2,162	98	Paved parking, HSG C			
8,023	70	Noods, Good, HSG C			
30,200	74	>75% Grass cover, Good, HSG C			
41,089	75	Weighted Average			
38,223		93.02% Pervious Area			
2,866		6.98% Impervious Area			

22201- Prepare <u>HydroCA</u>	PROPO ed by Jor D® 10.20	SED nes & Be -3c_s/n 00	ach Engir 1762 © 202	neers Inc 23 HydroCAI	"Type III 24-hr 50-YR 24HR Rainfall=6.51 Printed 3/22/2024 D Software Solutions LLC Page 48
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
20.7	100	0.0248	0.08		Sheet Flow,
0.4	21	0.0248	0.79		Woods: Light underbrush n= 0.400 P2= 2.90" Shallow Concentrated Flow, Woodland Kv= 5.0 fps
1.7	90	0.0167	0.90		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
22.8	211	Total			

Summary for Subcatchment 10S: 10S

Runoff = 2.29 cfs @ 12.09 hrs, Volume= 0.173 af, Depth> 5.11" Routed to Pond 3P : Center of Cul De Sac

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YR 24HR Rainfall=6.51"

Area (st	f) CN	Description	Description				
72	8 98	Roofs, HSC	ЭC				
9,51	6 98	Paved park	ing, HSG C	C			
7,44	2 74	>75% Gras	s cover, Go	lood, HSG C			
17,68	6 88	Weighted A	Weighted Average				
7,44	2	42.08% Per	42.08% Pervious Area				
10,24	4	57.92% Imp	pervious Ar	rea			
Tc Leng	th Slo	pe Velocity	Capacity	Description			
(min) (fee	et) (ft/	ft) (ft/sec)	(cfs)				
6.0				Direct Entry,			

Summary for Subcatchment 11S: 11S

Runoff = 0.89 cfs @ 12.14 hrs, Volume= 0.073 af, Depth> 4.13" Routed to Pond 24P : Plunge Pool with Culvert Outlet

Are	a (sf)	CN	Description				
	1,756	98	Paved parking, HSG C				
	7,537	74	>75% Grass cover, Good, HSG C				
	9,293	79	Weighted Average				
	7,537		81.10% Pervious Area				
	1,756		18.90% Impervious Area				

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
9.7	73	0.0123	0.13		Sheet Flow,			
0.5	121	0.0165	4.25	17.00	Trap/Vee/Rect Channel Flow, Bot.W=1.00' D=1.00' Z= 3.0 '/' Top.W=7.00' n= 0.030 Stream, clean & straight			
10.2	194	Total						
Summary for Subcatchment 12S: Units 5&6								
Runoff Route	Runoff = 0.14 cfs @ 12.09 hrs, Volume= 0.012 af, Depth> 6.27" Routed to Pond 4P : Drip Edge							

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YR 24HR Rainfall=6.51"

A	rea (sf)	CN	Description					
	838	98	Roofs, HSG	G C				
	156	98	Water Surfa	ace, HSG C				
	994	98	Weighted A	Weighted Average				
	994		100.00% In	100.00% Impervious Area				
То	Longth	Slop	o Volocity	Capacity	Description			
	Lengin	Siop	e velocity	Capacity	Description			
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)				
6.0					Direct Entry,			

Summary for Subcatchment 13S: Unit 5

Runoff = 0.08 cfs @ 12.09 hrs, Volume= 0.007 af, Depth> 6.27" Routed to Pond 5P : Drip Edge

rea (sf)	CN	Description					
395	98	Roofs, HSG	S C				
185	98	Water Surfa	ace, HSG C				
580	98	Weighted Average					
580		100.00% Impervious Area					
Length	Slop	e Velocity	Capacity	Description			
(feet)	(ft/f	i) (ft/sec)	(cfs)				
				Direct Entry,			
	ea (sf) 395 185 580 580 Length (feet)	ea (sf) CN 395 98 185 98 580 98 580 Length Slop (feet) (ft/ft	ea (sf) CN Description 395 98 Roofs, HSG 185 98 Water Surfa 580 98 Weighted A 580 100.00% In Length Slope Velocity (feet) (ft/ft) (ft/sec)	ea (sf)CNDescription39598Roofs, HSG C18598Water Surface, HSG C58098Weighted Average580100.00%Impervious ALengthSlopeVelocityCapacity(feet)(ft/ft)(ft/sec)(cfs)			

22201-PROPOSED	Type III 24-hr	50-YR 24HR Raii	nfall=6.51'
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Summary for Subcatchment 14S: Units 3&4

Runoff = 0.15 cfs @ 12.09 hrs, Volume= 0.013 af, Depth> 6.27" Routed to Pond 6P : Drip Edge

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YR 24HR Rainfall=6.51"

A	rea (sf)	CN	Description						
	838	98	Roofs, HSC	ЭC					
	208	98	Water Surfa	ace, HSG C					
	1,046	98	Weighted A	verage					
	1,046	6 100.00% Impervious Area							
Tc (min)	Length (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description				
6.0					Direct Entry,				
	Summary for Subcatchment 15S: Unit 4								

Runoff = 0.07 cfs @ 12.09 hrs, Volume= 0.006 af, Depth> 6.27" Routed to Pond 7P : Drip Edge

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YR 24HR Rainfall=6.51"

Α	rea (sf)	CN	Description				
	395	98	Roofs, HSC	ЭС			
	103	98	Water Surfa	ace, HSG C	;		
	498	98	Weighted Average				
	498		100.00% Impervious Area				
Tc (min)	Length (feet)	Slop (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description		
6.0					Direct Entry,		

Summary for Subcatchment 16S: Unit 3

Runoff = 0.07 cfs @ 12.09 hrs, Volume= 0.006 af, Depth> 6.27" Routed to Pond 8P : Drip Edge

Α	rea (sf)	CN	Description
	395	98	Roofs, HSG C
	123	98	Water Surface, HSG C
	518	98	Weighted Average
	518		100.00% Impervious Area

22201-	PROPO	SED				Type III 24	-hr 50-YR 24HR Rai	nfall=6.51"
Prepare	d by Jon	ies & E	Beach Engir	ieers Inc			Printed	3/22/2024
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Tc (min)	Length (feet)	Slop (ft/fl	e Velocity (ft/sec)	Capacity (cfs)	Descriptior	1		
6.0					Direct Ent	ry,		
			Summa	ar for Su	haatahma	nt 170, 11ni	ita 190	
			Summai	ry for Su	DCatchine	nt 175: Un	15 102	
Runoff Route	= ed to Pon	0.15 d 10P :	cfs @ 12.09 Drip Edge	9 hrs, Volu	ıme=	0.013 af, Do	epth> 6.27"	
Runoff b Type III	y SCS TF 24-hr 50-	R-20 m -YR 24	ethod, UH=S HR Rainfall=	SCS, Weigl 6.51"	nted-CN, Tim	ne Span= 0.00	0-24.00 hrs, dt= 0.05 h	rs
А	rea (sf)	CN	Description					
	838 208	98 98	Roofs, HSC Water Surfa	GC ace, HSG (5			
	1,046 1,046	98	Weighted A 100.00% Im	verage pervious A	Area			
Tc (min)	Length (feet)	Slop (ft/ft	e Velocity :) (ft/sec)	Capacity (cfs)	Descriptior	1		
6.0					Direct Ent	ry,		
			Summ	ary for S	Subcatchm	nent 18S: U	nit 1	
Runoff Route	= ed to Pon	0.07 d 11P :	cfs @ 12.09 Drip Edge	9 hrs, Volu	ıme=	0.006 af, De	epth> 6.27"	
Runoff b Type III	y SCS TF 24-hr 50-	R-20 m -YR 24	ethod, UH=S HR Rainfall=	SCS, Weigl 6.51"	nted-CN, Tim	ne Span= 0.00	0-24.00 hrs, dt= 0.05 h	rs
А	rea (sf)	CN	Description					
	395	98	Roofs, HSC	G C				
	103	98	Water Surfa	ace, HSG (2			
	498 498	98	Weighted A 100.00% Im	verage pervious A	Area			

TcLengthSlopeVelocityCapacityDescription(min)(feet)(ft/ft)(ft/sec)(cfs)6.0Direct Entry,

Summary for Subcatchment 19S: 19S

Runoff = 0.34 cfs @ 12.09 hrs, Volume= 0.028 af, Depth> 6.27" Routed to Pond 20P : Barn

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Α	rea (sf)	CN	Description				
	1,995	98	Roofs, HSC	βB			
	380	98	Water Surfa	ace, HSG E	3		
	2,375	98	Weighted Average				
	2,375		100.00% Impervious Area				
Tc	Length	Slop	e Velocity	Capacity	Description		
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)			
6.0					Direct Entry,		

Summary for Subcatchment 20S: 20S

Runoff = 0.34 cfs @ 12.09 hrs, Volume= 0.028 af, Depth> 6.27" Routed to Pond 22P : Barn

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YR 24HR Rainfall=6.51"

A	rea (sf)	CN	Description				
	1,995	98	Roofs, HSG	βB			
	380	98	Water Surfa	ace, HSG B	3		
	2,375	98	Weighted A	verage			
	2,375		100.00% Impervious Area				
Tc	Length	Slop	e Velocity	Capacity	Description		
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)			
6.0					Direct Entry,		
					•		

Summary for Subcatchment 21S: Gravel Trail

Runoff = 0.07 cfs @ 12.09 hrs, Volume= 0.005 af, Depth> 4.78" Routed to Pond 23P : Drip Edge

A	rea (sf)	CN	Description				
	483	82	Dirt roads,	HSG B			
	91	98	Water Surfa	ace, HSG B	3		
	574	85	Weighted Average				
	483		84.15% Pervious Area				
	91		15.85% Impervious Area				
Tc (min)	Length (feet)	Slop (ft/fl	e Velocity) (ft/sec)	Capacity (cfs)	Description		
6.0			/ (- /		Direct Entry,		

22201-PROPOSED	Type III 24-hr 🗄	50-YR 24HR Raii	nfall=6.51'
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Summary for Subcatchment 22S: Unit 2

0.006 af, Depth> 6.27"

Runoff = 0.07 cfs @ 12.09 hrs, Volume= Routed to Pond 25P : Drip Edge

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50-YR 24HR Rainfall=6.51"

A	rea (sf)	CN	Description				
	395	98	Roofs, HSC	G C			
	123	98	Water Surfa	ace, HSG C			
	518	98	Weighted Average				
	518		100.00% Impervious Area				
Тс	Length	Slop	e Velocity	Capacity	Description		
(min)	(feet)	(ft/f) (ft/sec)	(cfs)			
6.0					Direct Entry,		

Summary for Reach 1R: Flow Through 9S

[80] Warning: Exceeded Pond 1P by 0.08' @ 12.30 hrs (1.14 cfs 0.034 af)

 Inflow Area =
 0.312 ac, 21.51% Impervious, Inflow Depth =
 1.94"
 for 50-YR 24HR event

 Inflow =
 2.18 cfs @
 12.15 hrs, Volume=
 0.051 af

 Outflow =
 1.35 cfs @
 12.17 hrs, Volume=
 0.051 af, Atten= 38%, Lag= 1.3 min

 Routed to Reach 3R : Culvert
 0.051 af, Atten= 38%, Lag= 1.3 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 1.45 fps, Min. Travel Time= 1.6 min Avg. Velocity = 0.47 fps, Avg. Travel Time= 5.0 min

Peak Storage= 130 cf @ 12.17 hrs Average Depth at Peak Storage= 0.10', Surface Width= 13.72' Bank-Full Depth= 0.50' Flow Area= 10.0 sf, Capacity= 43.14 cfs

30.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight Length= 140.0' Slope= 0.0329 '/' Inlet Invert= 196.40', Outlet Invert= 191.80'

‡

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Summary for Reach 3R: Culvert

[52] Hint: Inlet/Outlet conditions not evaluated

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[62] Hint: Exceeded Reach 1R OUTLET depth by 0.73' @ 12.20 hrs

[64] Warning: Exceeded Reach 1R outlet bank by 0.33' @ 12.21 hrs

Inflow Area =1.469 ac, 11.80% Impervious, Inflow Depth > 3.39"for 50-YR 24HR eventInflow =4.15 cfs @12.20 hrs, Volume=0.415 afOutflow =4.23 cfs @12.21 hrs, Volume=0.415 af, Atten= 0%, Lag= 0.5 minRouted to Pond 3P : Center of Cul De Sac20.415 af, Atten= 0%, Lag= 0.5 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 4.92 fps, Min. Travel Time= 0.2 min Avg. Velocity = 1.93 fps, Avg. Travel Time= 0.4 min

Peak Storage= 42 cf @ 12.21 hrs Average Depth at Peak Storage= 0.83', Surface Width= 1.18' Bank-Full Depth= 1.25' Flow Area= 1.2 sf, Capacity= 5.48 cfs

15.0" Round Pipe n= 0.012 Length= 49.0' Slope= 0.0061 '/' Inlet Invert= 191.80', Outlet Invert= 191.50'



Summary for Reach 4R: Swale

 Inflow Area =
 1.875 ac, 21.79% Impervious, Inflow Depth > 3.09"
 for 50-YR 24HR event

 Inflow =
 1.37 cfs @
 12.85 hrs, Volume=
 0.483 af

 Outflow =
 1.37 cfs @
 12.85 hrs, Volume=
 0.483 af, Atten= 0%, Lag= 0.4 min

 Routed to Reach 5R : Flow Through 1S
 S
 S
 S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 3.36 fps, Min. Travel Time= 0.6 min Avg. Velocity = 1.87 fps, Avg. Travel Time= 1.1 min

Peak Storage= 49 cf @ 12.85 hrs Average Depth at Peak Storage= 0.24' , Surface Width= 2.43' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 30.09 cfs

1.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight Side Slope Z-value= 3.0 '/' Top Width= 7.00' Length= 120.0' Slope= 0.0517 '/' Inlet Invert= 189.70', Outlet Invert= 183.50'



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30.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight Length= 600.0' Slope= 0.0367 '/' Inlet Invert= 196.00', Outlet Invert= 174.00'



Summary for Reach AP1: Analysis Point 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow A	Area	=	5.631 ac,	8.09% Impervious,	Inflow Depth >	3.3	I" for 50-YR 24HR event
Inflow		=	10.64 cfs @	12.27 hrs, Volume	= 1.552	af	
Outflov	N	=	10.64 cfs @	12.27 hrs, Volume	= 1.552	af, /	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	ea =	0.903 ac,	0.00% Impervious,	Inflow Depth > 3.	30" for 50-YR 24HR event
Inflow	=	2.40 cfs @	12.27 hrs, Volume	= 0.249 af	
Outflow	=	2.40 cfs @	12.27 hrs, Volume	= 0.249 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow A	rea =	0.624 ac,	0.00% Impervious, I	nflow Depth > 2.0	07" for 50-YR 24HR event
Inflow	=	0.90 cfs @	12.36 hrs, Volume=	0.108 af	
Outflow	=	0.90 cfs @	12.36 hrs, Volume=	0.108 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Analysis Point 4

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	ea =	2.605 ac,	0.00% Impervious,	Inflow Depth > 2.8	80" for 50-YR 24HR event
Inflow	=	4.63 cfs @	12.47 hrs, Volume	= 0.609 af	
Outflow	=	4.63 cfs @	12.47 hrs, Volume	= 0.609 af,	Atten= 0%, Lag= 0.0 min

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP5: Analysis Point 5

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	1.933 ac,	3.46% Impervious,	Inflow Depth >	2.43"	for 50-YR 24HR event
Inflow	=	4.72 cfs @	12.40 hrs, Volume	= 0.392	af	
Outflow	=	4.72 cfs @	12.40 hrs, Volume	= 0.392	af, Att	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Pond 1P: Isolated Wetland

[93] Warning: Storage range exceeded by 0.15'

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=51)

Inflow Area	=	0.312 ac, 2	1.51% Imp	ervious,	Inflow	Depth >	4.03	" for	50-YR	24HR e	event
Inflow	=	1.29 cfs @	12.13 hrs,	Volume	=	0.105	af				
Outflow	=	2.21 cfs @	12.15 hrs,	Volume	=	0.081	af, A	tten= 0	%, La	g= 1.0 r	nin
Discarded	=	0.03 cfs @	12.16 hrs,	Volume	=	0.032	af				
Primary	=	2.18 cfs @	12.15 hrs,	Volume	=	0.051	af				
Routed	to Reac	h 1R : Flow	Through 9S								

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 196.56' @ 12.16 hrs Surf.Area= 2,828 sf Storage= 1,191 cf

Plug-Flow detention time= 146.7 min calculated for 0.081 af (77% of inflow) Center-of-Mass det. time= 65.9 min (883.8 - 817.9)

Volume	Inve	ert Avail	.Storage	Storage Description	า		
#1	195.3	0'	1,191 cf	Custom Stage Dat	t a (Irregular) Listed	below (Recalc)	
Elevatio (fee	on et)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft <u>)</u>	
195.3 196.0 196.4 196.4	30 00 40 41	235 1,050 2,828 2,828	72.0 148.0 211.0 211.0	0 416 747 28	0 416 1,163 1,191	235 1,568 3,369 3,371	
Device	Routing	Inv	ert Outle	et Devices			
#1	Primary	196.	40' 20.0 Head 2.50 Coet 2.65	' long x 6.0' breadt d (feet) 0.20 0.40 0 3.00 3.50 4.00 4.4 f. (English) 2.37 2.5 2.66 2.66 2.67 2.1	Broad-Crested I 0.60 0.80 1.00 1.2 50 5.00 5.50 51 2.70 2.68 2.68 69 2.72 2.76 2.83	Rectangular Weir 20 1.40 1.60 1.80 2.67 2.65 2.65 2.	2.00 65
#2	Discarde	d 195.	30' 0.30 Con	0 in/hr Exfiltration of ductivity to Groundw	over Surface area ater Elevation = 194	4.80' Phase-In= 0).10'

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Discarded OutFlow Max=0.03 cfs @ 12.16 hrs HW=196.54' (Free Discharge) **2=Exfiltration** (Controls 0.03 cfs)

Primary OutFlow Max=2.13 cfs @ 12.15 hrs HW=196.55' TW=196.50' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir**(Weir Controls 2.13 cfs @ 0.70 fps)

Summary for Pond 2P: Depression in Woods

Inflow Area	a =	1.933 ac,	3.46% Impervi	ious, Inflow l	Depth >	3.51"	for 50-Y	'R 24HR event
Inflow	=	5.08 cfs @	12.32 hrs, Vo	lume=	0.566	af		
Outflow	=	4.83 cfs @	12.40 hrs, Vo	lume=	0.491	af, Atte	en= 5%, I	_ag= 4.6 min
Discarded	=	0.11 cfs @	12.40 hrs, Vo	lume=	0.099	af		
Primary	=	4.72 cfs @	12.40 hrs, Vo	lume=	0.392	af		
Routed	to Reac	h AP5 : Anal	ysis Point 5					

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 176.61' @ 12.40 hrs Surf.Area= 7,514 sf Storage= 4,758 cf

Plug-Flow detention time= 88.1 min calculated for 0.491 af (87% of inflow) Center-of-Mass det. time= 30.2 min (870.3 - 840.2)

Volume	Inve	ert Avai	il.Storage	Storage Descriptio	n		
#1	175.7	'0'	5,471 cf	Custom Stage Da	ita (Irregular) Listed b	elow (Recalc)	
Elevatio (fee	on et)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
175.7	' 0	2,764	204.0	0	0	2,764	
176.0)0	3,841	265.0	986	986	5,042	
176.4	10	7,514	341.0	2,230	3,217	8,709	
176.7	70	7,514	341.0	2,254	5,471	8,811	
Device	Routing	In	vert Outl	et Devices			
#1	Primary	176	5.40' 20.0 Hear 2.50	' long x 2.0' bread d (feet) 0.20 0.40 3.00 3.50 f (English) 2.54 2	th Broad-Crested R 0.60 0.80 1.00 1.20	ectangular Weir) 1.40 1.60 1.80 2 2 70 2 77 2 89 2 8	2.00
#2	Discarde	ed 175	2.85 5.70' 0.30 Con	3.07 3.20 3.32 0 in/hr Exfiltration ductivity to Groundv	over Surface area vater Elevation = 175	.20' Phase-In= 0.	.10'

Discarded OutFlow Max=0.11 cfs @ 12.40 hrs HW=176.60' (Free Discharge) **2=Exfiltration** (Controls 0.11 cfs)

22201-PROPOSED	Type III 24-hr	50-YR 24HR Rainfall=6.51"
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Summary for Pond 3P: Center of Cul De Sac

[63] Warning: Exceeded Reach 3R INLET depth by 2.47' @ 13.10 hrs

Inflow Area = 1.875 ac, 21.79% Impervious, Inflow Depth > 3.76" for 50-YR 24HR event 5.75 cfs @ 12.17 hrs, Volume= Inflow = 0.588 af Outflow 1.37 cfs @ 12.85 hrs, Volume= 0.483 af, Atten= 76%, Lag= 40.5 min = Primary = 1.37 cfs @ 12.85 hrs, Volume= 0.483 af Routed to Reach 4R : Swale

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 194.61' @ 12.85 hrs Surf.Area= 4,219 sf Storage= 12,602 cf

Plug-Flow detention time= 239.0 min calculated for 0.482 af (82% of inflow) Center-of-Mass det. time= 171.4 min (986.9 - 815.6)

Volume	Invert	Avail.Stor	rage Storage D	escription	
#1	190.00'	16,17	1 cf Custom S	Stage Data (Pris	smatic)Listed below (Recalc)
Elevation (feet)	Su	rf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
190.00		1 491	0	0	
191.00		1,934	1,713	1,713	
192.00		2,483	2,209	3,921	
194.00		3,751	6,234	10,155	
195.00		4,514	4,133	14,288	
195.40		4,903	1,883	16,171	
Device R	outing	Invert	Outlet Devices		
#1 P	rimary	190.00'	15.0" Round C L= 47.0' CPP, Inlet / Outlet Inv n= 0.012. Flow	Culvert projecting, no ho vert= 190.00' / 18 Area= 1.23 sf	eadwall, Ke= 0.900 39.70' S= 0.0064 '/' Cc= 0.900
#2 D	evice 1	190.00'	2.0" Vert. Orifi	ce/Grate C= 0.	.600 Limited to weir flow at low heads
#3 D	evice 1	191.30'	2.0" Vert. Orifi	ce/Grate C= 0.	.600 Limited to weir flow at low heads
#4 D	evice 1	193.40'	2.0" Vert. Orifi	ce/Grate C= 0.	.600 Limited to weir flow at low heads
#5 D	evice 1	193.65'	0.7" W x 9.6" H Limited to weir	I Vert. Orifice/G flow at low head	Frate C= 0.600 s
#6 D	evice 1	194.45'	12.0" Horiz. Or Limited to weir	r ifice/Grate C= flow at low head	9.600 s
Primary O [€] —1=Culve	utFlow Ma ert (Passe	ax=1.37 cfs (s 1.37 cfs of	12.85 hrs HW 9.32 cfs potentia	=194.61' TW=18 Il flow)	89.94' (Dynamic Tailwater)

2=Orifice/Grate (Orifice Controls 0.22 cfs @ 10.25 fps) -3=Orifice/Grate (Orifice Controls 0.19 cfs @ 8.65 fps) -4=Orifice/Grate (Orifice Controls 0.11 cfs @ 5.12 fps)

-5=Orifice/Grate (Orifice Controls 0.16 cfs @ 3.53 fps)

-6=Orifice/Grate (Weir Controls 0.68 cfs @ 1.32 fps)

#1

Discarded

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Summary for Pond 4P: Drip Edge

Inflow Area = 0.023 ac,100.00% Impervious, Inflow Depth >	6.27" for 50-YR 24HR event
Inflow = 0.14 cfs @ 12.09 hrs, Volume= 0.012 a	af
Outflow = 0.14 cfs @ 12.12 hrs, Volume= 0.012 a	af, Atten= 0%, Lag= 2.1 min
Discarded = 0.03 cfs @ 12.10 hrs, Volume= 0.010 a	af
Secondary = 0.12 cfs @ 12.12 hrs, Volume= 0.002 a	af
Routed to Pond 2P : Depression in Woods	
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.	05 hrs / 3
Peak Elev= 191.50' @ 12.10 hrs Surf.Area= 0.004 ac Storage= 0.	002 af
e v	
Plug-Flow detention time= 48.5 min calculated for 0.012 af (99% of in	nflow)
Center-of-Mass det. time= 43.2 min (786.7 - 743.5)	/
Volume Invert Avail.Storage Storage Description	
#1 189.90' 0.002 af 3.00'W x 52.00'L x 1.60'H P	rismatoid
0.006 af Overall x 40.0% Vo	ids
Device Routing Invert Outlet Devices	
#0 Secondary 191 50' Automatic Storage Overflow (Discharged without head)
#1 Discarded 189.90' 0.300 in/hr Exfiltration over Su	rface area
Conductivity to Groundwater Elev	ation = 189.83' Phase-In= 0.10'
Discarded OutFlow Max=0.03 cfs @ 12.10 brs HW=191.50' (Free	Discharge)
1=Evfiltration (Controls 0.03 cfs)	, Discharge)
Secondary OutFlow Max=0.00 cfs @ 12.12 hrs HW=191.50' TW=	176.44' (Dynamic Tailwater)
Summary for Pond 5P. Drin	Edge
Summary for Fond SF. Drip	Luge
Inflow Area = 0.013 ac,100.00% Impervious, Inflow Depth >	6.27" for 50-YR 24HR event
1000 = 0.08 cfs @ 12.09 hrs, Volume = 0.007 a	
Outflow = $0.02 \text{ cfs} @ 12.42 \text{ hrs}, \text{ Volume} = 0.007 \text{ a}$	af, Atten= 71% , Lag= 19.9 min
Discarded = $0.02 \text{ cfs} @ 12.42 \text{ hrs}$, Volume= 0.007 a	
Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 a	af
Routed to Reach 4R : Swale	
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.	05 hrs / 3
Peak Elev= 191.13' @ 12.42 hrs Surf.Area= 0.004 ac Storage= 0.	002 af
Plug-Flow detention time= 55.8 min calculated for 0.007 af (99% of in	nflow)
Center-of-Mass det. time= 49.1 min (792.7 - 743.5)	
Volume Invert Avail.Storage Storage Description	
#1 189.90' 0.003 af 4.50'W x 41.00'L x 1.60'H P	rismatoid
0.007 af Overall x 40.0% Vo	ids
Device Routing Invert Outlet Devices	
#0 Secondary 191.50' Automatic Storage Overflow (I	Discharged without head)

189.90' 0.300 in/hr Exfiltration over Surface area

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Conductivity to Groundwater Elevation = 189.83' Phase-In= 0.10'

Discarded OutFlow Max=0.02 cfs @ 12.42 hrs HW=191.13' (Free Discharge) **1=Exfiltration** (Controls 0.02 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=189.90' TW=189.70' (Dynamic Tailwater)

Summary for Pond 6P: Drip Edge

Inflow Area = Inflow = Outflow = Discarded = Secondary = Routed to Reac	0.024 ac,100.0 0.15 cfs @ 12 0.08 cfs @ 12 0.08 cfs @ 12 0.00 cfs @ 0 h 5R : Flow Thro	0% Impervious, Inflow Depth > 6.27" for 50-YR 24HR event .09 hrs, Volume= 0.013 af .22 hrs, Volume= 0.012 af, Atten= 46%, Lag= 8.0 min .22 hrs, Volume= 0.012 af .00 hrs, Volume= 0.000 af bugh 1S
Routing by Dyn-Ste	or-Ind method T	"me Span= 0 00-24 00 brs_dt= 0 05 brs / 3
Peak Flev= 189 62	'@ 12 22 hrs S	Surf Area = 0.005 ac Storage = 0.002 af
Plua-Flow detentio	n time= 20.2 mir	n calculated for 0.012 af (99% of inflow)
Center-of-Mass de	t. time= 16.6 mir	n (760.2 - 743.5)
Volume Inve	rt Avail.Storag	ge Storage Description
#1 188.52	2' 0.002	af 4.00'W x 52.00'L x 1.20'H Prismatoid
		0.006 af Overall x 40.0% Voids
Device Routing	Invert	Outlet Devices
#0 Secondar	y 189.72'	Automatic Storage Overflow (Discharged without head)
#1 Discarded	188.52'	0.300 in/hr Exfiltration over Surface area
		Conductivity to Groundwater Elevation = 188.50' Phase-In= 0.10'
Discarded OutFlo	w Max=0.08 cfs Controls 0.08 c	@ 12.22 hrs HW=189.61' (Free Discharge) fs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=188.52' TW=183.50' (Dynamic Tailwater)

Summary for Pond 7P: Drip Edge

Inflow Area =	0.011 ac,100.0	0% Impervious,	Inflow Depth > 6.	27" for 50-YR 24HR event
Inflow =	0.07 cfs @ 12	.09 hrs, Volume=	= 0.006 af	
Outflow =	0.00 cfs @ 14	.27 hrs, Volume=	= 0.003 af,	Atten= 95%, Lag= 131.2 min
Discarded =	0.00 cfs @ 14	.25 hrs, Volume=	= 0.003 af	
Secondary =	0.00 cfs @ 14	.27 hrs, Volume=	= 0.000 af	
Routed to Reac	h 4R : Swale			

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 192.00'@ 14.25 hrs Surf.Area= 0.002 ac Storage= 0.004 af

Plug-Flow detention time= 333.5 min calculated for 0.003 af (52% of inflow) Center-of-Mass det. time= 206.7 min (950.2 - 743.5)

22201-	PROPOSE	D	Type III 24-hr	50-YR 24HR Rainfall=6.51"
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Volume	Invert	Avail.Storage	Storage Description	
#1	188.00'	0.004 af	2.50'W x 41.00'L x 4.00'H Prismatoid 0.009 af Overall x 40.0% Voids	I
Device	Routing	Invert Ou	tlet Devices	
#0 #1	Secondary Discarded	192.00' Au 188.00' 0.3 Co	tomatic Storage Overflow (Discharge 00 in/hr Exfiltration over Surface area nductivity to Groundwater Elevation = 18	d without head) a 86.50' Phase-In= 0.10'
Discard Η1=Ex	ed OutFlow filtration(Co	Max=0.00 cfs @ ontrols 0.00 cfs)	14.25 hrs HW=192.00' (Free Discharg	ge)
Second	ary OutFlow	Max=0.00 cfs @	2 14.27 hrs HW=192.00' TW=189.86'	(Dynamic Tailwater)
		Sun	nmary for Pond 8P: Drip Edge	
Inflow A Inflow Outflow Discarde Seconda Route	rea = 0. = 0. = 0. ed = 0. ary = 0. ed to Reach A	.012 ac,100.00% 07 cfs @ 12.09 02 cfs @ 12.48 02 cfs @ 12.48 00 cfs @ 0.00 AP1 : Analysis Po	Impervious, Inflow Depth > 6.27" fo hrs, Volume= 0.006 af hrs, Volume= 0.006 af, Atten= hrs, Volume= 0.006 af hrs, Volume= 0.000 af point 1	r 50-YR 24HR event 77%, Lag= 23.4 min
Routing Peak Ele	by Dyn-Stor-I ev= 189.52' @	nd method, Time 0 12.48 hrs Sur	e Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 f.Area= 0.003 ac Storage= 0.002 af	
Plug-Flo Center-o	of-Mass det. ti	ime= 78.0 min ca ime= 71.3 min (8	llculated for 0.006 af (99% of inflow) 314.8 - 743.5)	
Volume	Invert	Avail.Storage	Storage Description	
#1	187.60'	0.003 af	3.00'W x 41.00'L x 2.40'H Prismatoid 0.007 af Overall x 40.0% Voids	
Device	Routing	Invert Ou	tlet Devices	
#0 #1	Secondary Discarded	190.00' Au 187.60' 0.3 Co	tomatic Storage Overflow (Discharge 300 in/hr Exfiltration over Surface area nductivity to Groundwater Elevation = 18	d without head) a 87.50' Phase-In= 0.10'
Discarded OutFlow Max=0.02 cfs @ 12.48 hrs HW=189.52' (Free Discharge)				
Second	ary OutFlow	Max=0.00 cfs @	0.00 hrs HW=187.60' TW=0.00' (Dy	namic Tailwater)
Summary for Pond 10P: Drip Edge				
Inflow A Inflow Outflow Discarde Seconda Route	rea = 0. = 0. = 0. ed = 0. ary = 0. ed to Reach 3	.024 ac,100.00% 15 cfs @ 12.09 03 cfs @ 12.52 03 cfs @ 12.52 00 cfs @ 0.00 3R : Culvert	Impervious, Inflow Depth > 6.27" fo hrs, Volume= 0.013 af hrs, Volume= 0.012 af, Atten= hrs, Volume= 0.012 af hrs, Volume= 0.000 af	r 50-YR 24HR event 80%, Lag= 25.8 min

22201 - Prepare	PROPOSE	D & Beach End	<i>Type III 24-hr 50-YR 24HR Ra</i> gineers Inc Printed	infall=6.51" 3/22/2024
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Routing Peak El	by Dyn-Stor-I ev= 195.32' @	nd method, T) 12.52 hrs	Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Surf.Area= 0.005 ac Storage= 0.005 af	
Plug-Flo Center-o	ow detention ti of-Mass det. ti	me= 101.7 m me= 94.7 mir	nin calculated for 0.012 af (99% of inflow) n(838.2 - 743.5)	
Volume		Avail.Stora	lge Storage Description	
#1	192.80	0.006	0.015 af Overall x 40.0% Voids	
Device	Routing	Invert	Outlet Devices	
#0 #1	Secondary Discarded	196.00' 192.80'	Automatic Storage Overflow (Discharged without head) 0.300 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 192.67' Phase-Ir	= 0.10'
Discard Η1=Ex	ed OutFlow I	Max=0.03 cfs ontrols 0.03 c	s @ 12.52 hrs HW=195.32' (Free Discharge) cfs)	

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=192.80' TW=191.80' (Dynamic Tailwater)

Summary for Pond 11P: Drip Edge

Inflow Area =	0.011 ac,10	0.00% Imperv	ious, Inflow l	Depth >	6.27"	for 50-Y	R 24HR event
Inflow =	0.07 cfs @	12.09 hrs, Vo	olume=	0.006 a	af		
Outflow =	0.03 cfs @	12.27 hrs, Vo	olume=	0.006 a	af, Atte	en= 55%,	Lag= 10.9 min
Discarded =	0.03 cfs @	12.27 hrs, Vo	olume=	0.006 a	af		-
Secondary =	0.00 cfs @	0.00 hrs, Vo	olume=	0.000 a	af		
Routed to Reac	h 3R : Culve	rt					

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 195.02' @ 12.27 hrs Surf.Area= 0.002 ac Storage= 0.001 af

Plug-Flow detention time= 27.8 min calculated for 0.006 af (99% of inflow) Center-of-Mass det. time= 23.5 min (767.0 - 743.5)

Volume	Invert	Avail.Storag	e Storage Description
#1	193.70'	0.002 a	af 2.50'W x 41.00'L x 2.30'H Prismatoid 0.005 af Overall x 40.0% Voids
Device	Routing	Invert	Outlet Devices
#0	Secondary	196.00'	Automatic Storage Overflow (Discharged without head)
#1	Discarded	193.70'	0.300 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 193.67' Phase-In= 0.10'
Discard	ed OutFlow	Max=0.03 cfs	@ 12.27 hrs HW=195.01' (Free Discharge)

1=Exfiltration (Controls 0.03 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=193.70' TW=191.80' (Dynamic Tailwater)

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Summary for Pond 20P: Barn

Inflow A	rea =	0.055 ac,100.0	0% Impervious, Inflow Depth > 6.27" for 50-YR 24HR event
Inflow	=	0.34 cfs @ 12	.09 hrs, Volume= 0.028 af
Outflow	=	0.06 cfs @ 12	.54 hrs, Volume= 0.028 af, Atten= 82%, Lag= 27.1 min
Discarde	ed =	0.06 cis @ 12	.04 hrs, Volume = 0.028 al
Deconua	ary – od to Boock	0.00 CIS (0) 0	Doint 2
Rout	eu lo Reaci	TAPS . Analysis	
Routing Peak El	by Dyn-Sto ev= 171.46'	r-Ind method, T @ 12.54 hrs	ime Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Surf.Area= 0.009 ac_ Storage= 0.012 af
Plug-Flo Center-o	ow detentior of-Mass det	n time= 120.4 m . time= 110.5 m	in calculated for 0.028 af (98% of inflow) in (854.0 - 743.5)
Volume	Inver	t Avail.Stora	ge Storage Description
#1	168.15	0.013	af 4.00'W x 95.00'L x 3.85'H Prismatoid 0.034 af Overall x 40.0% Voids
Device	Routing	Invert	Outlet Devices
#0	Secondary	y 172.00'	Automatic Storage Overflow (Discharged without head)
#1	Discarded	168.15'	0.300 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 168.00' Phase-In= 0.10'
Discard	led OutFlov filtration(w Max=0.06 cfs Controls 0.06 c	@ 12.54 hrs HW=171.46' (Free Discharge) fs)
Second	ary OutFlo	w Max=0.00 cfs	s @ 0.00 hrs HW=168.15' TW=0.00' (Dynamic Tailwater)
			Summary for Pond 22P: Barn
Inflow A	rea =	0.055 ac,100.0	0% Impervious, Inflow Depth > 6.27" for 50-YR 24HR event
Inflow	=	0.34 cfs @ 12	.09 hrs, Volume= 0.028 af
Outflow	=	0.06 cfs @ 12	.54 hrs, Volume= 0.028 af, Atten= 82%, Lag= 27.1 min
Discard	ed =	0.06 cfs @ 12	.54 hrs, Volume= 0.028 af
Seconda	ary =	0.00 cfs @ 0	.00 hrs, Volume= 0.000 af
Rout	ed to React	h AP3 : Analysis	S Point 3
Routing	by Dyn-Sto	r-Ind method, T	ïme Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3
Peak El	ev= 171.46'	@ 12.54 hrs \$	Surf.Area= 0.009 ac Storage= 0.012 af
Plug-Flo Center-o	ow detentior of-Mass det	n time= 120.4 m . time= 110.5 m	in calculated for 0.028 af (98% of inflow) in (854.0 - 743.5)
<u>Volume</u>	Inver	t Avail.Storag	ge Storage Description
#1	168.15	0.013	af 4.00'W x 95.00'L x 3.85'H Prismatoid 0.034 af Overall x 40.0% Voids
Device	Routing	Invert	Outlet Devices
#0	<u> </u>		
#0	Secondary	y 172.00'	Automatic Storage Overflow (Discharged without head)

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Conductivity to Groundwater Elevation = 168.00' Phase-In= 0.10'

Discarded OutFlow Max=0.06 cfs @ 12.54 hrs HW=171.46' (Free Discharge) **1=Exfiltration** (Controls 0.06 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=168.15' TW=0.00' (Dynamic Tailwater)

Summary for Pond 23P: Drip Edge

Inflow Area = 0.013 ac, 15.85% Impervious, Inflow Depth > 4.78" for 50-YR 24HR event Inflow = 0.07 cfs @ 12.09 hrs, Volume= 0.005 af Outflow = 0.00 cfs @ 14.88 hrs, Volume= 0.003 af, Atten= 95%, Lag= 167.7 min Discarded = 0.00 cfs @ 14.88 hrs, Volume= 0.003 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Routed to Reach AP3 : Analysis Point 3 0.000 frs				
Routing by Dyn-S Peak Elev= 171.8	or-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 ' @ 14.88 hrs Surf.Area= 0.003 ac Storage= 0.003 af			
Plug-Flow detention Center-of-Mass de	n time= 323.3 min calculated for 0.003 af (61% of inflow) t. time= 222.1 min(1,019.3 - 797.2)			
Volume Inve	t Avail. Storage Storage Description			
#1 169.0	0' 0.003 af 3.00'W x 40.00'L x 3.00'H Prismatoid 0.008 af Overall x 40.0% Voids			
Device Routing				
#0 Seconda #1 Discarde	y 172.00' Automatic Storage Overflow (Discharged without head) 169.00' 0.300 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 168.00' Phase-In= 0.10'			
Discarded OutFlow Max=0.00 cfs @ 14.88 hrs HW=171.87' (Free Discharge) 1=Exfiltration (Controls 0.00 cfs)				
Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=169.00' TW=0.00' (Dynamic Tailwater)				
	Summary for Pond 24P: Plunge Pool with Culvert Outlet			
Inflow Area = Inflow =	0.213 ac, 18.90% Impervious, Inflow Depth > 4.13" for 50-YR 24HR event 0.89 cfs @ 12.14 hrs, Volume= 0.073 af			

0.073 af

Routing by Dyn-Stor-Ind method,	Time Span= 0.00-2	24.00 hrs, dt= 0.05 hrs / 3
Peak Elev= 193.44' @ 12.15 hrs	Surf.Area= 127 sf	Storage= 39 cf

Plug-Flow detention time= 1.7 min calculated for 0.073 af (100% of inflow) Center-of-Mass det. time= 1.2 min (817.3 - 816.2)

0.88 cfs @ 12.15 hrs, Volume=

Primary

=

Routed to Reach 3R : Culvert

22201-PROPOS Prepared by Jone HydroCAD® 10.20-3	s & Beach Engin s & No 00762 © 202	eers Inc 3 HydroCAD Softwa	re Solutions LLC	Printed	3/22/2024 Page 66
			c.		-
Volume Invel	rt Avail.Storage	e Storage Descri	ption Data (Prismatic) is	tod bolow (Pocolo)	
#1 193.00	4750	Custom Stage			
Elevation	Surf.Area I	nc.Store Cu	m.Store		
(feet)	(sq-ft) (cu	bic-feet) (cu	<u>pic-feet)</u>		
193.00	51	0	0		
194.00	222	137	137		
195.00	400	228	475		
Device Routing	Invert O	utlet Devices			
#1 Primary	193.00' 1 5	.0" Round Culve	rt		
	L=	50.0' CPP, squa	re edge headwall, k	(e= 0.500	
	In	et / Outlet Invert=	193.00' / 192.50' S	= 0.0100 '/' Cc= 0.9	900
	n=	0.012, Flow Area	= 1.23 ST		
Primary OutFlow 1=Culvert (Inle	Max=0.88 cfs @ 1 t Controls 0.88 cfs	2.15 hrs HW=193 @ 2.26 fps)	.44' TW=192.58' (I	Dynamic Tailwater)	
	Sun	mary for Pond	25P: Drip Edge		
Inflow Area = Inflow =	0.012 ac,100.00%	b Impervious, Inflo hrs. Volume=	w Depth > 6.27" 0.006 af	for 50-YR 24HR ev	ent
Outflow = Discarded =	0.02 cfs @ 12.44	hrs, Volume=	0.006 af, Atter	n= 73%, Lag= 21.3	min
Secondary =	0.00 cfs @ 0.00	hrs, Volume=	0.000 af		
Routed to Reac	h 6R : Flow Throu	gh 5S			
Routing by Dyn-Sto Peak Elev= 195.52	or-Ind method, Tim ' @ 12.44 hrs Su	e Span= 0.00-24.0 f.Area= 0.003 ac	0 hrs, dt= 0.05 hrs / Storage= 0.002 af	3	
Plug-Flow detention	n time= 63.9 min c t. time= 57.6 min (alculated for 0.006 801.1 - 743.5)	at (99% of inflow)		
Volume Inve	rt Avail.Storage	Storage Descrip	tion		
#1 193.75	5' 0.003 af	3.00'W x 41.00'l	x 2.25'H Prismato	id	
		0.006 af Overall	x 40.0% Voids		
Device Routing	Invert O	utlet Devices			
#0 Secondar	y 196.00' A i	utomatic Storage	Overflow (Discharg	ged without head)	
#1 Discarded	d 193.75' 0. Co	300 in/hr Exfiltrat	ion over Surface and and water Elevation =	ea 193.67' Phase-In	= 0.10'
Discarded OutFlow Max=0.02 cfs @ 12.44 hrs HW=195.51' (Free Discharge)					
Secondary OutFlo	w Max=0.00 cfs @	0.00 hrs HW=19	3.75' TW=196.00'	(Dynamic Tailwater)

22201-PROPOSED	Type III 24-hr	100-YR 24HR Rail	nfall=7.77"
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Summary for Subcatchment 1S: 1S

Runoff = 8.11 cfs @ 12.27 hrs, Volume= Routed to Reach AP1 : Analysis Point 1 0.852 af, Depth> 4.59"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR 24HR Rainfall=7.77"

Ar	rea (sf)	CN	Description		
	930	98	98 Roofs, HSG C		
	1,120	98	Paved parking, HSG C		
	47,794	70	Woods, Good, HSG C		
	23,377	74	>75% Grass cover, Good, HSG C		
	23,763	77	Woods, Good, HSG D		
	42	80	>75% Gras	s cover, Go	ood, HSG D
	97,026	73	Weighted A	verage	
	94,976		97.89% Pe	rvious Area	
	2,050		2.11% Impe	ervious Are	а
Tc	Length	Slope	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	
16.6	100	0.0433	3 0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
1.4	113	0.0708	3 1.33		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
1.4	70	0.0286	6 0.85		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.5	37	0.054	1.16		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
19.9	320	Total			

Summary for Subcatchment 2S: 2S

Runoff = 5.49 cfs @ 12.25 hrs, Volume= 0.556 af, Depth> 4.37" Routed to Reach AP1 : Analysis Point 1

Area (sf)	CN	Description
1,242	82	Dirt roads, HSG B
19,492	55	Woods, Good, HSG B
45,842	77	Woods, Good, HSG D
66,576 66,576	71	Weighted Average 100.00% Pervious Area
22201-PROPOSED	Type III 24-hr	100-YR 24HR Rainfall=7.77"
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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.3	82	0.0610	0.11		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
2.9	18	0.1111	0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
0.2	21	0.1111	1.67		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.4	30	0.0571	1.19		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
2.4	139	0.0367	0.96		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps

18.2 290 Total

Summary for Subcatchment 3S: 3S

Runoff	=	3.18 cfs @	12.26 hrs,	Volume=
Route	d to Re	each AP2 : Anal	ysis Point 2	

0.328 af, Depth> 4.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR 24HR Rainfall=7.77"

A	rea (sf)	CN [Description					
	27,514	70 \	Woods, Good, HSG C					
	11,825	74 >	>75% Gras	s cover, Go	ood, HSG C			
	39,339	71 \	Neighted A	verage				
	39,339		100.00% Pe	ervious Are	а			
Тс	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
10.6	81	0.0123	0.13		Sheet Flow,			
					Grass: Short n= 0.150 P2= 2.90"			
7.3	19	0.0123	0.04		Sheet Flow,			
					Woods: Light underbrush n= 0.400 P2= 2.90"			
1.2	40	0.0123	0.55		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
19.1	140	Total						

Summary for Subcatchment 4S: 4S

Runoff = 1.31 cfs @ 12.35 hrs, Volume= 0.152 af, Depth> 2.93" Routed to Reach AP3 : Analysis Point 3

22201-	PROPO	SED			Type III 24-hr 100-YR 24HR Rainfall=7.77'
Prepare	d by Jor	ies & Bea	ach Engir	neers Inc	Printed 3/22/2024
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A	rea (sf)	CN D	escription		
	1.810	82 D	irt roads.	HSG B	
	19.394	55 W	/oods. Go	od. HSG B	
	5,981	61 >	75% Ġras	s cover, Go	ood, HSG B
	27,185	58 W	/eighted A	verage	
	27,185	1	00.00% P	ervious Are	a
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
9.6	49	0.0408	0.09		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
12.8	51	0.0213	0.07		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
1.0	43	0.0213	0.73		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.2	51	0.0588	3.90		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
23.6	194	Total			

Summary for Subcatchment 5S: 5S

Runoff = 6.33 cfs @ 12.46 hrs, Volume= Routed to Reach AP4 : Analysis Point 4 0.823 af, Depth> 3.79"

CN	Description
82	Dirt roads, HSG B
55	Woods, Good, HSG B
87	Dirt roads, HSG C
74	>75% Grass cover, Good, HSG C
70	Woods, Good, HSG C
89	Dirt roads, HSG D
77	Woods, Good, HSG D
66	Weighted Average
	100.00% Pervious Area
	CN 82 55 87 74 70 89 77 66

22201-PROPOSED	Type III 24-hr	100-YR 24HR Rainfall=7.77"
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Тс	l enath	Slope	Velocity	Canacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Decemption
 21.0	100	0.0239	0.08		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
0.4	17	0.0239	0.77		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.8	48	0.0417	1.02		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
1.2	94	0.0638	1.26		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
2.9	116	0.0172	0.66		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.6	51	0.0784	1.40		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
5.5	176	0.0114	0.53		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps

32.4 602 Total

Summary for Subcatchment 6S: 6S

0.135 af, Depth> 5.17"

Runoff	=	1.65 cfs	@ 12.	13 hrs,	Volume=
Routed	l to	Pond 1P : Isola	ated We	etland	

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR 24HR Rainfall=7.77"

A	rea (sf)	CN	Description					
	2,925	98	Paved park	ing, HSG C	;			
	5,274	74	>75% Gras	s cover, Go	ood, HSG C			
	5,399	70	Woods, Go	od, HSG C				
	13,598	78	Weighted Average					
	10,673		78.49% Pervious Area					
	2,925		21.51% Impervious Area					
_		~		• •				
TC	Length	Slope	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)				
9.3	92	0.0217	7 0.16		Sheet Flow,			
					Grass: Short	n= 0.150	P2= 2.90"	

Summary for Subcatchment 7S: 7S

Runoff	=	6.61 cfs @	12.32 hrs,	Volume=	0.739 af,	Depth> 4.59"
Routed	to Pond	2P : Depres	sion in Woo	ds		

22201-	PROPO	SED			Type III 24-hr 100-YR 24HR Rainfall=7.77"
Prepare	ed by Jon	ies & Be	each Engir	neers Inc	Printed 3/22/2024
<u>HydroCA</u>	D® 10.20	-3c s/n 0	0762 © 202	23 HydroCA	D Software Solutions LLC Page 71
A	rea (sf)	CN	Description		
	898	98	Roofs, HSC	ЭC	
	2,014	98 I	Paved park	ing, HSG C	
	37,527	70	Woods, Go	od, HSG C	
	33,711	74 :	>75% Gras	s cover, Go	bod, HSG C
	9,806	77	Woods, Go	od, HSG D	
	247	80 :	<u>>75% Gras</u>	s cover, Go	ood, HSG D
	84,203	73	Weighted A	verage	
	81,291	ę	96.54% Pe	rvious Area	
	2,912	4	3.46% Impe	ervious Are	а
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.2	13	0.0200	0.87		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 2.90"
1.4	20	0.1200	0.24		Sheet Flow,
					Grass: Short n= 0.150 P2= 2.90"
7.3	39	0.0513	0.09		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
7.3	28	0.0260	0.06		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.90"
2.6	127	0.0260	0.81		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.8	75	0.1067	1.63		Shallow Concentrated Flow,
					Woodland Kv= 5.0 tps
1.0	56	0.0357	0.94		Shallow Concentrated Flow,
	00		4 5 4		Woodland Kv= 5.0 fps
0.2	22	0.0909	1.51		Shallow Concentrated Flow,
0.0	70	0.0405	0.50		vvoodiand KV= 5.0 fps
2.3	76	0.0125	0.56		Snallow Concentrated Flow,
23.1	456	l otal			

Summary for Subcatchment 9S: 9S

Runoff = 3.40 cfs @ 12.31 hrs, Volume= 0.378 af, Depth> 4.81" Routed to Reach 3R : Culvert

Area (sf)	CN	Description
704	98	Roofs, HSG C
2,162	98	Paved parking, HSG C
8,023	70	Woods, Good, HSG C
30,200	74	>75% Grass cover, Good, HSG C
41,089	75	Weighted Average
38,223		93.02% Pervious Area
2,866		6.98% Impervious Area

22201-	PROPO	SED			Type III 24-hr	100-YR 2	24HR Rainfa	hll=7.77'
Prepare	d by Jor	es & Be	ach Engir	eers Inc			Printed 3/2	22/2024
HydroCA	D® 10.20	-3c_s/n 00	762 © 202	3 HydroCA	D Software Solutions LLC		F	<u>Page 72</u>
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
20.7	100	0.0248	0.08		Sheet Flow,			
0.4	21	0.0248	0.79		Woods: Light underbrush Shallow Concentrated Fle Woodland Kv= 5.0 fps	n= 0.400 ow,	P2= 2.90"	

22.8 211 Total

90 0.0167

1.7

Summary for Subcatchment 10S: 10S

Shallow Concentrated Flow.

Short Grass Pasture Kv= 7.0 fps

Runoff = 2.80 cfs @ 12.09 hrs, Volume= 0.214 af, Depth> 6.34" Routed to Pond 3P : Center of Cul De Sac

0.90

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR 24HR Rainfall=7.77"

Are	a (sf)	CN	Description		
	728	98	Roofs, HSC	θC	
ę	9,516	98	Paved park	ing, HSG C	C
	7,442	74	>75% Ġras	s cover, Go	bood, HSG C
1	7,686	88	Weighted A	verage	
-	7,442		42.08% Pe	rvious Area	a
1(0,244		57.92% Imp	pervious Ar	rea
Tc l	_ength	Slope	e Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
6.0					Direct Entry,
					-

Summary for Subcatchment 11S: 11S

Runoff = 1.13 cfs @ 12.14 hrs, Volume= 0.094 af, Depth> 5.29" Routed to Pond 24P : Plunge Pool with Culvert Outlet

Ar	ea (sf)	CN	Description
	1,756	98	Paved parking, HSG C
	7,537	74	>75% Grass cover, Good, HSG C
	9,293	79	Weighted Average
	7,537		81.10% Pervious Area
	1,756		18.90% Impervious Area

00004					
22201-	PROPO	SED			Type III 24-nr 100-YR 24HR Rainfall=7.77
Prepare	ed by Jon		ach Engir	ieers inc	
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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
97	73	0.0123	0.13		Sheet Flow.
0.1		0.0.20	0.10		Grass: Short n= 0.150 P2= 2.90"
0.5	121	0.0165	4.25	17.00	Trap/Vee/Rect Channel Flow,
					Bot.W=1.00' D=1.00' Z= 3.0 '/' Top.W=7.00'
					n= 0.030 Stream, clean & straight
10.2	194	Total			
			Summa	ry for Sul	ocatchment 12S: Units 5&6
				-	
Runoff	=	0.17 cf	s @ 12.0	9 hrs, Volu	me= 0.014 af, Depth> 7.53"
Route	ed to Pon	d 4P : Dr	ip Edge	,	
Runoff b	Y SCS TF	R-20 met	hod, UH=S	SCS, Weigh	ited-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III	24-hr 100	0-YR 24H	IR Rainfall	=7.77"	
A	rea (sf)	CN E	Description		
	838	98 F	Poofs HSC	C C	

	838	98	Roofs, HSC	G C	
	156	98	Water Surfa	ace, HSG C	
	994	98	Weighted A	verage	
	994		100.00% In	npervious A	vrea
Tc	Length	Slop	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	
6.0					Direct Entry,

Summary for Subcatchment 13S: Unit 5

Runoff = 0.10 cfs @ 12.09 hrs, Volume= 0.008 af, Depth> 7.53" Routed to Pond 5P : Drip Edge

A	rea (sf)	CN	Description		
	395	98	Roofs, HSC	G C	
	185	98	Water Surfa	ace, HSG C	C
	580	98	Weighted A	verage	
	580		100.00% In	npervious A	Area
т	L a ca antila	01	• \/_l;t.	0	Description
IC	Length	Slop	e velocity	Capacity	Description
(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)	
6.0					Direct Entry,

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Summary for Subcatchment 14S: Units 3&4

0.015 af, Depth> 7.53"

Runoff = 0.18 cfs @ 12.09 hrs, Volume= Routed to Pond 6P : Drip Edge

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR 24HR Rainfall=7.77"

Are	a (sf)	CN	Description		
	838	98	Roofs, HSG	S C	
	208	98	Water Surfa	ace, HSG C	
	1,046	98	Weighted A	verage	
	1,046		100.00% In	pervious A	rea
Tc I _(min)	_ength (feet)	Slop (ft/fl	e Velocity) (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,
			Summ	ary for S	ubcatchment 15S: Unit 4

Runoff = 0.09 cfs @ 12.09 hrs, Volume= 0.007 af, Depth> 7.53" Routed to Pond 7P : Drip Edge

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR 24HR Rainfall=7.77"

Α	rea (sf)	CN	Description				
	395	98	Roofs, HSC	G C			
	103	98	Water Surfa	ace, HSG C			
	498	98	Weighted A	verage			
	498		100.00% In	npervious A	rea		
Tc	Length	Slope	e Velocity	Capacity	Description		
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)			
6.0					Direct Entry,		

Summary for Subcatchment 16S: Unit 3

Runoff = 0.09 cfs @ 12.09 hrs, Volume= 0.007 af, Depth> 7.53" Routed to Pond 8P : Drip Edge

 Area (sf)	CN	Description
395	98	Roofs, HSG C
 123	98	Water Surface, HSG C
518	98	Weighted Average
518		100.00% Impervious Area

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Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)
6.0 Direct Entry,
Summary for Subcatchment 17S: Units 1&2
Runoff = 0.18 cfs @ 12.09 hrs, Volume= 0.015 af, Depth> 7.53" Routed to Pond 10P : Drip Edge
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR 24HR Rainfall=7.77"
Area (sf) CN Description
838 98 Roofs, HSG C 208 98 Water Surface, HSG C
1,04698Weighted Average1,046100.00% Impervious Area
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)
6.0 Direct Entry,
Summary for Subcatchment 18S: Unit 1
Runoff = 0.09 cfs @ 12.09 hrs, Volume= 0.007 af, Depth> 7.53" Routed to Pond 11P : Drip Edge
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR 24HR Rainfall=7.77"
Area (sf) CN Description
395 98 Roofs, HSG C
49898Weighted Average498100.00% Impervious Area

TcLengthSlopeVelocityCapacityDescription(min)(feet)(ft/ft)(ft/sec)(cfs)

6.0

Direct Entry,

Summary for Subcatchment 19S: 19S

Runoff = 0.41 cfs @ 12.09 hrs, Volume= 0.034 af, Depth> 7.53" Routed to Pond 20P : Barn

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A	rea (sf)	CN	Description		
	1,995	98	Roofs, HSC	βB	
	380	98	Water Surfa	ace, HSG B	В
	2,375	98	Weighted A	verage	
	2,375		100.00% In	npervious A	Area
-		01		0	
IC	Length	Slope	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	
6.0					Direct Entry,

Summary for Subcatchment 20S: 20S

0.41 cfs @ 12.09 hrs, Volume= Runoff 0.034 af, Depth> 7.53" = Routed to Pond 22P : Barn

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR 24HR Rainfall=7.77"

Α	rea (sf)	CN	Description		
	1,995	98	Roofs, HSG	βB	
	380	98	Water Surfa	ace, HSG B	В
	2,375	98	Weighted A	verage	
	2,375		100.00% In	npervious A	Area
Tc	Length	Slop	e Velocity	Capacity	Description
(min)	(feet)	(ft/f	i) (ft/sec)	(cfs)	
6.0					Direct Entry,
					•

Summary for Subcatchment 21S: Gravel Trail

0.09 cfs @ 12.09 hrs, Volume= 0.007 af, Depth> 5.99" Runoff = Routed to Pond 23P : Drip Edge

A	rea (sf)	CN	Description		
	483	82	Dirt roads,	HSG B	
	91	98	Water Surfa	ace, HSG B	В
	574	85	Weighted A	verage	
	483		84.15% Pe	rvious Area	a
	91		15.85% Imp	pervious Ar	rea
Та	Longth	Clan	a Valacity	Canaaitu	Description
IC	Lengin	Siop	e velocity	Capacity	Description
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	
6.0					Direct Entry,

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Summary for Subcatchment 22S: Unit 2

0.007 af, Depth> 7.53"

Runoff = 0.09 cfs @ 12.09 hrs, Volume= Routed to Pond 25P : Drip Edge

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Type III 24-hr 100-YR 24HR Rainfall=7.77"

A	rea (sf)	CN	Description		
	395	98	Roofs, HSC	G C	
	123	98	Water Surfa	ace, HSG C	
	518	98	Weighted A	verage	
	518		100.00% In	npervious A	Area
Тс	Length	Slop	e Velocity	Capacity	Description
(min)	(feet)	(ft/f	i) (ft/sec)	(cfs)	
6.0					Direct Entry,

Summary for Reach 1R: Flow Through 9S

[80] Warning: Exceeded Pond 1P by 0.04' @ 12.70 hrs (0.50 cfs 0.032 af)

Inflow Area = 0.312 ac, 21.51% Impervious, Inflow Depth = 3.00" for 100-YR 24HR event Inflow = 1.91 cfs @ 12.15 hrs, Volume= 0.078 af Outflow = 1.61 cfs @ 12.15 hrs, Volume= 0.078 af, Atten= 16%, Lag= 0.3 min Routed to Reach 3R : Culvert

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 1.57 fps, Min. Travel Time= 1.5 min Avg. Velocity = 0.48 fps, Avg. Travel Time= 4.8 min

Peak Storage= 143 cf @ 12.15 hrs Average Depth at Peak Storage= 0.11', Surface Width= 14.04' Bank-Full Depth= 0.50' Flow Area= 10.0 sf, Capacity= 43.14 cfs

30.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight Length= 140.0' Slope= 0.0329 '/' Inlet Invert= 196.40', Outlet Invert= 191.80'

‡

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Summary for Reach 3R: Culvert

[52] Hint: Inlet/Outlet conditions not evaluated

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[62] Hint: Exceeded Reach 1R OUTLET depth by 0.90' @ 12.20 hrs

[64] Warning: Exceeded Reach 1R outlet bank by 0.51' @ 12.21 hrs

Inflow Area =1.469 ac, 11.80% Impervious, Inflow Depth > 4.50" for 100-YR 24HR eventInflow =5.37 cfs @ 12.21 hrs, Volume=0.550 afOutflow =5.40 cfs @ 12.21 hrs, Volume=0.550 af, Atten= 0%, Lag= 0.0 minRouted to Pond 3P : Center of Cul De SacSac

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 5.09 fps, Min. Travel Time= 0.2 min Avg. Velocity = 2.05 fps, Avg. Travel Time= 0.4 min

Peak Storage= 52 cf @ 12.21 hrs Average Depth at Peak Storage= 1.01', Surface Width= 0.99' Bank-Full Depth= 1.25' Flow Area= 1.2 sf, Capacity= 5.48 cfs

15.0" Round Pipe n= 0.012 Length= 49.0' Slope= 0.0061 '/' Inlet Invert= 191.80', Outlet Invert= 191.50'



Summary for Reach 4R: Swale

 Inflow Area =
 1.875 ac, 21.79% Impervious, Inflow Depth > 4.12" for 100-YR 24HR event

 Inflow =
 3.39 cfs @
 12.57 hrs, Volume=
 0.644 af

 Outflow =
 3.39 cfs @
 12.58 hrs, Volume=
 0.643 af, Atten= 0%, Lag= 0.3 min

 Routed to Reach 5R : Flow Through 1S

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Max. Velocity= 4.29 fps, Min. Travel Time= 0.5 min Avg. Velocity = 1.94 fps, Avg. Travel Time= 1.0 min

Peak Storage= 95 cf @ 12.58 hrs Average Depth at Peak Storage= 0.37', Surface Width= 3.24' Bank-Full Depth= 1.00' Flow Area= 4.0 sf, Capacity= 30.09 cfs

1.00' x 1.00' deep channel, n= 0.030 Stream, clean & straight Side Slope Z-value= 3.0 '/' Top Width= 7.00' Length= 120.0' Slope= 0.0517 '/' Inlet Invert= 189.70', Outlet Invert= 183.50'



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30.00' x 0.50' deep Parabolic Channel, n= 0.030 Stream, clean & straight Length= 600.0' Slope= 0.0367 '/' Inlet Invert= 196.00', Outlet Invert= 174.00'



Summary for Reach AP1: Analysis Point 1

[40] Hint: Not Described (Outflow=Inflow)

Inflow A	Area	=	5.631 ac,	8.09% Impervious,	Inflow Depth > 4.	37" for 100-YR 24HR event
Inflow	:	=	14.08 cfs @	12.27 hrs, Volume	= 2.050 af	
Outflov	V	=	14.08 cfs @	12.27 hrs, Volume	= 2.050 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Analysis Point 2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Ar	ea =	0.903 ac,	0.00% Impervious,	Inflow Depth > 4.3	36" for 100-YR 24HR event
Inflow	=	3.18 cfs @	12.26 hrs, Volume	= 0.328 af	
Outflow	=	3.18 cfs @	12.26 hrs, Volume	= 0.328 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Analysis Point 3

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	0.624 ac,	0.00% Impervious,	Inflow Depth > 2.9	97" for 100-YR 24HR event
Inflow	=	1.37 cfs @	12.40 hrs, Volume	= 0.154 af	
Outflow	=	1.37 cfs @	12.40 hrs, Volume	= 0.154 af,	Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Analysis Point 4

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	2.605 ac,	0.00% Impervious, Inflow	Depth > 3.79"	for 100-YR 24HR event
Inflow	=	6.33 cfs @	12.46 hrs, Volume=	0.823 af	
Outflow	=	6.33 cfs @	12.46 hrs, Volume=	0.823 af, Atte	en= 0%, Lag= 0.0 min

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP5: Analysis Point 5

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	1.933 ac,	3.46% Impervious, I	nflow Depth > 3.49"	for 100-YR 24HR event
Inflow	=	6.32 cfs @	12.38 hrs, Volume=	0.563 af	
Outflow	=	6.32 cfs @	12.38 hrs, Volume=	0.563 af, Atte	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Pond 1P: Isolated Wetland

[93] Warning: Storage range exceeded by 0.14'

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=62)

Inflow Area	ı =	0.312 ac,	21.51% Imp	ervious,	Inflow	Depth >	5.1	7" for	100	-YR 24	HR event
Inflow	=	1.65 cfs @	12.13 hrs,	Volume	=	0.135	af				
Outflow	=	1.94 cfs @	12.15 hrs,	Volume	=	0.109	af,	Atten=	0%,	Lag= 0	.9 min
Discarded	=	0.03 cfs @	12.15 hrs,	Volume	=	0.033	af				
Primary	=	1.91 cfs @	12.15 hrs,	Volume	=	0.078	af				
Routed to Reach 1R : Flow Through 9S											

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 196.55' @ 12.15 hrs Surf.Area= 2,828 sf Storage= 1,191 cf

Plug-Flow detention time= 119.4 min calculated for 0.109 af (81% of inflow) Center-of-Mass det. time= 46.2 min (857.0 - 810.8)

Volume	Inve	rt Avail.	Storage	Storage Description	า		
#1	195.3	0'	1,191 cf	Custom Stage Dat	t a (Irregular) Listed	below (Recalc)	
Elevatio	on S et)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft <u>)</u>	
195.3 196.0 196.4 196.4	30 00 40 41	235 1,050 2,828 2,828	72.0 148.0 211.0 211.0	0 416 747 28	0 416 1,163 1,191	235 1,568 3,369 3,371	
Device	Routing	Inv	ert Outle	et Devices			
#1	Primary	196.4	40' 20.0 Hea 2.50 Coe 2.65	' long x 6.0' breadt d (feet) 0.20 0.40 0 3.00 3.50 4.00 4. f. (English) 2.37 2.5 2.66 2.66 2.67 2.	Broad-Crested 0.60 0.80 1.00 1.2 50 5.00 5.50 51 2.70 2.68 2.68 69 2.72 2.76 2.83 2.72 2.76 2.83	Rectangular Weir 20 1.40 1.60 1.80 2.67 2.65 2.65 2.	2.00 65
#2	Discardeo	d 195.3	30' 0.30 Con	0 in/hr Exfiltration (ductivity to Groundw	over Surface area ater Elevation = 19	4.80' Phase-In= ().10'

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Discarded OutFlow Max=0.03 cfs @ 12.15 hrs HW=196.55' (Free Discharge) **2=Exfiltration** (Controls 0.03 cfs)

Primary OutFlow Max=1.86 cfs @ 12.15 hrs HW=196.55' TW=196.51' (Dynamic Tailwater) **1=Broad-Crested Rectangular Weir**(Weir Controls 1.86 cfs @ 0.62 fps)

Summary for Pond 2P: Depression in Woods

Inflow Area	a =	1.933 ac,	3.46% Imperviou	s, Inflow De	epth >	4.60"	for 100	-YR 24HR event
Inflow	=	6.66 cfs @	12.32 hrs, Volui	ne=	0.742	af		
Outflow	=	6.43 cfs @	12.38 hrs, Volui	ne=	0.667	af, Atte	n= 3%,	Lag= 3.5 min
Discarded	=	0.11 cfs @	12.38 hrs, Volui	ne=	0.104	af		
Primary	=	6.32 cfs @	12.38 hrs, Volui	ne=	0.563	af		
Routed to Reach AP5 : Analysis Point 5								

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 176.65' @ 12.38 hrs Surf.Area= 7,514 sf Storage= 5,082 cf

Plug-Flow detention time= 72.8 min calculated for 0.665 af (90% of inflow) Center-of-Mass det. time= 25.6 min (858.1 - 832.5)

Volume	Inve	ert Avai	il.Storage	Storage Descriptio	n		
#1	175.7	'0'	5,471 cf	Custom Stage Da	ita (Irregular) Listed b	pelow (Recalc)	
Elevatio (fee	on et)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft <u>)</u>	
175.7 176.0 176.4 176.7	70 00 40 70	2,764 3,841 7,514 7,514	204.0 265.0 341.0 341.0	0 986 2,230 2,254	0 986 3,217 5,471	2,764 5,042 8,709 8,811	
Device	Routing	In	vert Out	et Devices			
#1	Primary	176	5.40' 20.0 Hea 2.50 Coe	' long x 2.0' bread d (feet) 0.20 0.40 3.00 3.50 f (English) 2.54 2	th Broad-Crested R 0.60 0.80 1.00 1.20	ectangular Weir 1.40 1.60 1.80	2.00
#2	Discarde	2.0 2.0 Discarded 175.70' 0. 0 Co		3.07 3.20 3.32 0 in/hr Exfiltration ductivity to Groundv	over Surface area vater Elevation = 175	.20' Phase-In=	0.10'

Discarded OutFlow Max=0.11 cfs @ 12.38 hrs HW=176.65' (Free Discharge) **2=Exfiltration** (Controls 0.11 cfs)

Primary OutFlow Max=6.29 cfs @ 12.38 hrs HW=176.65' TW=0.00' (Dynamic Tailwater) ←1=Broad-Crested Rectangular Weir (Weir Controls 6.29 cfs @ 1.27 fps)

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Summary for Pond 3P: Center of Cul De Sac

[63] Warning: Exceeded Reach 3R INLET depth by 2.55' @ 12.75 hrs

Inflow Area = 1.875 ac, 21.79% Impervious, Inflow Depth > 4.90" for 100-YR 24HR event Inflow = 7.27 cfs @ 12.15 hrs, Volume= 0.765 af 3.38 cfs @ 12.57 hrs, Volume= Outflow 0.643 af, Atten= 54%, Lag= 25.7 min = Primary = 3.38 cfs @ 12.57 hrs, Volume= 0.643 af Routed to Reach 4R : Swale

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 194.93' @ 12.57 hrs Surf.Area= 4,459 sf Storage= 13,965 cf

Plug-Flow detention time= 195.3 min calculated for 0.641 af (84% of inflow) Center-of-Mass det. time= 132.6 min (942.2 - 809.6)

Volume	Invert	Avail.Stor	age Storage D	escription		
#1	190.00'	16,17	1 cf Custom S	tage Data (Pri	smatic)Listed below (F	Recalc)
Elevatio (fee	n Sı t)	urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
190.0 191.0 192.0 194.0 195.0	0 0 0 0	1,491 1,934 2,483 3,751 4 514	0 1,713 2,209 6,234 4 133	0 1,713 3,921 10,155 14 288		
195.4	0	4,903	1,883	16,171		
Device	Routing	Invert	Outlet Devices			
#1	Primary	190.00'	15.0" Round C L= 47.0' CPP, Inlet / Outlet Inv n= 0.012. Flow	ulvert projecting, no h ert= 190.00' / 1 Area= 1.23 sf	neadwall, Ke= 0.900 89.70' S= 0.0064 '/'	Cc= 0.900
#2	Device 1	190.00'	2.0" Vert. Orific	ce/Grate C= 0).600 Limited to weir f	low at low heads
#3 #4 #5	Device 1 Device 1 Device 1	191.30' 193.40' 193.65'	2.0" Vert. Orific 2.0" Vert. Orific 0.7" W x 9.6" H Limited to weir f	ce/Grate C= 0 ce/Grate C= 0 Vert. Orifice/(low at low head).600 Limited to weir f).600 Limited to weir f Grate C= 0.600 ds	low at low heads low at low heads
#6	Device 1	194.45'	12.0" Horiz. Or Limited to weir f	ifice/Grate C= low at low head	= 0.600 ds	
Primary	OutFlow M	lax=3.37 cfs (es 3.37 cfs of) 12.57 hrs HW= 9.67 cfs potentia	=194.93' TW=1 flow)	190.07' (Dynamic Tail	lwater)

-2=Orifice/Grate (Orifice Controls 0.23 cfs @ 10.60 fps)

-3=Orifice/Grate (Orifice Controls 0.20 cfs @ 9.06 fps)

-4=Orifice/Grate (Orifice Controls 0.13 cfs @ 5.78 fps)

-5=Orifice/Grate (Orifice Controls 0.21 cfs @ 4.46 fps)

-6=Orifice/Grate (Orifice Controls 2.61 cfs @ 3.32 fps)

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Summary for Pond 4P: Drip Edge

Inflow Area = 0.023 ac,100.00%	Impervious, Inflow Depth > 7.53" for 100-YR 24HR event				
Inflow = 0.17 cfs @ 12.09 I	hrs, Volume= 0.014 af				
Outflow = $0.16 \text{ cfs} @ 12.11$	hrs, Volume= 0.014 af, Atten= 4%, Lag= 1.4 min				
Discarded = $0.03 \text{ cfs} @ 12.00 \text{ cfs}$	hrs, Volume= 0.001 af				
Secondary = 0.14 cfs @ 12.11	nrs, volume= 0.003 at				
Routed to Pond 2P : Depression in	vvoods				
Routing by Dyn-Stor-Ind method, Time	Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3				
Peak Elev= 191.50' @ 12.00 hrs Surf.	Area= 0.004 ac Storage= 0.002 af				
Plug-Flow detention time= 46.1 min cal	culated for 0.014 af (99% of inflow)				
Center-of-Mass det. time= 41.1 min (7	82.2 - 741.2)				
Volume Invert Avail Storage	Storage Description				
#1 189.90' 0.002 af	3 00'W x 52 00'L x 1 60'H Prismatoid				
#1 100.00 0.002 al	0.006 af Overall x 40.0% Voids				
Device Routing Invert Out	let Devices				
#0 Secondary 191 50' Aut	comatic Storage Overflow (Discharged without head)				
#1 Discarded 189.90' 0.30	00 in/hr Exfiltration over Surface area				
Cor	iductivity to Groundwater Elevation = 189.83' Phase-In= 0.10'				
	5				
Discarded OutFlow Max=0.03 cfs @ 7	12.00 hrs HW=191.50' (Free Discharge)				
1=Exfiltration (Controls 0.03 cfs)					
Secondary OutElow Max-0.00 of a	12 11 brs. HW-101 50', TW-176 54', (Dynamic Tailwater)				
Secondary Outriow Max-0.00 cis @					
Sum	mary for Pond 5P: Drip Edge				
Inflow Area = 0.013 ac,100.00%	Impervious, Inflow Depth > 7.53" for 100-YR 24HR event				
Inflow = 0.10 cfs @ 12.09 l	hrs, Volume= 0.008 af				
Outflow = $0.03 \text{ cfs} @ 12.42$	hrs, Volume= 0.008 af, Atten= 71%, Lag= 19.9 min				
Discarded = $0.03 \text{ cfs} @ 12.42 \text{ l}$	nrs, Volume= 0.000 af				
Secondary = $0.00 \text{ cis} (0, 0.00)$	nrs, volume= 0.000 al				
Rouled to Reach 4R. Swale					
Pouting by Dyn Stor Ind method. Time	Shan- 0.00.24.00 hrs. $dt= 0.05$ hrs. / 3				
Peak Elev- 101 30' \oslash 12 42 hrs Surf	$\Delta r_{00} = 0.004 \text{ ac}$ Storage = 0.003 af				
Feak Liev- 191.39 @ 12.42 IIIS Sull.	Alea- 0.004 ac Stolage- 0.005 al				
Plug-Flow detention time= 56.3 min calculated for 0.008 at (99% of inflow)					
Center-of-Mass det. time= 50.1 min (7	91.2 - 741.2)				
Volume Invert Avail.Storage	Storage Description				
#1 189.90' 0.003 af	4.50'W x 41.00'L x 1.60'H Prismatoid				
	0.007 af Overall x 40.0% Voids				
Device Routing Invert Out	let Devices				

#0	Secondary	191.50'	Automatic Storage Overflow (Discharged without head)
#1	Discarded	189.90'	0.300 in/hr Exfiltration over Surface area

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Conductivity to Groundwater Elevation = 189.83' Phase-In= 0.10'

Discarded OutFlow Max=0.03 cfs @ 12.42 hrs HW=191.39' (Free Discharge) **1=Exfiltration** (Controls 0.03 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=189.90' TW=189.70' (Dynamic Tailwater)

Summary for Pond 6P: Drip Edge

Inflow Ar Inflow Outflow Discarde Seconda Route	nflow Area = 0.024 ac,100.00% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event nflow = 0.18 cfs @ 12.09 hrs, Volume= 0.015 af Outflow = 0.12 cfs @ 12.18 hrs, Volume= 0.015 af, Atten= 31%, Lag= 5.8 min Discarded = 0.09 cfs @ 12.15 hrs, Volume= 0.015 af Secondary = 0.03 cfs @ 12.18 hrs, Volume= 0.000 af Routed to Reach 5R : Flow Through 1S 15						
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 189.72' @ 12.15 hrs Surf.Area= 0.005 ac Storage= 0.002 af							
Plug-Flov	w detentior	n time= 19.4 min	calculated for 0.015 af (99% of inflow)				
Center-o	f-Mass det	. time= 16.1 min	(757.2 - 741.2)				
Volume	Inver	t Avail.Storag	ge Storage Description				
#1	188.52	2' 0.002 ;	af 4.00'W x 52.00'L x 1.20'H Prismatoid 0.006 af Overall x 40.0% Voids				
Device	Routing	Invert	Outlet Devices				
#0 #1	Secondar Discarded	y 189.72' 188.52'	Automatic Storage Overflow (Discharged without head) 0.300 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 188.50' Phase-In= 0.10'				
Discarded OutFlow Max=0.09 cfs @ 12.15 hrs HW=189.72' (Free Discharge)							
Secondary OutFlow Max=0.00 cfs @ 12.18 hrs HW=189.72' TW=183.55' (Dynamic Tailwater)							
Summary for Pond 7P: Drip Edge							

Inflow Area =	0.011 ac,100.00% Impervious, Inflow	Depth > 7.53" for 100-YR 24HR eve	ənt
Inflow =	0.09 cfs @ 12.09 hrs, Volume=	0.007 af	
Outflow =	0.03 cfs @ 12.42 hrs, Volume=	0.004 af, Atten= 66%, Lag= 19.8 m	in
Discarded =	0.00 cfs @ 12.35 hrs, Volume=	0.003 af	
Secondary =	0.03 cfs @ 12.42 hrs, Volume=	0.001 af	
Routed to Reac	h 4R : Swale		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 192.00'@ 12.35 hrs Surf.Area= 0.002 ac Storage= 0.004 af

Plug-Flow detention time= 278.3 min calculated for 0.004 af (58% of inflow) Center-of-Mass det. time= 162.1 min (903.2 - 741.2)

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Volume Invert Avail.Storage Storage Description				
#1 188.00' 0.004 af 2.50'W x 41.00'L x 4.00'H Prismatoid 0.009 af Overall x 40.0% Voids				
Device Routing Invert Outlet Devices				
#0Secondary192.00'Automatic Storage Overflow (Discharged without head)#1Discarded188.00'0.300 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 186.50'Phase-In= 0.10'				
Discarded OutFlow Max=0.00 cfs @ 12.35 hrs HW=192.00' (Free Discharge)				
Secondary OutFlow Max=0.00 cfs @ 12.42 hrs HW=192.00' TW=190.03' (Dynamic Tailwater)				
Summary for Pond 8P: Drip Edge				
Inflow Area = 0.012 ac,100.00% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event Inflow = 0.09 cfs @ 12.09 hrs, Volume= 0.007 af Outflow = 0.02 cfs @ 12.48 hrs, Volume= 0.007 af, Atten= 77%, Lag= 23.4 min Discarded = 0.02 cfs @ 12.48 hrs, Volume= 0.007 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Routed to Reach AP1 : Analysis Point 1 0.000 af 0.000 af				
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 189.91' @ 12.48 hrs Surf.Area= 0.003 ac Storage= 0.003 af				
Plug-Flow detention time= 79.6 min calculated for 0.007 af (99% of inflow) Center-of-Mass det. time= 73.2 min (814.3 - 741.2)				
Volume Invert Avail.Storage Storage Description				
#1 187.60' 0.003 af 3.00'W x 41.00'L x 2.40'H Prismatoid 0.007 af Overall x 40.0% Voids				
Device Routing Invert Outlet Devices				
#0Secondary190.00'Automatic Storage Overflow (Discharged without head)#1Discarded187.60'0.300 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 187.50'Phase-In= 0.10'				
Discarded OutFlow Max=0.02 cfs @ 12.48 hrs HW=189.91' (Free Discharge) -1=Exfiltration (Controls 0.02 cfs)				
Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=187.60' TW=0.00' (Dynamic Tailwater)				
Summary for Pond 10P: Drip Edge				
Inflow Area = 0.024 ac,100.00% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event Inflow = 0.18 cfs @ 12.09 hrs, Volume= 0.015 af Outflow = 0.04 cfs @ 12.52 hrs, Volume= 0.015 af, Atten= 80%, Lag= 25.8 min Discarded = 0.04 cfs @ 12.52 hrs, Volume= 0.015 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af				

Routed to Reach 3R : Culvert

22201-PROPOSED	Type III 24-hr	100-YR 24HR Rair	nfall=7.77"
Prepared by Jones & Beach Engineers Inc		Printed	3/22/2024
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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 195.84' @ 12.52 hrs Surf.Area= 0.005 ac Storage= 0.006 af

Plug-Flow detention time= 104.2 min calculated for 0.015 af (99% of inflow) Center-of-Mass det. time= 97.2 min (838.3 - 741.2)

Volume	Invert	Avail.Stora	ge Storage Description
#1	192.80'	0.006	af 4.00'W x 52.00'L x 3.20'H Prismatoid 0.015 af Overall x 40.0% Voids
Device	Routing	Invert	Outlet Devices
#0	Secondary	196.00'	Automatic Storage Overflow (Discharged without head)
#1	Discarded	192.80'	0.300 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 192.67' Phase-In= 0.10'

Discarded OutFlow Max=0.04 cfs @ 12.52 hrs HW=195.84' (Free Discharge) **1=Exfiltration** (Controls 0.04 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=192.80' TW=191.80' (Dynamic Tailwater)

Summary for Pond 11P: Drip Edge

Inflow Area =	0.011 ac,100.00% Impervious, Inflow	Depth > 7.53" f	or 100-YR 24HR event
Inflow =	0.09 cfs @ 12.09 hrs, Volume=	0.007 af	
Outflow =	0.04 cfs @_ 12.27 hrs, Volume=	0.007 af, Atten	= 55%, Lag= 10.9 min
Discarded =	0.04 cfs @_ 12.27 hrs, Volume=	0.007 af	-
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af	
Routed to Re	each 3R : Culvert		

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 195.28' @ 12.27 hrs Surf.Area= 0.002 ac Storage= 0.001 af

Plug-Flow detention time= 27.5 min calculated for 0.007 af (99% of inflow) Center-of-Mass det. time= 23.5 min (764.6 - 741.2)

Volume	Invert	Avail.Stora	ge Storage Description
#1	193.70'	0.002	af 2.50'W x 41.00'L x 2.30'H Prismatoid 0.005 af Overall x 40.0% Voids
Device	Routing	Invert	Outlet Devices
#0	Secondary	196.00'	Automatic Storage Overflow (Discharged without head)
#1	Discarded	193.70	Conductivity to Groundwater Elevation = 193.67' Phase-In= 0.10'
Discard	ed OutFlow	/lax=0.04 cfs	s @ 12.27 hrs HW=195.27' (Free Discharge)

1=Exfiltration (Controls 0.04 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=193.70' TW=191.80' (Dynamic Tailwater)

22201-PROPOSED	Type III 24-hr	100-YR 24HR Rainfall=7.77'
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Summary for Pond 20P: Barn

INNOW A	rea =	0.055 ac,100.0	10% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event			
Inflow	=	0.41 cfs @ 12	.09 hrs, Volume= 0.034 af			
Outriow	=	0.12 cfs @ 12	.42 hrs, Volume= 0.034 af, Atten= 70%, Lag= 20.3 min			
Discarde	ea =	0.07 cts @ 12	.40 hrs, Volume= 0.003 af			
Seconda	ary = ad ta Daaak		.42 nrs, volume= 0.000 af			
Rout	ed to Reacr	1 AP3 : Analysis	S POINT 3			
Routing	Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3					
Feak El	ev- 172.00	@ 12.40 115 3	Sull.Alea - 0.009 ac Stolage - 0.015 al			
Plug-Flo Center-o	w detentior of-Mass det	n time= 121.2 m . time= 109.4 m	in calculated for 0.034 af (98% of inflow) in (850.6 - 741.2)			
Volume	Inver	t Avail.Stora	ge Storage Description			
#1	168,15	' 0.013	af 4.00'W x 95.00'L x 3.85'H Prismatoid			
<i>//</i> 1	100.10	0.010	0.034 af Overall x 40.0% Voids			
Device	Routing	Invert	Outlet Devices			
#0	Secondary	/ 172.00'	Automatic Storage Overflow (Discharged without head)			
#1	Discarded	168.15'	0.300 in/hr Exfiltration over Surface area			
			Conductivity to Groundwater Elevation = 168.00' Phase-In= 0.10'			
			······································			
Discard 1=Ex	ed OutFlow	v Max=0.07 cfs Controls 0.07 c	a@ 12.40 hrs HW=172.00' (Free Discharge) fs)			
Second	ary OutFlo	w Max=0.00 cfs	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater)			
Second	ary OutFlo	w Max=0.00 cfs	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn			
Second	ary OutFlo rea =	w Max=0.00 cfs 0.055 ac,100.0	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn 00% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event			
Second Inflow A Inflow	ary OutFlo rea = =	w Max=0.00 cfs 0.055 ac,100.0 0.41 cfs @ 12	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn 0% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event .09 hrs, Volume= 0.034 af			
Second Inflow A Inflow Outflow	ary OutFlo rea = = =	w Max=0.00 cfs 0.055 ac,100.0 0.41 cfs @ 12 0.12 cfs @ 12	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn 0% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event .09 hrs, Volume= 0.034 af .42 hrs, Volume= 0.034 af, Atten= 70%, Lag= 20.3 min			
Second Inflow A Inflow Outflow Discarde	ary OutFlo rea = = = ed =	w Max=0.00 cfs 0.055 ac,100.0 0.41 cfs @ 12 0.12 cfs @ 12 0.07 cfs @ 12	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn 00% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event .09 hrs, Volume= 0.034 af .42 hrs, Volume= 0.034 af, Atten= 70%, Lag= 20.3 min .40 hrs, Volume= 0.033 af			
Second Inflow A Inflow Outflow Discarde Seconda	ary OutFlo rea = = ed = ary =	w Max=0.00 cfs 0.055 ac,100.0 0.41 cfs @ 12 0.12 cfs @ 12 0.07 cfs @ 12 0.05 cfs @ 12	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn 00% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event .09 hrs, Volume= 0.034 af .42 hrs, Volume= 0.033 af .42 hrs, Volume= 0.000 af			
Second Inflow A Inflow Outflow Discarde Seconda Rout	ary OutFlo rea = = = ed = ary = ed to Reach	w Max=0.00 cfs 0.055 ac,100.0 0.41 cfs @ 12 0.12 cfs @ 12 0.07 cfs @ 12 0.05 cfs @ 12 1 AP3 : Analysis	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn 00% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event .09 hrs, Volume= 0.034 af .42 hrs, Volume= 0.034 af, Atten= 70%, Lag= 20.3 min .40 hrs, Volume= 0.033 af .42 hrs, Volume= 0.000 af .9 point 3			
Second Inflow A Inflow Outflow Discarde Seconda Rout	ary OutFlo rea = = = ed = ary = ed to Reach	w Max=0.00 cfs 0.055 ac,100.0 0.41 cfs @ 12 0.12 cfs @ 12 0.07 cfs @ 12 0.05 cfs @ 12 n AP3 : Analysis	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn 00% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event .09 hrs, Volume= 0.034 af .42 hrs, Volume= 0.034 af, Atten= 70%, Lag= 20.3 min .40 hrs, Volume= 0.033 af .42 hrs, Volume= 0.000 af			
Second Inflow A Inflow Outflow Discarde Seconda Routing	ary OutFlo rea = = ed = ary = ed to Reach by Dyn-Sto	w Max=0.00 cfs 0.055 ac,100.0 0.41 cfs @ 12 0.12 cfs @ 12 0.07 cfs @ 12 0.05 cfs @ 12 n AP3 : Analysis r-Ind method, T	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn 0% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event .09 hrs, Volume= 0.034 af .42 hrs, Volume= 0.034 af, Atten= 70%, Lag= 20.3 min .40 hrs, Volume= 0.033 af .42 hrs, Volume= 0.000 af s Point 3 Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3			
Second Inflow A Inflow Outflow Discarde Seconda Routing Peak Ele	ary OutFlo rea = = ed = ary = ed to Reach by Dyn-Sto ev= 172.00'	w Max=0.00 cfs 0.055 ac,100.0 0.41 cfs @ 12 0.12 cfs @ 12 0.07 cfs @ 12 0.05 cfs @ 12 n AP3 : Analysis r-Ind method, T @ 12.40 hrs \$	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn 0% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event .09 hrs, Volume= 0.034 af .42 hrs, Volume= 0.034 af, Atten= 70%, Lag= 20.3 min .40 hrs, Volume= 0.033 af .42 hrs, Volume= 0.000 af s Point 3 Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Surf.Area= 0.009 ac Storage= 0.013 af			
Second Inflow A Inflow Outflow Discarde Seconda Routing Peak Ele Plug-Flo	ary OutFlo rea = = ed = ary = ed to Reach by Dyn-Sto ev= 172.00'	w Max=0.00 cfs 0.055 ac,100.0 0.41 cfs @ 12 0.12 cfs @ 12 0.07 cfs @ 12 0.05 cfs @ 12 n AP3 : Analysis r-Ind method, T @ 12.40 hrs s n time= 121.2 m	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn 00% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event .09 hrs, Volume= 0.034 af .42 hrs, Volume= 0.034 af, Atten= 70%, Lag= 20.3 min .40 hrs, Volume= 0.033 af .42 hrs, Volume= 0.000 af s Point 3 Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Surf.Area= 0.009 ac Storage= 0.013 af in calculated for 0.034 af (98% of inflow)			
Second Inflow A Inflow Outflow Discarde Seconda Routing Peak Ele Plug-Flc Center-o	ary OutFlo rea = = ed = ary = ed to Reach by Dyn-Sto ev= 172.00' pw detentior of-Mass det	w Max=0.00 cfs 0.055 ac,100.0 0.41 cfs @ 12 0.12 cfs @ 12 0.07 cfs @ 12 0.05 cfs @ 12 n AP3 : Analysis r-Ind method, T @ 12.40 hrs s n time= 121.2 m . time= 109.4 m	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn 0% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event .09 hrs, Volume= 0.034 af .42 hrs, Volume= 0.034 af, Atten= 70%, Lag= 20.3 min .40 hrs, Volume= 0.033 af .42 hrs, Volume= 0.000 af s Point 3 Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Surf.Area= 0.009 ac Storage= 0.013 af in calculated for 0.034 af (98% of inflow) in (850.6 - 741.2)			
Second Inflow A Inflow Outflow Discarde Seconda Routing Peak Ele Plug-Flo Center-o	ary OutFlo rea = = ed = ary = ed to Reach by Dyn-Sto ev= 172.00' ow detention of-Mass det	w Max=0.00 cfs 0.055 ac,100.0 0.41 cfs @ 12 0.12 cfs @ 12 0.07 cfs @ 12 0.05 cfs @ 12 n AP3 : Analysis r-Ind method, T @ 12.40 hrs s n time= 121.2 m time= 109.4 m	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn 0% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event .09 hrs, Volume= 0.034 af .42 hrs, Volume= 0.034 af, Atten= 70%, Lag= 20.3 min .40 hrs, Volume= 0.033 af .42 hrs, Volume= 0.003 af .42 hrs, Volume= 0.000 af s Point 3 Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Surf.Area= 0.009 ac Storage= 0.013 af in calculated for 0.034 af (98% of inflow) in (850.6 - 741.2) ge Storage Description			
Second Inflow A Inflow Outflow Discarde Seconda Routing Peak Ele Plug-Flc Center-o Volume #1	ary OutFlo rea = = ed = ary = ed to Reach by Dyn-Sto ev= 172.00' bw detention of-Mass det <u>Inver</u> 168.15	w Max=0.00 cfs 0.055 ac,100.0 0.41 cfs @ 12 0.12 cfs @ 12 0.07 cfs @ 12 0.05 cfs @ 12 0.05 cfs @ 12 n AP3 : Analysis r-Ind method, T @ 12.40 hrs s n time= 121.2 m time= 109.4 m t Avail.Storag	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn 10% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event .09 hrs, Volume= 0.034 af .42 hrs, Volume= 0.034 af, Atten= 70%, Lag= 20.3 min .40 hrs, Volume= 0.033 af .42 hrs, Volume= 0.000 af s Point 3 Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Surf.Area= 0.009 ac Storage= 0.013 af in calculated for 0.034 af (98% of inflow) in (850.6 - 741.2) ge Storage Description af 4.00'W x 95.00'L x 3.85'H Prismatoid			
Second Inflow A Inflow Outflow Discarde Seconda Routing Peak Ele Plug-Flo Center-o Volume #1	ary OutFlo rea = = ed = ary = ed to Reach by Dyn-Sto ev= 172.00' ow detention of-Mass det <u>Inver</u> 168.15	w Max=0.00 cfs 0.055 ac,100.0 0.41 cfs @ 12 0.12 cfs @ 12 0.07 cfs @ 12 0.05 cfs @ 12 0.05 cfs @ 12 n AP3 : Analysis r-Ind method, T @ 12.40 hrs s n time= 121.2 m time= 109.4 m t Avail.Storag	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn 0% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event .09 hrs, Volume= 0.034 af .42 hrs, Volume= 0.034 af, Atten= 70%, Lag= 20.3 min .40 hrs, Volume= 0.033 af .42 hrs, Volume= 0.033 af .42 hrs, Volume= 0.000 af s Point 3 5 Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Surf.Area= 0.009 ac Storage= 0.013 af in calculated for 0.034 af (98% of inflow) in (850.6 - 741.2) ge Storage Description af 4.00'W x 95.00'L x 3.85'H Prismatoid 0.034 af Overall x 40.0% Voids			
Second Inflow A Inflow Outflow Discarde Seconda Routing Peak Ele Plug-Flo Center-o Volume #1	ary OutFlo rea = = ed = ary = ed to Reach by Dyn-Sto ev= 172.00' ow detention of-Mass det <u>Inver</u> 168.15 <u>Routing</u>	w Max=0.00 cfs 0.055 ac,100.0 0.41 cfs @ 12 0.12 cfs @ 12 0.07 cfs @ 12 0.05 cfs @ 12 n AP3 : Analysis r-Ind method, T @ 12.40 hrs \$ n time= 121.2 m time= 109.4 m <u>t Avail.Storag</u> 0.013	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn 00% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event .09 hrs, Volume= 0.034 af .42 hrs, Volume= 0.034 af, Atten= 70%, Lag= 20.3 min .40 hrs, Volume= 0.033 af .42 hrs, Volume= 0.000 af s Point 3 Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Surf.Area= 0.009 ac Storage= 0.013 af in calculated for 0.034 af (98% of inflow) in (850.6 - 741.2) ge Storage Description af 4.00'W x 95.00'L x 3.85'H Prismatoid 0.034 af Overall x 40.0% Voids			
Second Inflow A Inflow Outflow Discarde Seconda Routing Peak Ele Plug-Flo Center-o Volume #1 <u>Device</u> #0	ary OutFlo rea = = ed = ary = ed to Reach by Dyn-Sto ev= 172.00' ow detention of-Mass det <u>Inver</u> 168.15 <u>Routing</u> Secondary	w Max=0.00 cfs 0.055 ac,100.0 0.41 cfs @ 12 0.12 cfs @ 12 0.07 cfs @ 12 0.05 cfs @ 12 0.05 cfs @ 12 n AP3 : Analysis r-Ind method, T @ 12.40 hrs \$ n time= 121.2 m time= 109.4 m t Avail.Storag ' 0.013 Invert / 172.00'	s @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater) Summary for Pond 22P: Barn 00% Impervious, Inflow Depth > 7.53" for 100-YR 24HR event .09 hrs, Volume= 0.034 af .42 hrs, Volume= 0.034 af, Atten= 70%, Lag= 20.3 min .40 hrs, Volume= 0.033 af .42 hrs, Volume= 0.000 af s Point 3 Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Surf.Area= 0.009 ac Storage= 0.013 af in calculated for 0.034 af (98% of inflow) in (850.6 - 741.2) ge Storage Description af 4.00'W x 95.00'L x 3.85'H Prismatoid 0.034 af Overall x 40.0% Voids Outlet Devices Automatic Storage Overflow (Discharged without head)			

22201-PROPOSED	Type III 24-hr	100-YR 24HR Rainfall=7.77"
Prepared by Jones & Beach Engineers Inc		Printed 3/22/2024
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Conductivity to Groundwater Elevation = 168.00' Phase-In= 0.10'

Discarded OutFlow Max=0.07 cfs @ 12.40 hrs HW=172.00' (Free Discharge) **1=Exfiltration** (Controls 0.07 cfs)

Secondary OutFlow Max=0.00 cfs @ 12.42 hrs HW=172.00' TW=0.00' (Dynamic Tailwater)

Summary for Pond 23P: Drip Edge

Inflow Area = 0.013 ac, 15.85% Impervious, Inflow Depth > 5.99" for 100-YR 24HR event Inflow = 0.09 cfs @ 12.09 hrs, Volume= 0.007 af Outflow = 0.03 cfs @ 12.46 hrs, Volume= 0.004 af, Atten= 70%, Lag= 22.5 min Discarded = 0.00 cfs @ 12.40 hrs, Volume= 0.003 af Secondary = 0.02 cfs @ 12.46 hrs, Volume= 0.001 af Routed to Reach AP3 : Analysis Point 3 0.001 af 0.001 af					
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 172.00' @ 12.40 hrs Surf.Area= 0.003 ac Storage= 0.003 af					
Plug-Flow detention time= 270.8 min calculated for 0.004 af (65% of inflow) Center-of-Mass det. time= 174.5 min (965.5 - 791.0)					
Volume Invert Avail.Storage Storage Description					
#1 169.00' 0.003 af 3.00'W x 40.00'L x 3.00'H Prismatoid 0.008 af Overall x 40.0% Voids					
Device Routing Invert Outlet Devices					
#0 Secondary 172.00' Automatic Storage Overflow (Discharged without head)					
#1 Discarded 169.00' 0.300 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 168.00' Phase-In= 0.10'					
Discarded OutFlow Max=0.00 cfs @ 12.40 hrs HW=172.00' (Free Discharge) 1=Exfiltration (Controls 0.00 cfs)					
Secondary OutFlow Max=0.00 cfs @ 12.46 hrs HW=172.00' TW=0.00' (Dynamic Tailwater)					
Summary for Pond 24P: Plunge Pool with Culvert Outlet					
Inflow Area = 0.213 ac, 18.90% Impervious, Inflow Depth > 5.29" for 100-YR 24HR event Inflow = 1.13 cfs @ 12.14 hrs, Volume= 0.094 af Outflow = 1.12 cfs @ 12.15 hrs, Volume= 0.094 af, Atten= 0%, Lag= 0.6 min Primary = 1.12 cfs @ 12.15 hrs, Volume= 0.094 af Routed to Reach 3R : Culvert					
Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 193.51' @ 12.15 hrs Surf.Area= 137 sf Storage= 48 cf					

Plug-Flow detention time= 1.5 min calculated for 0.094 af (100% of inflow) Center-of-Mass det. time= 1.1 min (810.3 - 809.2)

	D® 10.20-3c	s/n 00762 © 2	023 HydroCAD S	Software Solutions LLC	Page
/olume	Invert	Avail.Stora	ide Storade D	Description	
#1	193.00'	475	ocf Custom	Stage Data (Prismati	c) Listed below (Recalc)
Elovatio	n Su	rf Area	Inc Store	Cum Store	
fee)	et)	(sq-ft) (cubic-feet)	(cubic-feet)	
193.0	00	51	0	0	
194.0	00	222	137	137	
195.0	00	455	339	475	
)evice	Routing	Invert	Outlet Devices		
#1	Primary	193.00'	15.0" Round	Culvert	
			L= 50.0' CPP,	, square edge headwa	II, Ke= 0.500
			Inlet / Outlet In	vert= 193.00' / 192.50	' S= 0.0100 '/' Cc= 0.900
			1 - 0.012, FIOW	V Alea- 1.25 SI	
rimary —1=Cu	OutFlow Ma Ilvert (Inlet C	ax=1.12 cfs @ controls 1.12 c	12.15 hrs HW fs @ 2.42 fps)	/=193.50' TW=192.75	' (Dynamic Tailwater)
		Su	Immary for F	Pond 25P: Drip Ec	lge
flow A	rea = 0	012 20 100 0	0% Impervious	Inflow Depth > 7.53	8" for 100 VP 24HP event
niow A nflow	= 0	.012 ac, 100.0 09 cfs @ 12	09 hrs Volum	e = 0.007 af	5 IOI IOO-IR 24HR event
outflow	= 0.	02 cfs @ 12.	44 hrs, Volum	e= 0.007 af, A	Atten= 73%, Lag= 21.3 min
iscarde		00 -t- <u></u>	A A L		
	ea – 0.	02 CTS @ 12.	44 nrs, voium	e= 0.007 af	
econda	ary = 0.1	02 cfs @ 12. 00 cfs @ 0.	44 nrs, Volum 00 hrs, Volum	e= 0.007 af e= 0.000 af	
econda Route	ary = 0. ary = 0. ed to Reach 6	02 cfs @ 12. 00 cfs @ 0. 6R : Flow Thro	44 nrs, Volum 00 hrs, Volum ough 5S	e= 0.007 af e= 0.000 af	
econda Route	ary = 0. ary = 0. ed to Reach 6	02 cfs @ 12. 00 cfs @ 0. 5R : Flow Thro Ind method, T	44 nrs, Volum 00 hrs, Volum bugh 5S ime Span= 0.00	e= 0.007 af e= 0.000 af 0-24.00 hrs, dt= 0.05 l	nrs / 3
econda Route outing eak Ele	ed – 0. ary = 0. ed to Reach 6 by Dyn-Stor-l ev= 195.88' @	02 crs @ 12. 00 cfs @ 0. 5R : Flow Thro Ind method, T 0 12.44 hrs S	44 nrs, Volum 00 hrs, Volum ough 5S ime Span= 0.00 ourf.Area= 0.00	e= 0.007 af e= 0.000 af 0-24.00 hrs, dt= 0.05 f 3 ac Storage= 0.002	nrs / 3 af
econda Route outing eak Ele lug-Flo enter-o	ed – 0. ary = 0. ed to Reach 6 by Dyn-Stor-l ev= 195.88' @ w detention ti of-Mass det. ti	02 crs @ 12. 00 cfs @ 0. 5R : Flow Thro Ind method, T 0 12.44 hrs S ime= 64.8 min ime= 58.8 min	44 nrs, Volum 00 hrs, Volum ough 5S ime Span= 0.00 curf.Area= 0.00 calculated for (800.0 - 741.2	e= 0.007 af e= 0.000 af 0-24.00 hrs, dt= 0.05 H 3 ac Storage= 0.002 0.007 af (99% of inflor 2)	nrs / 3 af W)
econda Routing Peak Ele Plug-Flo Center-c	ed – 0. ary = 0. ed to Reach 6 by Dyn-Stor-l ev= 195.88' @ w detention to of-Mass det. to	02 crs @ 12. 00 cfs @ 0. 5R : Flow Thro Ind method, T 0 12.44 hrs S ime= 64.8 min ime= 58.8 min	44 nrs, Volum 00 hrs, Volum ough 5S ime Span= 0.00 calculated for (800.0 - 741.2	e= 0.007 af e= 0.000 af 0-24.00 hrs, dt= 0.05 f 3 ac Storage= 0.002 0.007 af (99% of inflov 2)	nrs / 3 af w)
econda Routing eak Ele lug-Flo enter-c olume #1	ed – 0. ary = 0. ed to Reach 6 by Dyn-Stor-l ev= 195.88' @ w detention ti of-Mass det. ti <u>Invert</u> 193.75'	02 crs @ 12. 00 cfs @ 0. 5R : Flow Thro 10 method, T 12.44 hrs 5 ime= 64.8 min ime= 58.8 min <u>Avail.Storac</u> 0.003	44 nrs, Volum 00 hrs, Volum ough 5S ime Span= 0.00 curf.Area= 0.00 calculated for (800.0 - 741.2 <u>e Storage De</u> af 3.00'W x 4	e= 0.007 af e= 0.000 af 0-24.00 hrs, dt= 0.05 H 3 ac Storage= 0.002 0.007 af (99% of inflow 2) escription 1.00'L x 2.25'H Prism	nrs / 3 af w)
econda Routing eak Ele lug-Flo enter-c <u>olume</u> #1	ed – 0. ary = 0. ed to Reach 6 by Dyn-Stor-l ev= 195.88' @ w detention to of-Mass det. to <u>Invert</u> 193.75'	02 cfs @ 12. 00 cfs @ 0. 5R : Flow Thro Ind method, T 0 12.44 hrs S ime= 64.8 min ime= 58.8 min <u>Avail.Storac</u> 0.003	44 nrs, Volum 00 hrs, Volum ough 5S ime Span= 0.00 calculated for (800.0 - 741.2 <u>le Storage De</u> af 3.00'W x 4 0.006 af O	e= 0.007 af e= 0.000 af 0-24.00 hrs, dt= 0.05 H 3 ac Storage= 0.002 0.007 af (99% of inflow 2) escription 1.00'L x 2.25'H Prism verall x 40.0% Voids	nrs / 3 af w) natoid
econda Routing eak Ele lug-Flo enter-c <u>olume</u> #1	ed – 0. ary = 0. ed to Reach 6 by Dyn-Stor-l ev= 195.88' @ w detention to of-Mass det. to <u>Invert</u> 193.75' Routing	02 crs @ 12. 00 cfs @ 0. 5R : Flow Thro Ind method, T 0 12.44 hrs S ime= 64.8 min ime= 58.8 min <u>Avail.Storac</u> 0.003	44 nrs, Volum 00 hrs, Volum ough 5S ime Span= 0.00 calculated for (800.0 - 741.2 <u>le Storage De</u> af 3.00'W x 4 0.006 af O ^o	e= 0.007 af e= 0.000 af 0-24.00 hrs, dt= 0.05 f 3 ac Storage= 0.002 0.007 af (99% of inflow 2) escription 1.00'L x 2.25'H Prism verall x 40.0% Voids	nrs / 3 af w) natoid
econda Routing eak Ele lug-Flo enter-co olume #1 evice #0	ed – 0. ary = 0. ed to Reach 6 by Dyn-Stor- ev= 195.88' @ w detention ti of-Mass det. ti <u>Invert</u> 193.75' <u>Routing</u> Secondary	02 crs @ 12. 00 cfs @ 0. 5R : Flow Thro Ind method, T 0 12.44 hrs S ime= 64.8 min ime= 58.8 min <u>Avail.Storac</u> 0.003 <u>Invert</u> 196.00'	44 nrs, Volum 00 hrs, Volum ough 5S ime Span= 0.00 calculated for (800.0 - 741.2 <u>le Storage De</u> af 3.00'W x 4 0.006 af O <u>Outlet Devices</u> Automatic Sto	e= 0.007 af e= 0.000 af 0-24.00 hrs, dt= 0.05 H 3 ac Storage= 0.002 0.007 af (99% of inflow 2) escription 1.00'L x 2.25'H Prism verall x 40.0% Voids	harged without head)
econda Routing eak Ele lug-Flo enter-co olume #1 #0 #1	ed – 0. ary = 0. ed to Reach 6 by Dyn-Stor-l ev= 195.88' @ ww detention to of-Mass det. to <u>Invert</u> 193.75' <u>Routing</u> Secondary Discarded	02 cfs @ 12. 00 cfs @ 0. 5R : Flow Thro 11 method, T 12.44 hrs 5 ime= 64.8 min ime= 58.8 min <u>Avail.Storag</u> 0.003 <u>Invert</u> 196.00' 193.75'	44 nrs, Volum 00 hrs, Volum ough 5S ime Span= 0.00 calculated for (800.0 - 741.2 <u>le Storage De</u> af 3.00'W x 4 0.006 af O <u>Outlet Devices</u> Automatic Sto 0.300 in/hr Ext Conductivity to	e= 0.007 af e= 0.000 af 0-24.00 hrs, dt= 0.05 H 3 ac Storage= 0.002 0.007 af (99% of inflow 0 2) escription 1.00'L x 2.25'H Prism verall x 40.0% Voids orage Overflow (Disc filtration over Surfac Groundwater Elevation	hrs / 3 af w) hatoid harged without head) e area on = 193.67' Phase-In= 0.10'
econda Routing eak Ele lug-Flo enter-co <u>olume</u> #1 #0 #1 iscard	ed – 0. ary = 0. ed to Reach 6 by Dyn-Stor-lev= 195.88' @ w detention to of-Mass det. to <u>Invert</u> 193.75' <u>Routing</u> Secondary Discarded ed OutFlow	02 crs @ 12. 00 cfs @ 0. 5R : Flow Thro Ind method, T 0 12.44 hrs S ime= 64.8 min ime= 58.8 min <u>Avail.Storac</u> 0.003 <u>Invert</u> 196.00' 193.75' Max=0.02 cfs ontrols 0.02 cfs	44 nrs, Volume 00 hrs, Volume bugh 5S ime Span= 0.00 calculated for (800.0 - 741.2 <u>le Storage De</u> af 3.00'W x 4 0.006 af Or <u>Outlet Devices</u> Automatic Sto 0.300 in/hr Ext Conductivity to @ 12.44 hrs H	e= 0.007 af e= 0.000 af 0-24.00 hrs, dt= 0.05 H 3 ac Storage= 0.002 0.007 af (99% of inflow 0 2) escription 1.00'L x 2.25'H Prism verall x 40.0% Voids orage Overflow (Disc filtration over Surfac Groundwater Elevatio tW=195.87' (Free Disc	hrs / 3 af w) hatoid harged without head) e area on = 193.67' Phase-In= 0.10' scharge)

APPENDIX III

Test Pit Logs

TEST PITS FOR 669 High Street Candia September 14, 2023 JBE Project No. 22201

Performed by: Joseph Coronati, Jones & Beach Engineers, Inc., SSD #1716

Test Pit #1		
0"- 6"		topsoil
6"- 20"	10YR 4/4	dark yellowish brown fine sandy loam rocky, friable
20"- 60"	10YR 6/4	light yellowish brown sandy clay firm, saturated
SHWT = 20" Roots to 20" $H_2O @ 36"$ No Refusal observed		
Perc Rate = 20 min/inch		
Test Pit #2		
0"-6"		topsoil
6"- 18"	10YR 3/4	dark yellowish brown fine sandy loam friable
18"	10Y 4/4	dark yellowish brown silty sand friable, saturated

SHWT = 18"Roots to 18"H₂O @ 23" No Refusal observed Perc Rate = 20 min/inch



<u>Test Pit #3</u> 0"- 10"		topsoil
10"- 22"	10YR 3/4	dark yellowish brown fine sandy loam friable
22"- 60"	10YR 4/4	dark yellowish brown Ioamy sand friable many mottles
SHWT = 22" Roots to 18" NO H2O No Refusal observed Perc Rate = 16 min/inch		
Test Pit #4 0"- 16"		topsoil
16"- 60"	10YR 4/4	dark yellowish brown loamy sand, wet loose, friable
SHWT = 16" Roots to 16" H₂O @ 16" No Refusal observed Perc Rate = 14 min/inch		
Test Pit #5 0"- 10"		topsoil
10"- 20"	10YR 3/4	dark yellowish brown fine sandy loam friable
20"- 60"	10Y 4/4	dark yellowish brown Ioamy sand firm, mottles
SHWT = 20" Roots to 20" NO H₂O observed No Refusal observed Perc Rate = 14 min/inch		

Test Pit #6 o"- 8"		topsoil
8"- 24"	10YR 3/4	dark yellowish brown fine sandy loam friable
24"- 60"	10Y 4/4	dark yellowish brown loamy sand firm, moist
SHWT = 24" Roots to 24" NO H ₂ O observed No Refusal observed Perc Rate = 14 min/inch		
<u>Test Pit #7</u> o"- 6"		topsoil
6"- 24"	10YR 4/4	dark yellowish brown loamy sand friable, dry
24"- 54"	10YR 4/4	dark yellowish brown Ioamy sand firm, cobbles, mottles
SHWT = 24"		

SHWT = 24" Roots to 24" NO H₂O observed No Refusal observed Perc Rate = 12 min/inch

APPENDIX IV

NRCS Soil Map

Attachment from Candia Planning Board Meeting on 4/3/2024



Conservation Service

MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available А misunderstanding of the detail of mapping and accuracy of soil Water Features line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed В scale. Transportation B/D Rails +++ Please rely on the bar scale on each map sheet for map С measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service US Routes \sim Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available Local Roads Maps from the Web Soil Survey are based on the Web Mercator ~ projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Α -Aerial Photography Albers equal-area conic projection, should be used if more A/D accurate calculations of distance or area are required. в This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: Rockingham County, New Hampshire С Survey Area Data: Version 26, Aug 22, 2023 C/D Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. D Date(s) aerial images were photographed: Data not available. Not rated or not available العراقة Soil Rating Points The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background А imagery displayed on these maps. As a result, some minor A/D shifting of map unit boundaries may be evident. В B/D



Hydrologic Soil Group-Rockingham County, New Hampshire

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
140B	Chatfield-Hollis-Canton complex, 0 to 8 percent slopes, rocky	В	6.9	35.9%
446A	Scituate-Newfields complex, 0 to 3 percent slopes	С	5.7	29.3%
447A	Scituate-Newfields complex, 0 to 3 percent slopes, very stony	C	4.9	25.3%
657B	Ridgebury fine sandy loam, 3 to 8 percent slopes, very stony	D	1.8	9.5%
Totals for Area of Intere	st		19.3	100.0%

Hydrologic Soil Group—Rockingham County, New Hampshire

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

APPENDIX V

Extreme Precipitation Estimates



Extreme Precipitation Tables

Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Metadata for Point												
Smoothing State	Yes											
Location												
Latitude	43.076 degrees North											
Longitude	71.342 degrees West											
Elevation	140 feet											
Date/Time	Mon Mar 04 2024 16:12:26 GMT-0500 (Eastern Standard Time)											

Extreme Precipitation Estimates

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7d
1yr	0.26	0.40	0.49	0.65	0.81	1.02	1yr	0.70	0.98	1.18	1.50	1.90	2.42	2.65	1yr	2.15	2.55	2.95	3.
2yr	0.32	0.49	0.61	0.80	1.01	1.27	2yr	0.87	1.16	1.47	1.85	2.31	<mark>2.90</mark>	3.23	2yr	2.57	3.11	3.59	4.
5yr	0.38	0.58	0.73	0.98	1.26	1.60	5yr	1.08	1.46	1.86	2.33	2.92	3.65	4.12	5yr	3.23	3.96	4.56	5.
10yr	0.42	0.66	0.84	1.14	1.48	1.90	10yr	1.28	1.72	2.22	2.79	3.49	<mark>4.34</mark>	4.95	10yr	3.84	4.76	5.47	6.
25yr	0.50	0.79	1.01	1.39	1.85	2.39	25yr	1.59	2.15	2.79	3.53	4.41	<mark>5.47</mark>	6.31	25yr	4.84	6.07	6.96	8.
50yr	0.57	0.91	1.16	1.62	2.18	2.85	50yr	1.88	2.55	3.34	4.22	5.27	<mark>6.51</mark>	7.59	50yr	5.77	7.30	8.35	9.
100yr	0.64	1.04	1.34	1.89	2.58	3.40	100yr	2.23	3.03	4.00	5.05	6.30	<mark>7.77</mark>	9.13	100yr	6.87	8.78	10.02	11
200yr	0.73	1.20	1.55	2.22	3.06	4.04	200yr	2.64	3.59	4.76	6.03	7.51	9.26	11.00	200yr	8.20	10.57	12.02	13
500yr	0.88	1.44	1.88	2.73	3.82	5.09	500yr	3.30	4.51	6.02	7.63	9.51	11.70	14.06	500yr	10.35	13.52	15.32	16

Lower Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7d
1yr	0.22	0.33	0.41	0.55	0.67	0.88	1yr	0.58	0.86	1.04	1.34	1.58	2.10	2.48	1yr	1.86	2.38	2.73	3.
2yr	0.31	0.48	0.59	0.79	0.98	1.16	2yr	0.84	1.14	1.32	1.75	2.23	2.81	3.11	2yr	2.49	2.99	3.48	4.
5yr	0.35	0.54	0.67	0.92	1.17	1.39	5yr	1.01	1.36	1.56	2.03	2.60	3.35	3.74	5yr	2.97	3.60	4.17	5.
10yr	0.39	0.60	0.74	1.03	1.34	1.58	10yr	1.15	1.54	1.77	2.29	2.92	3.82	4.29	10yr	3.38	4.13	4.77	5.
25yr	0.45	0.68	0.85	1.21	1.59	1.85	25yr	1.37	1.81	2.09	2.66	3.41	4.52	5.13	25yr	4.00	4.93	5.68	6.
50yr	0.49	0.75	0.94	1.35	1.81	2.10	50yr	1.57	2.05	2.36	2.99	3.83	5.13	5.86	50yr	4.54	5.63	6.47	7.
100yr	0.56	0.84	1.05	1.52	2.09	2.38	100yr	1.80	2.33	2.68	3.36	4.31	5.81	6.69	100yr	5.14	6.43	7.36	9.
200yr	0.62	0.93	1.18	1.71	2.39	2.69	200yr	2.06	2.63	3.04	3.77	4.85	6.57	8.07	200yr	5.82	7.76	8.37	10
500yr	0.72	1.08	1.38	2.01	2.86	3.17	500yr	2.47	3.10	3.59	4.40	5.69	7.70	9.70	500yr	6.82	9.33	9.88	12

Upper Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7d
1yr	0.29	0.45	0.55	0.73	0.90	1.08	1yr	0.78	1.05	1.21	1.61	2.04	2.61	2.89	1yr	2.31	2.78	3.28	3.
2yr	0.33	0.51	0.63	0.85	1.04	1.25	2yr	0.90	1.22	1.41	1.86	2.37	3.02	3.37	2yr	2.68	3.24	3.76	4.
5yr	0.41	0.63	0.78	1.07	1.36	1.59	5yr	1.17	1.55	1.81	2.34	2.99	3.96	4.53	5yr	3.50	4.36	4.98	5.
10yr	0.49	0.75	0.93	1.29	1.67	1.93	10yr	1.44	1.89	2.19	2.81	3.57	4.88	5.69	10yr	4.32	5.47	6.21	7.
25yr	0.62	0.94	1.17	1.67	2.20	2.51	25yr	1.90	2.45	2.83	3.56	4.51	6.46	7.70	25yr	5.72	7.40	8.30	9.
50yr	0.73	1.12	1.39	2.00	2.69	3.06	50yr	2.32	2.99	3.42	4.27	5.40	7.99	9.71	50yr	7.08	9.33	10.36	11
100yr	0.88	1.34	1.67	2.42	3.32	3.73	100yr	2.86	3.65	4.15	5.13	6.46	9.90	12.24	100yr	8.76	11.77	12.94	13
200yr	1.06	1.59	2.02	2.92	4.07	4.56	200yr	3.51	4.46	5.04	6.16	7.74	12.28	14.68	200yr	10.87	14.12	16.19	17
500yr	1.35	2.01	2.59	3.76	5.35	5.95	500yr	4.61	5.82	6.52	7.86	9.84	16.34	19.81	500yr	14.46	19.05	21.78	22



APPENDIX VI

Rip Rap Calculations
RIP RAP CALCULATIONS

"Beaver Meadows" 669 High Street, Candia, NH 03034 JBE #22201

Jones & Beach Engineers, Inc. P.O. Box 219 Stratham, NH 03885 22-Mar-24

Rip Rap equations were obtained from the *Stormwater Management and Erosion Control Handbook for Urban and Developing Areas in New Hampshire.* Aprons are sized for the 25-Year storm event.

TAILWATER < HALF THE D_0

$$\begin{split} &L_a = (1.8 \ x \ Q) \ / \ {D_0}^{3/2} + (7 \ x \ D_o) \\ &W = L_a + (3 \ x \ D_o) \ or \ defined \ channel \ width \\ &d_{50} = (0.02 \ x \ Q^{4/3}) \ / \ (T_w \ x \ D_0) \end{split}$$

Culvert or	Tailwater	Discharge	Diameter	Length of	Width of	d50-Median Stone
Catch Basin	(Feet)	(C.F.S.)	of Pipe	Rip Rap	Rip Rap	Rip Rap
(Sta. No.)	T _w	Q	D _o	L _a (feet)	W (feet)	d50 (feet)
3P	0.26	0.52	1.25	9.4	13	0.03
24P	0.26	0.69	1.25	9.6	13	0.04
3R	0.62	2.71	1.25	12.2	16	0.10

TAILWATER > HALF THE D_0

$$\begin{split} &L_a = (3.0 \ x \ Q) \ / \ {D_0}^{3/2} + (7 \ x \ D_o) \\ &W = (0.4 \ x \ L_a) + (3 \ x \ D_o) \ \text{or defined channel width} \\ &d_{50} = (0.02 \ x \ Q^{4/3}) \ / \ (T_w \ x \ D_0) \end{split}$$

Culvert or	Tailwater	Discharge	Diameter	Length of	Width of	d ₅₀ -Median Stone
Catch Basin	(Feet)	(C.F.S.)	of Pipe	Rip Rap	Rip Rap	Rip Rap
(Sta. No.)	T_{w}	Q	D _o	L _a (feet)	W (feet)	d50 (feet)
				#DIV/0!	#DIV/0!	#DIV/0!

Table 7-24 Recommended Rip Rap Gradation Ranges				
d ₅₀ Size =	0.25	Feet	3	Inches
% of Weight Smaller		Si	ze of Stone (Ind	ches)
Than the Given d ₅₀ Size		From		То
100%		5		6
85%		4		5
50%		3		5
15%		1		2

Table 7-24 Recommended Rip Rap Gradation Ranges				
d_{50} Size =	0.5	Feet	6	Inches
% of Weight Smaller		Siz	ze of Stone (Inc	hes)
Than the Given d ₅₀ Size		From		То
100%		9		12
85%		8		11
50%		6		9
15%		2		3

APPENDIX VII

Stormwater Operations and Maintenance Manual

STORMWATER MANAGEMENT OPERATIONS AND MAINTENANCE MANUAL

"Beaver Meadows" 669 High Street Candia, NH 03034 Tax Map 405, Lot 48

Prepared for:

Bob Carr 17 Vassar Street Manchester, NH 03104

> Prepared by: Jones & Beach Engineers, Inc. 85 Portsmouth Avenue P.O. Box 219 Stratham, NH 03885 (603) 772-4746 March 22, 2024 JBE Project No. 22201



Inspection and Maintenance of Facilities and Property

A. Maintenance of Common Facilities or Property

1. The Landowner, future owners and assigns are responsible to perform the maintenance obligations or hire a Professional Engineer to review the site on an annual basis for maintenance and certification of the stormwater system. The same shall keep receipts and records of all maintenance companies hired throughout the year to submit along with the following form.

B. General Inspection and Maintenance Requirements

- 1. Permanent stormwater and sediment and erosion control facilities to be maintained on the site include, but are not limited to, the following:
 - a. Roadway and driveways
 - b. Vegetation and landscaping
 - c. Detention Pond
 - d. Stone Drip Edges
 - e. Culverts
 - f. Rip-Rap Outlet Protection Aprons
 - g. Swale
- 2. Maintenance of permanent measures shall follow the following schedule:
 - a. Normal winter roadway maintenance including plowing and snow removal. Road sweeping at the end of every winter, preferably before the start of the spring rain season.
 - b. **Annual inspection** of the site for erosion, destabilization, settling, and sloughing. Any needed repairs are to be conducted immediately. **Annual inspection** of site's vegetation and landscaping. Any areas that are bare shall be reseeded and mulched with hay or, if the case is extreme, loamed and seeded or sodded to ensure adequate vegetative cover. Landscape specimens shall be replaced in kind, if they are found to be dead or dying.
 - c. Detention Ponds:

Detention ponds should require little maintenance, but must be inspected frequently during the first year of operation, and annually thereafter. Every five years, the services of a professional engineer shall be retained to perform a thorough inspection of all the aspects of the pond and its infrastructure. Any debris and sediment accumulations need to be removed from the outlet structure and disposed of properly. Inspect outlet structure for deterioration and or clogging. Detention pond should be mowed at least once annually so as to prevent the establishment of woody vegetation – trees must *never* be allowed to grow in a detention pond or its side slopes, as they may destabilize the structure and increase the potential for failure. Areas showing signs of erosion or thin or dying vegetation need to be repaired immediately by whatever means necessary, *with the exception of fertilizer*. Rodent burrows are to be repaired immediately and the suspect animals apprehended with non-lethal traps if the problem persists



d. Stone Drip Edges:

In the spring and fall, visually inspect the area around the edges and repair any erosion. Use small stones to stabilize erosion along drainage paths. Inspect stone area to ensure that it has not been displaced, undermined, or otherwise damaged. Displaced rock shall be replaced, or additional rock added in order to maintain the structure(s) in their undamaged state. Woody vegetation shall not be allowed to become established in stone areas, and/or any debris removed from the void spaces between the stones.

- e. **Inspection** of culvert inlets and outlets at least **once per month** during the rainy season (March to November). Any debris is to be removed and disposed of properly.
 - f. Rock riprap shall be **inspected annually** in order to ensure that it has not been displaced, undermined, or otherwise damaged. Displaced rock shall be replaced, or additional rock added in order to maintain the structure(s) in their undamaged state. Woody vegetation must not be allowed to become established in riprap areas, and/or any debris removed from the void spaces between the rocks. If the riprap is adjacent to a stream or other waterbody, the water shall be kept clear of obstructions, debris, and sediment deposits
 - g. Swales Inspect swales annually for erosion, sediment accumulation, vegetation loss, and presence of invasive species. Perform periodic mowing; frequency depends on location and type of grass. Remove debris and accumulated sediment, based on inspection. Repair eroded areas, remove invasive species and dead vegetation, and reseed as warranted by inspection

See attached sample forms as a guideline.

Any inquiries in regards to the design, function, and/or maintenance of any one of the above-mentioned facilities or tasks shall be directed to the project engineer:

Jones & Beach Engineers, Inc. 85 Portsmouth Avenue P.O. Box 219 Stratham, NH 03885

T#: (603) 772-4746 F#: (603) 772-0227



Commitment to maintenance requirements

I agree to complete and/or observe all of the required maintenance practices and their respective schedules as outlined above.

Signature

Print Name

Title

Date



Annual Operations and Maintenance Report

The Condominium Association, future owners and assigns are responsible to perform the maintenance obligations or hire a Professional Engineer to review the site on an annual basis for maintenance and certification of the stormwater system. The Association shall keep receipts and records of all maintenance companies hired throughout the year to submit along with the following form.

Construction Activity	Date of Inspection	Who Inspected	Findings of Inspector
Roadway and			
Driveways			
Vegetation and			
Landscaping			
Detention Pond			
Stone Drin Edges			
Stolle Drip Edges			
Culverts			
Rip Rap Outlet Protection			



Swales		
Other (please note):		



APPENDIX VIII

Pre- and Post-Construction Watershed Plans



CATCHMENT CH D	$\overbrace{\times}{\times}$
PATH	
ANDS 5 SOILS	
V ARROW	



TOTAL LOT AREA 87.8 ACRES

EXISTING WATERSHED PLAN

DRAWING No.







SUBCATCHMENTIREACHIXPONDIXTC PATH→→→WETLANDS→→→NRCS SOILS→→→FLOW ARROW→√→

PROJECT PARCEL TOWN OF CANDIA TAX MAP 405, LOT 48

APPLICANT BOB CARR 17 VASSAR STREET MANCHESTER, NH 03104 BK 6150, PG 2657

TOTAL LOT AREA 87.8 ACRES

PROPOSED WATERSHED PLAN

 Project:
 "BEAVER MEADOWS" 669 HIGH STREET, CANDIA, NH 03034

 Owner of Record:
 CLAUDIA PATRICIA CARR REVOCABLE TRUST AGREEMENT 17 VASSAR STREET, MANCHESTER, NH 03104

 DRAWING No.











